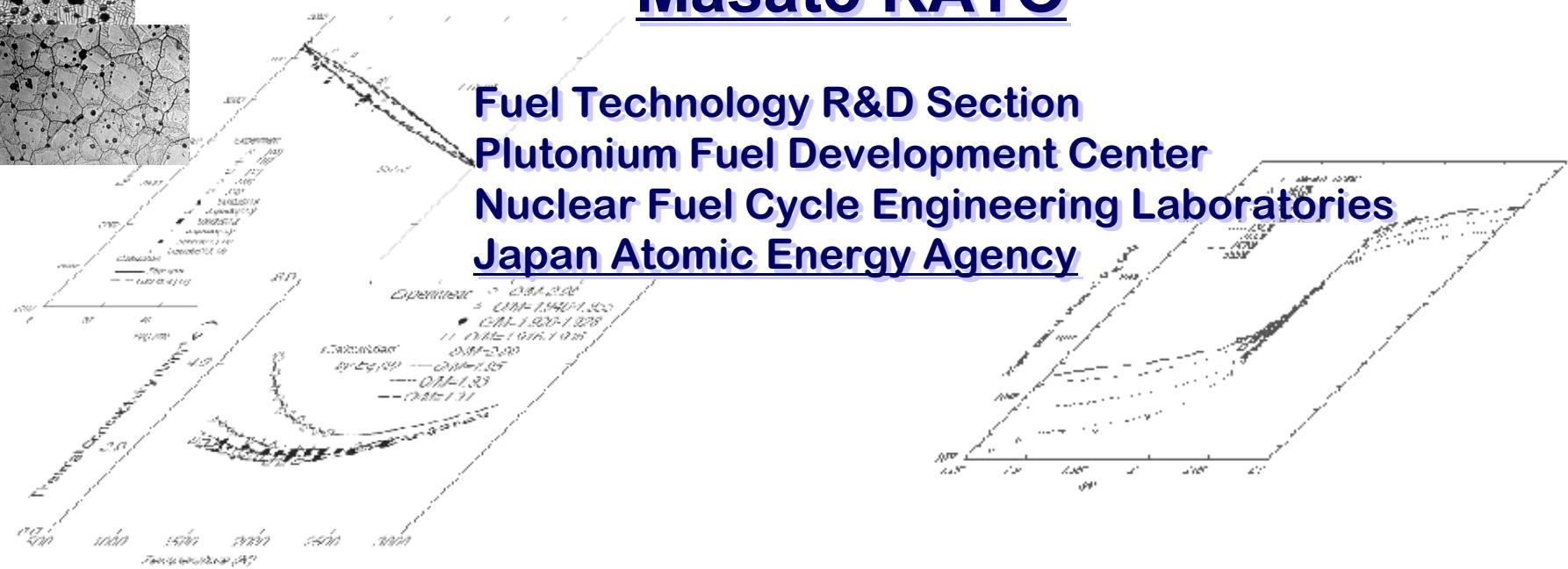


Development of Np and Am bearing MOX fuels for Japan sodium cooled fast reactors

Masato KATO

Fuel Technology R&D Section
Plutonium Fuel Development Center
Nuclear Fuel Cycle Engineering Laboratories
Japan Atomic Energy Agency



Japan Atomic Energy Agency

Background

— Development of MOX containing MA —



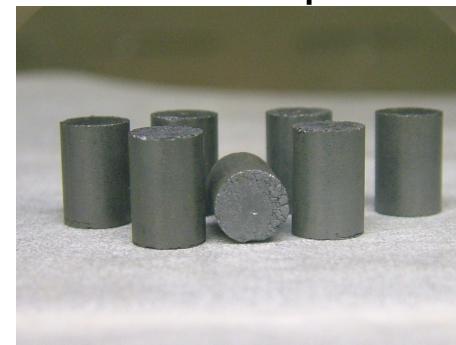
➤ Japan Atomic Energy Agency has developed homogeneous mixed oxide containing minor actinides (MA-MOX) for Japan sodium-cooled fast reactors.

Subjects to be carried out

1. Database and models for properties
2. Advanced fabrication process
3. Analysis code of irradiation behaviour of low O/M MA-MOX pellet



Hollow MOX pellets



Pellets of $(\text{Np}_{0.02}\text{Am}_{0.02}\text{Pu}_{0.3}\text{U}_{0.64})\text{O}_2$

Specification of the fuel pellet

Type : Hollow type

Pu content : 20 - 30%

MA content : ~ 5% (Np+Am+Cm)

Density : 95% TD

O/M : < 1.97

Background

— Development of MOX containing MA —



- Japan Atomic Energy Agency has developed homogeneous mixed oxide containing minor actinides (MA-MOX) for Japan sodium-cooled fast reactors.

Subjects to be carried out

1. Database and models for properties
2. Advanced fabrication process
3. Analysis code of irradiation behaviour of low O/M MA-MOX pellet

Experimental evaluation

1. Property Measurements
 - Thermodynamic data
 - Thermal properties
 - Chemical properties
2. Pellet Fabrication Test
 - Homogenization
 - O/M adjustment Technology
 - Sintering behavior
3. Irradiation test
 - Actinide redistribution
 - Microstructure change
 - FCCI

Background

— Development of MOX containing MA —



- Japan Atomic Energy Agency has developed homogeneous mixed oxide containing minor actinides (MA-MOX) for Japan sodium-cooled fast reactors.

Subjects to be carried out

1. Database and models for properties
2. Advanced fabrication process
3. Analysis code of irradiation behaviour of low O/M MA-MOX pellet

Experimental evaluation

1. Property Measurements
 - Thermodynamic data
 - Thermal properties
 - Chemical properties
2. Pellet Fabrication Test
 - Homogenization
 - O/M adjustment Technology
 - Sintering behaviour
3. Irradiation test
 - Actinide redistribution
 - Microstructure change
 - FCCI

Purpose of this work

To analysis PIE results by using the measured data to develop an analysis code.

Contents

1. Irradiation Test and PIE Results

- Irradiation condition
- Microstructure changes
- Actinides redistribution

2. Properties of the fuel pellets

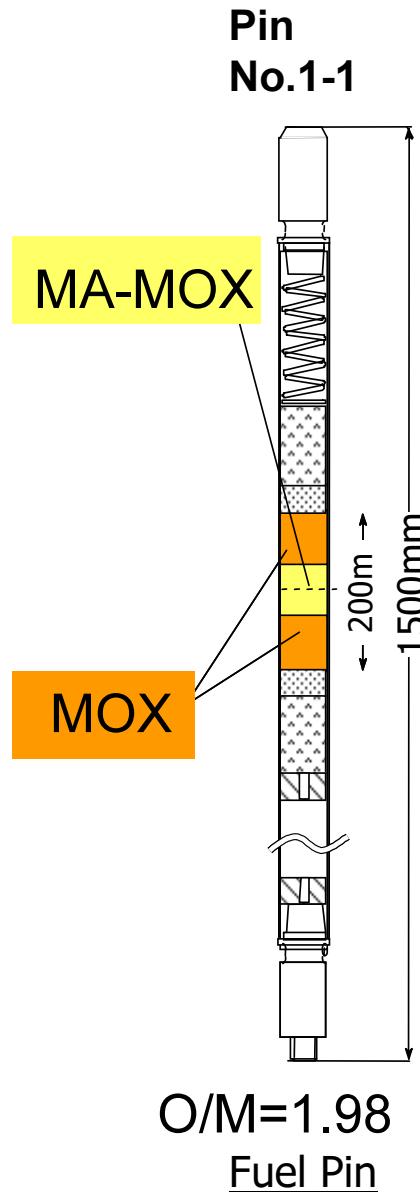
- Evaluation of properties
 - Lattice parameter, Melting temperature
 - Thermal conductivity, Oxygen potential

3. Analysis of Irradiation behaviour

- O/M redistribution
- Relation between Pu redistribution and vapour pressure
- Evaluation of microstructure change

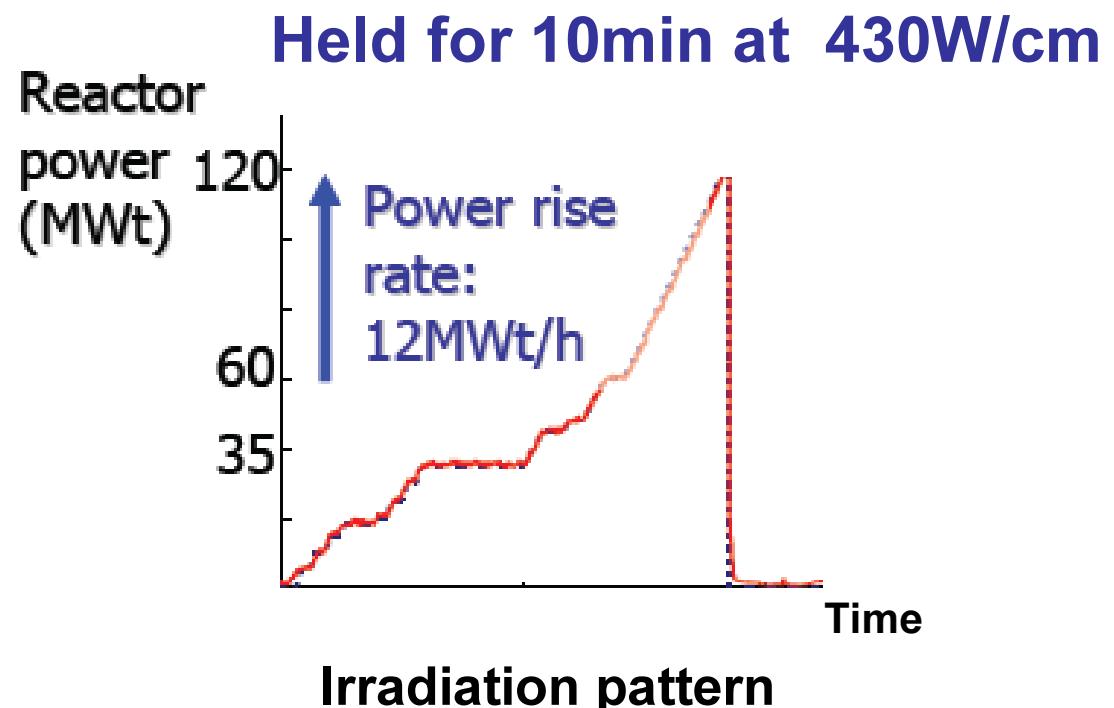
Irradiation test

Condition 1 

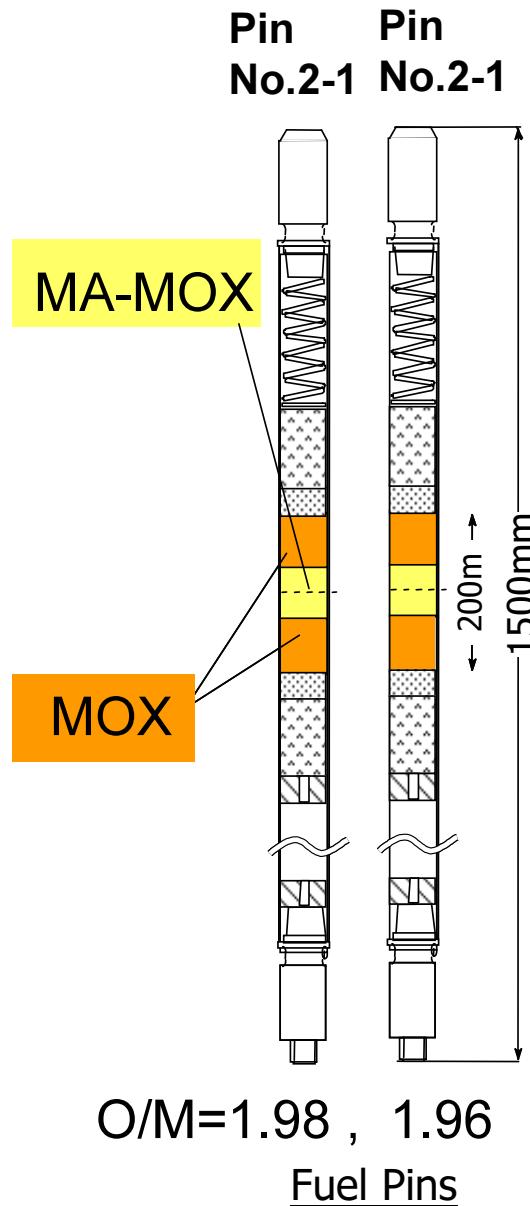


First Test

Pin No.	Name	Composition	O/M
No.1-1	MA-MOX	$(\text{Np}_{0.016}\text{Am}_{0.016}\text{Pu}_{0.3}\text{U}_{0.668})\text{O}_y$	1.98
	MOX	$(\text{Pu}_{0.3}\text{U}_{0.7})\text{O}_y$	1.98



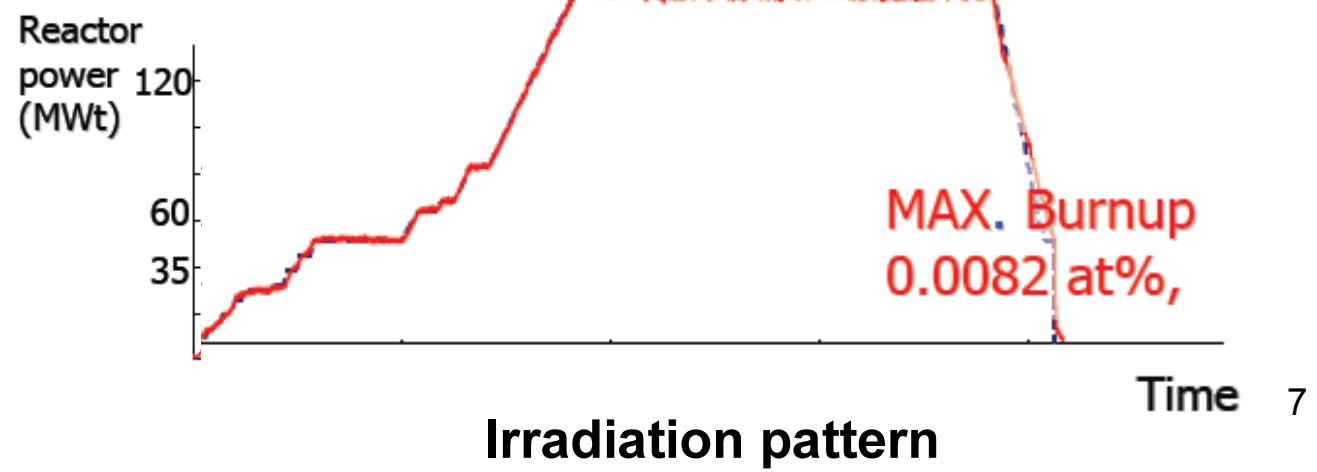
Irradiation test



Second Test

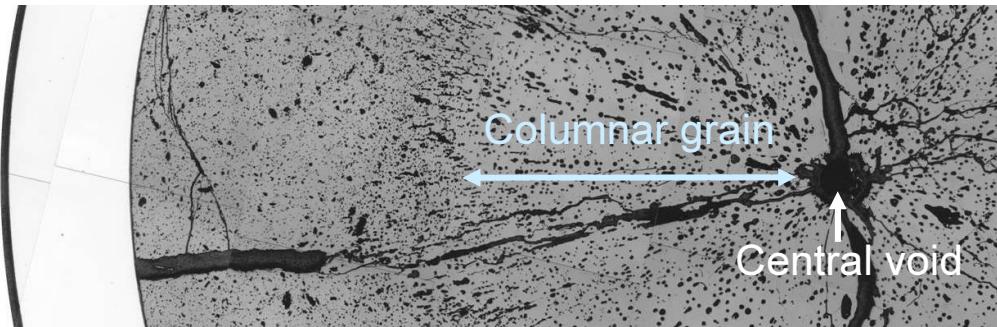
Pin No.	Name	Composition	O/M
No.2-1	MA-MOX	$(\text{Np}_{0.016}\text{Am}_{0.016}\text{Pu}_{0.3}\text{U}_{0.668})\text{O}_y$	1.98
	MOX	$(\text{Pu}_{0.3}\text{U}_{0.7})\text{O}_y$	1.98
No.2-2	MA-MOX	$(\text{Np}_{0.016}\text{Am}_{0.016}\text{Pu}_{0.3}\text{U}_{0.668})\text{O}_y$	1.96
	MOX	$(\text{Pu}_{0.3}\text{U}_{0.7})\text{O}_y$	1.96

Held for 24h at 430W/cm

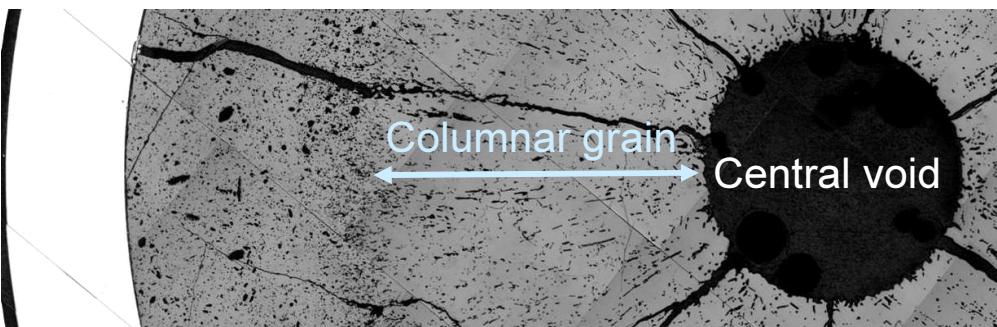


PIE Results

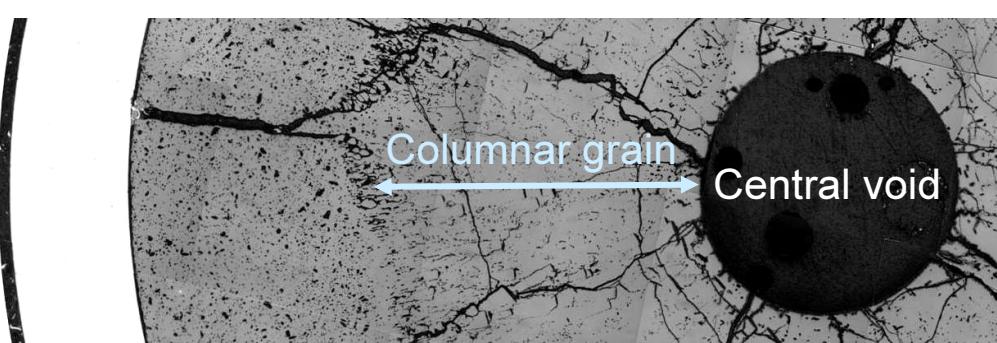
Microstructure Change



No.1-1 MA-MOX, O/M=1.98, at 427W/cm for **10 min**



No.2-1 MA-MOX, O/M=1.98, at 432W/cm for **24h**



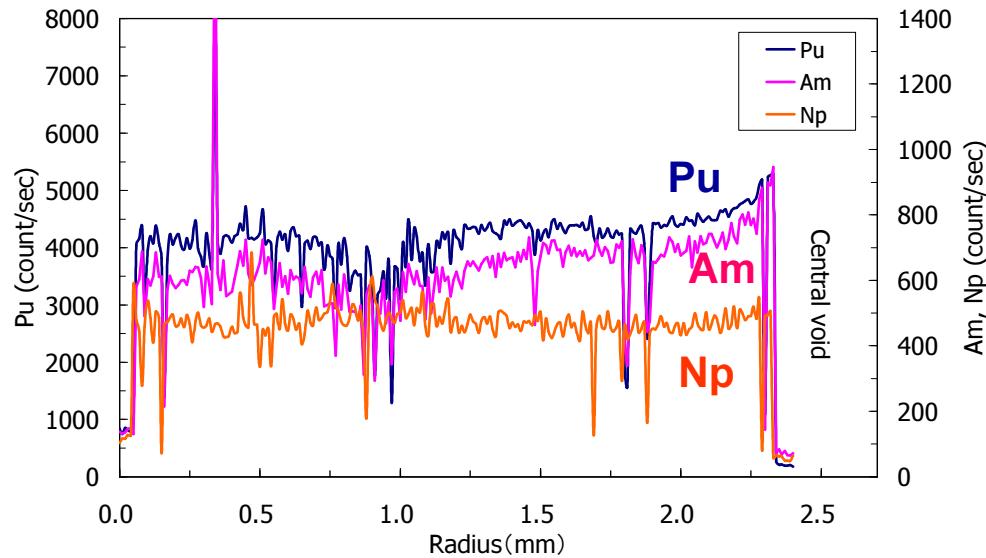
No.2-2 MA-MOX, O/M=1.96, at 429W/cm for **24h**

Observation results

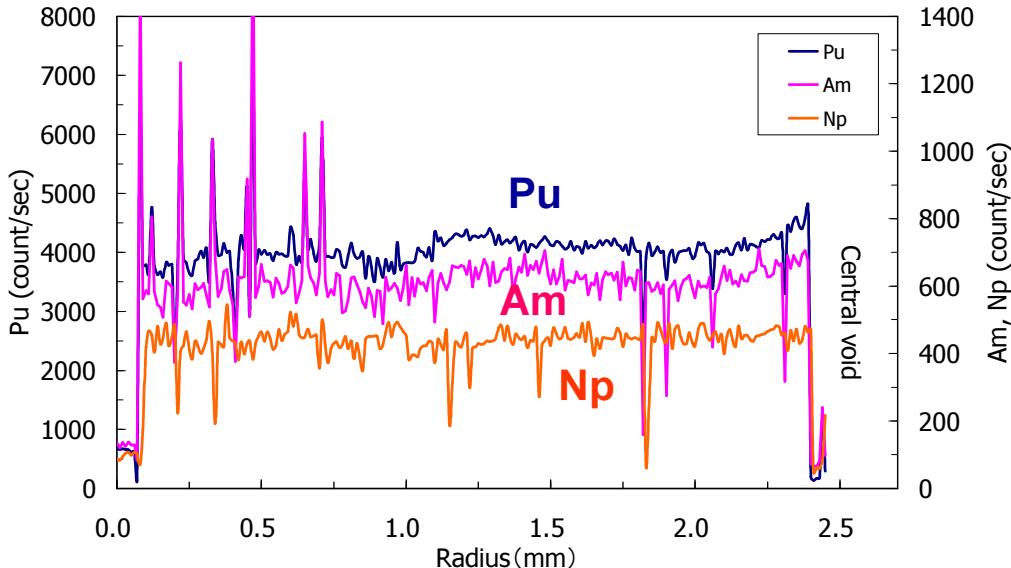
1. The heat rate of the fuels attained about 430W/cm.
2. The pellets were unmelted.
3. Pores migrated to the center.
4. Columnar grain and central void were observed

PIE Results

Actinide Redistribution



No.2-1 MA-MOX, $O/M=1.98$, at 432W/cm for 24h



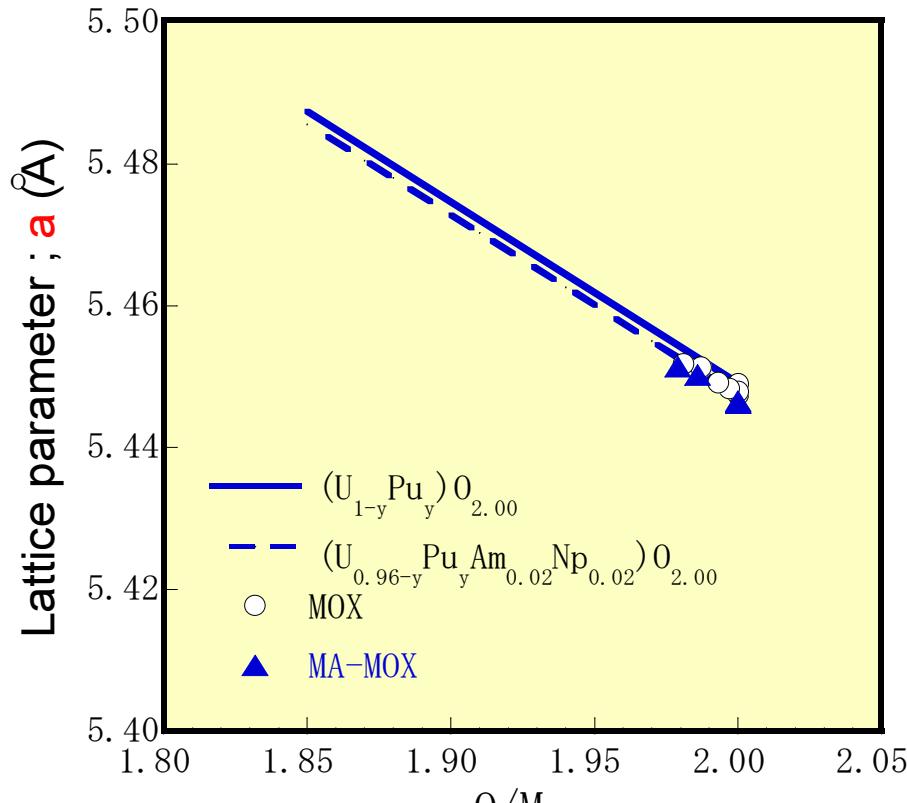
No.2-2 MA-MOX, $O/M=1.96$, at 429W/cm for 24h

Observation results

1. The content of Pu and Am increased at pellet center.
2. The increment of Pu and Am decreased with decreasing O/M.
3. The contents of Np and U were flat.

Properties of fuel pellets (1/4)

Lattice Parameter



Lattice Parameter vs. O/M ratio

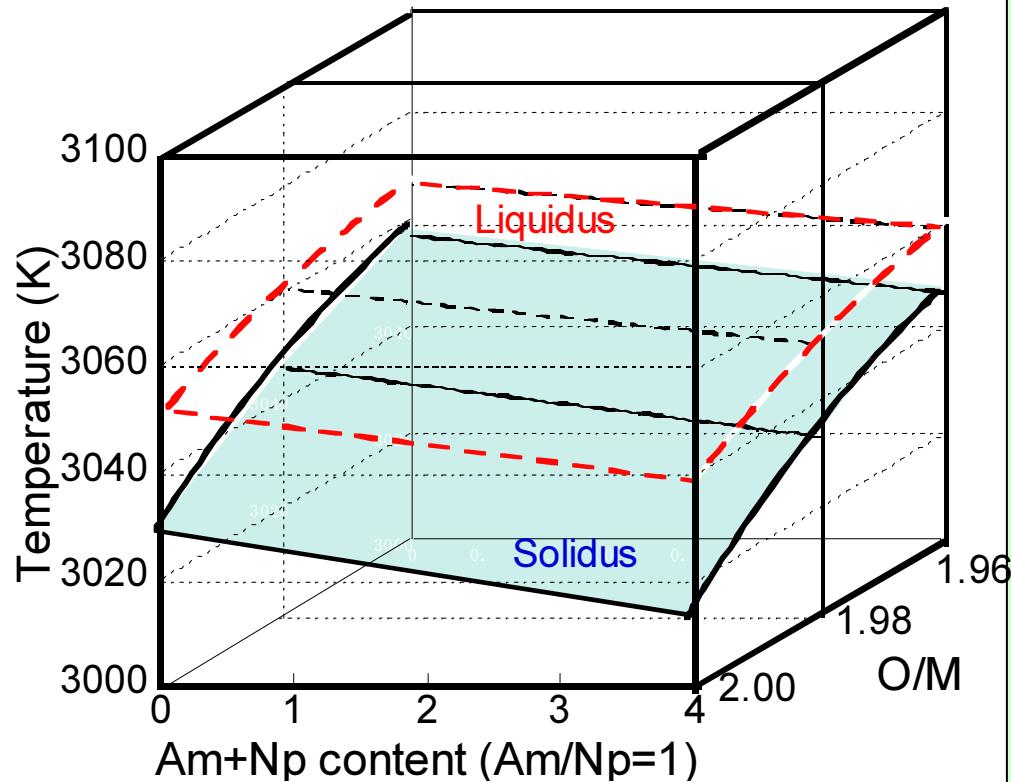
$$a = 4 / \sqrt{3} (r_c(1 + 0.112x) + r_a)$$

$$r_c = (r_U(1 - z - y' - y'') + r_{Pu}z + r_{Am}y' + r_{Np}y'')$$

Results

1. The model to represent the lattice parameter was derived.
2. MA content slightly caused the lattice parameters to decrease.
3. The difference of theoretical density is 0.01-0.02g/cm³.

10



Variation of Solidus and Liquidus Temp.

M.Kato, et al., ICAPP '09

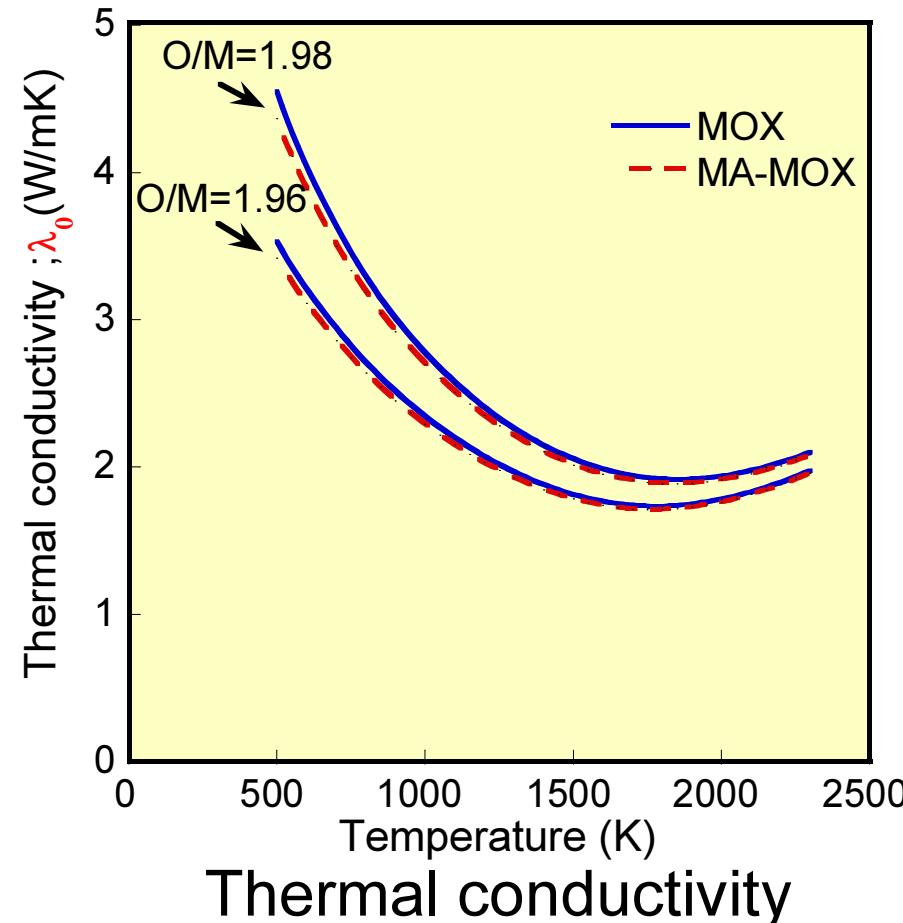
Results

1. The data were measured and analyzed by the ideal solid solution model.
2. MA content caused to decrease by 2-3K /%MA.
3. The solidus temperature of MA-MOX is over 3000K.

Properties of fuel pellets (3/4)

Plutonium Fuel Development Facility

Thermal conductivity



Results

1. The data were measured as functions of MA content, density, O/M and temperature.
2. MA content caused to decrease slightly in temperatures of less than 1000K.

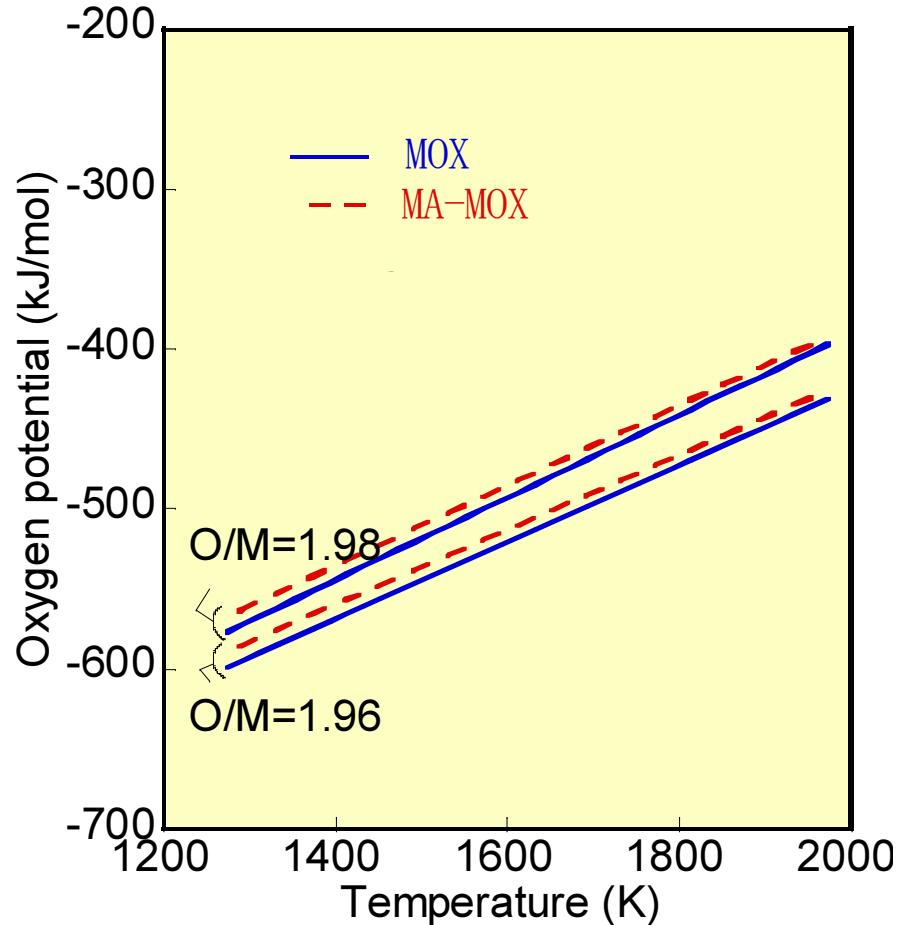
$$\lambda_0 = \frac{1}{(2.713x + 3.583 \times 10^{-1} \times z_1 + 6.317 \times 10^{-2} \times z_2 + 1.595 \times 10^{-2}) + (-2.625x + 2.493) \times 10^{-4} T} + \frac{1.541 \times 10^{11}}{T^{5/2}} \exp\left(\frac{1.522 \times 10^4}{T}\right)$$

z_1 : Am content
 z_2 : Np content
x: Deviation x in MO_{2-x}

Properties of fuel pellets (4/4)

Plutonium Fuel Development Facility

Oxygen potential



Results

1. The data were measured by gas equilibrium method.
2. MA content caused the oxygen potential to increase slightly.

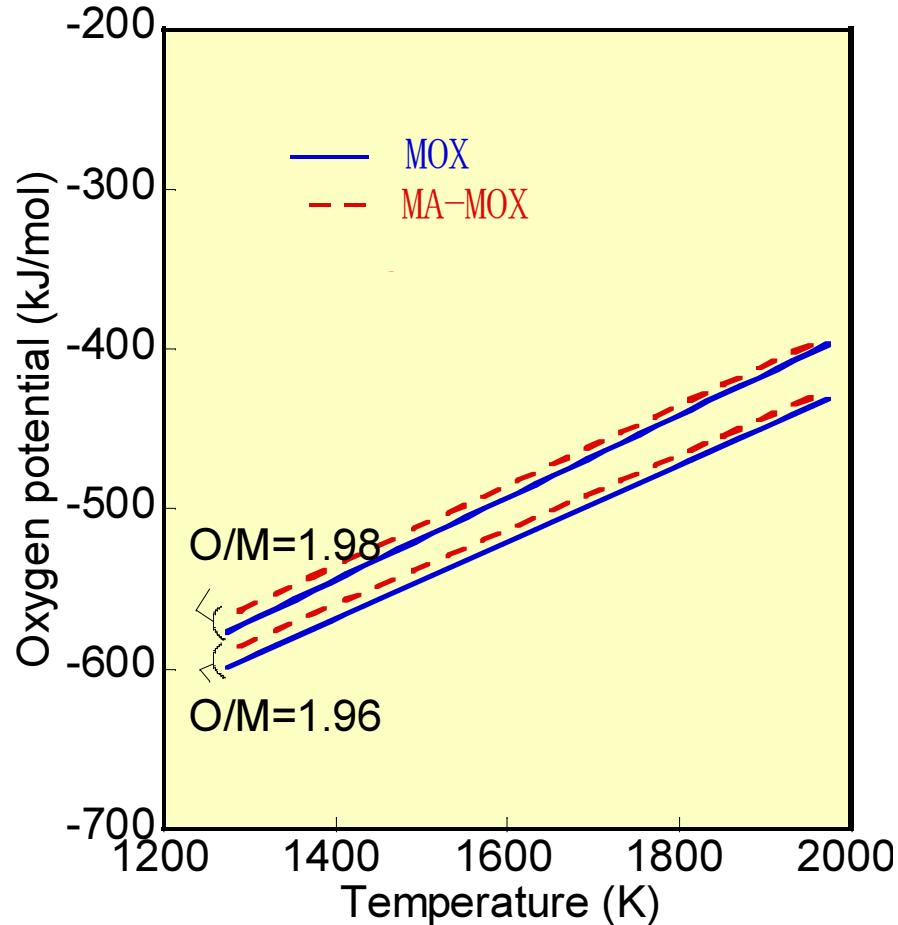
Oxygen potential

M.Kato, et al., J.N.M. 385 (2009) 419

Properties of fuel pellets (4/4)

Plutonium Fuel Development Facility

Oxygen potential



Oxygen potential

Results

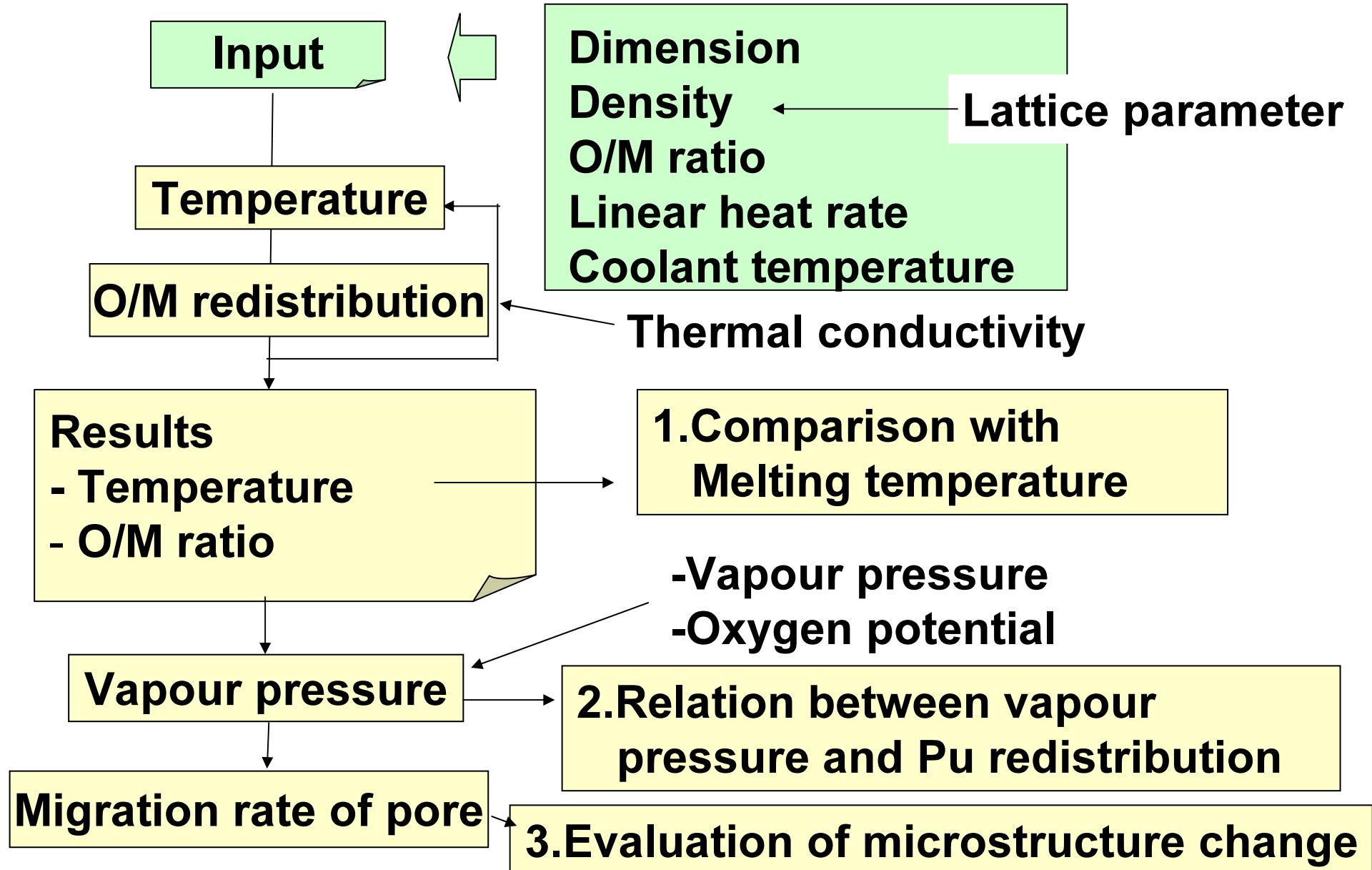
1. The data were measured by gas equilibrium method.
2. MA content caused the oxygen potential to increase slightly.

Summary

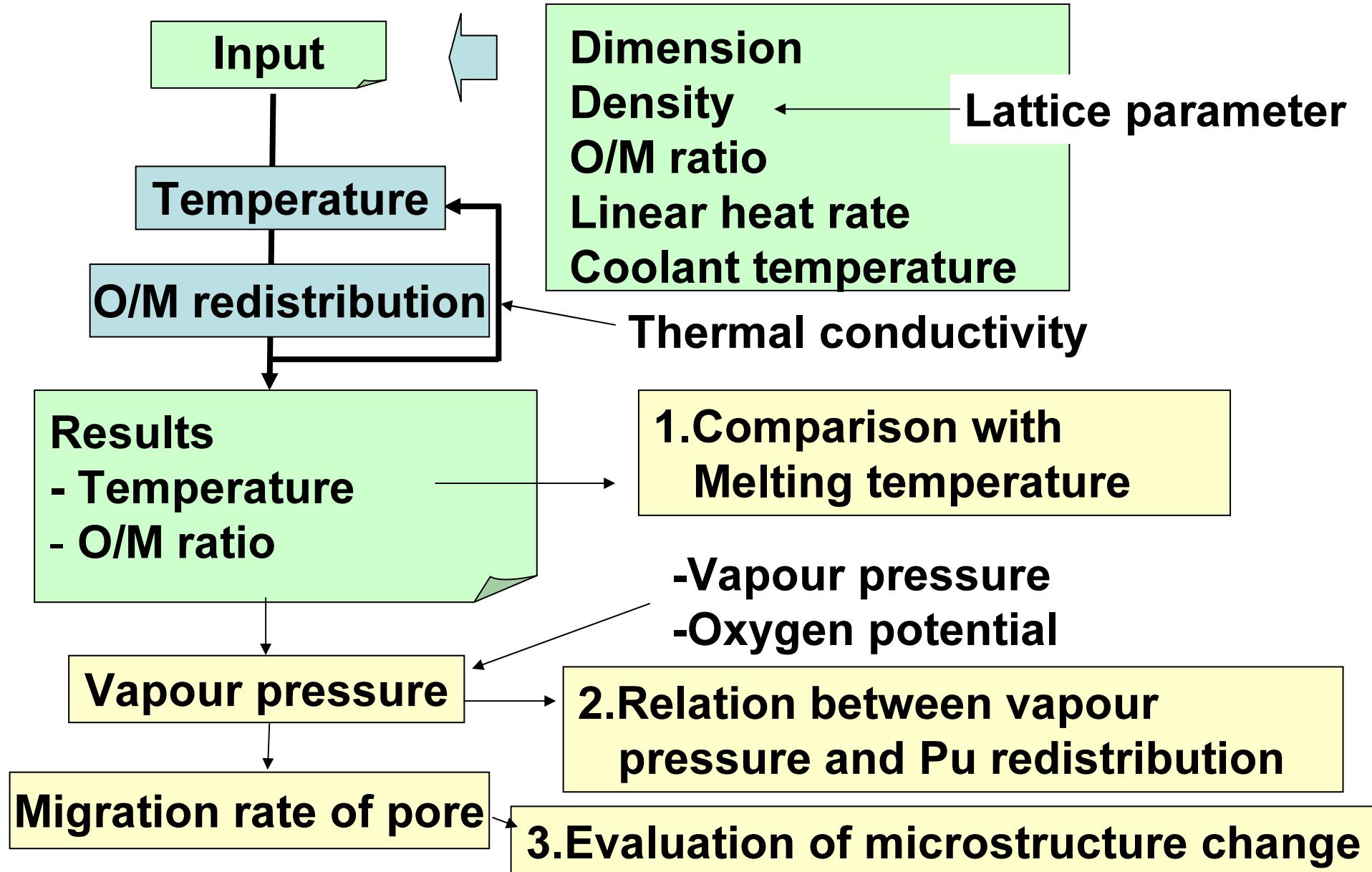
The effect of MA addition on the properties is negligibly small in the operation temperature range of FR fuels

Analysis of irradiation behaviour

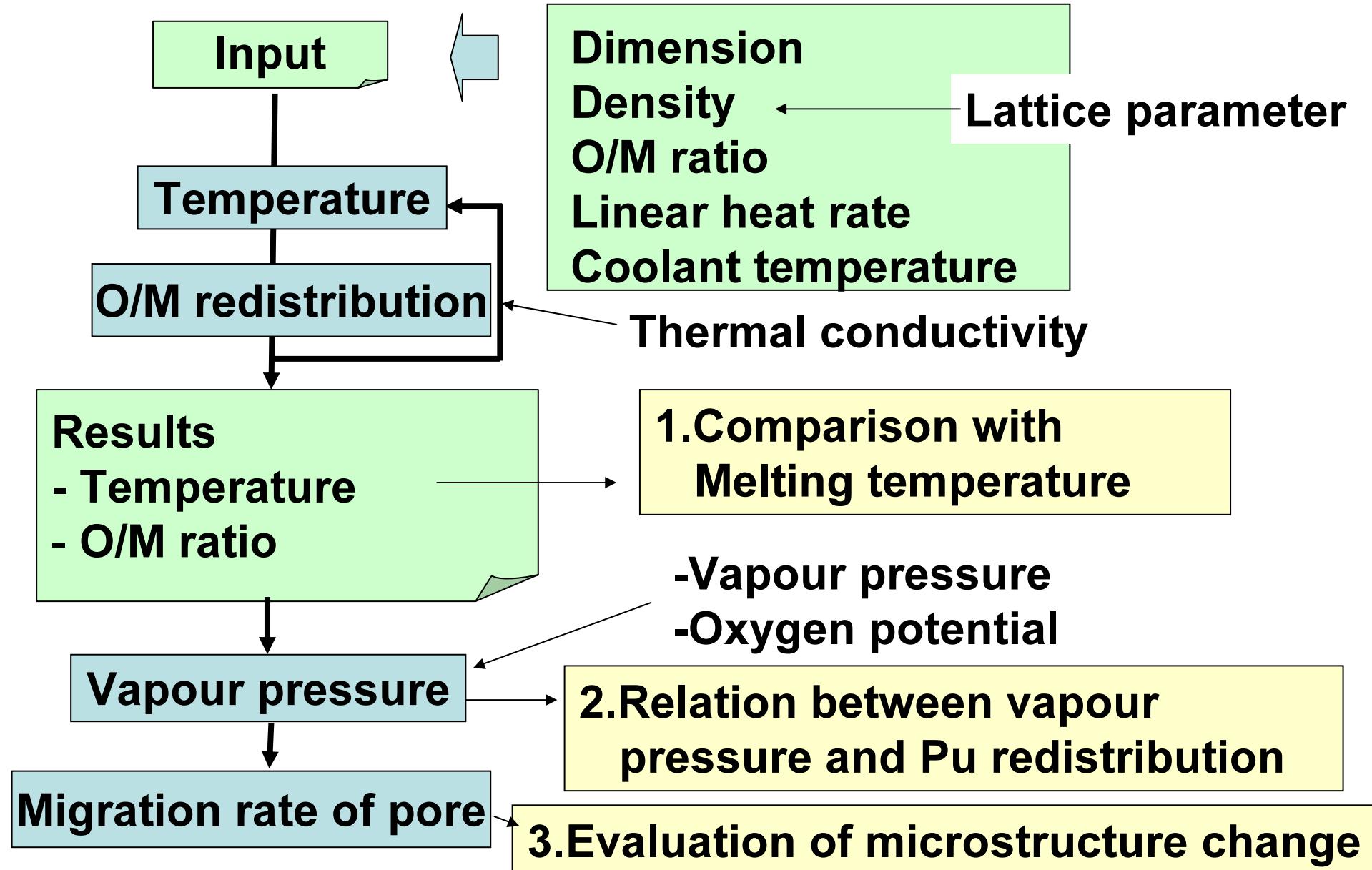
Analysis Procedure



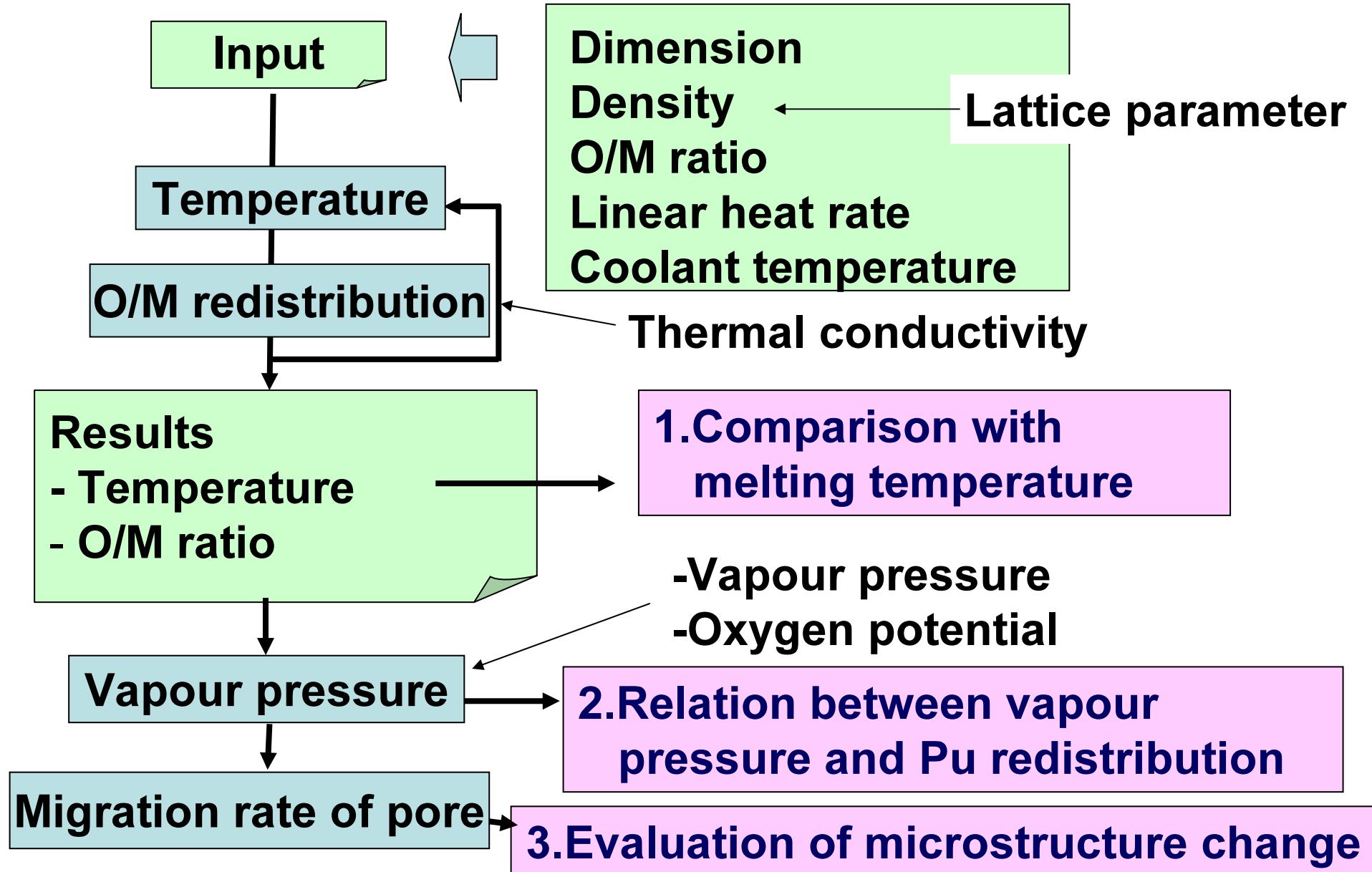
Analysis Procedure



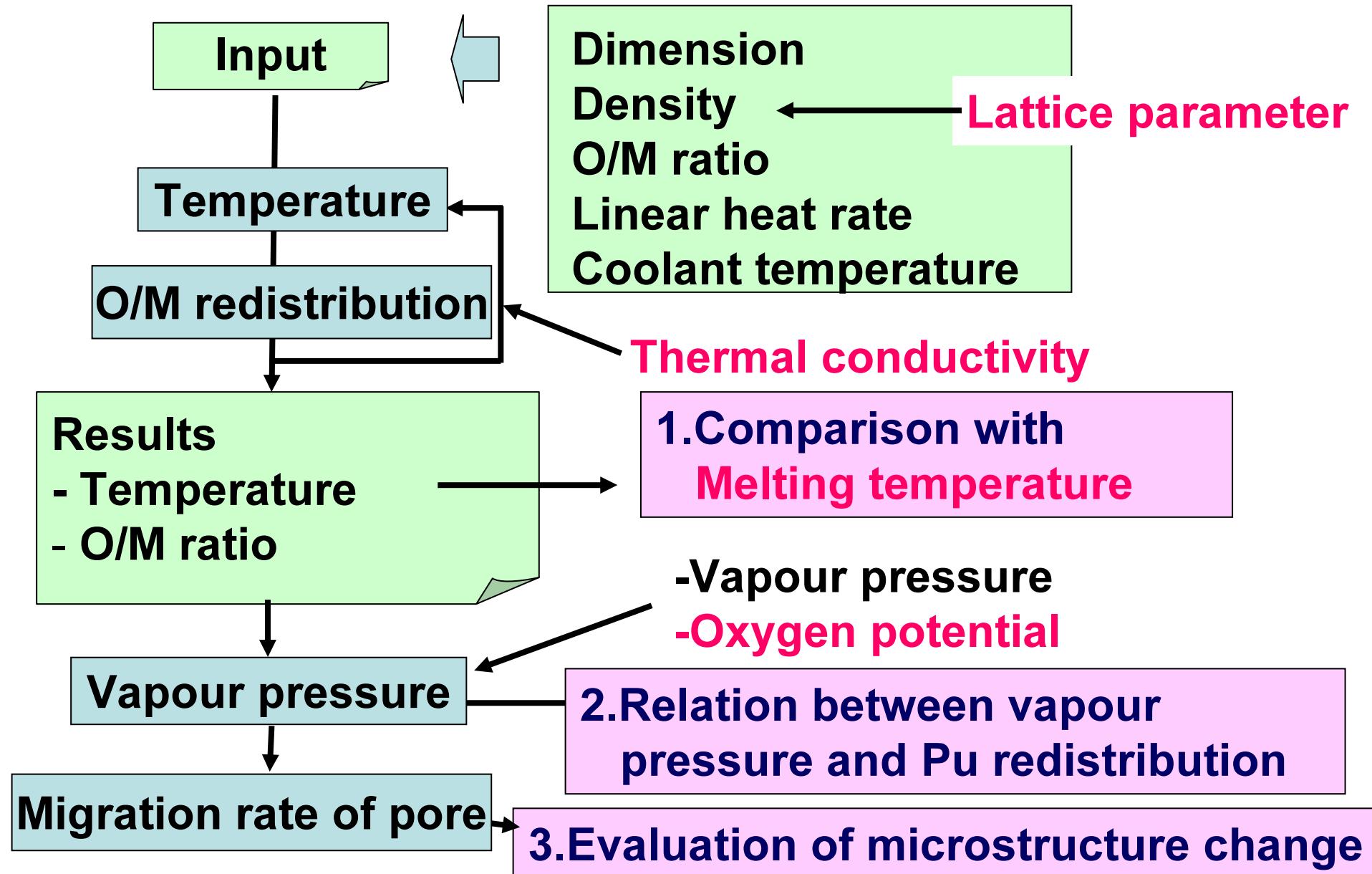
Analysis Procedure



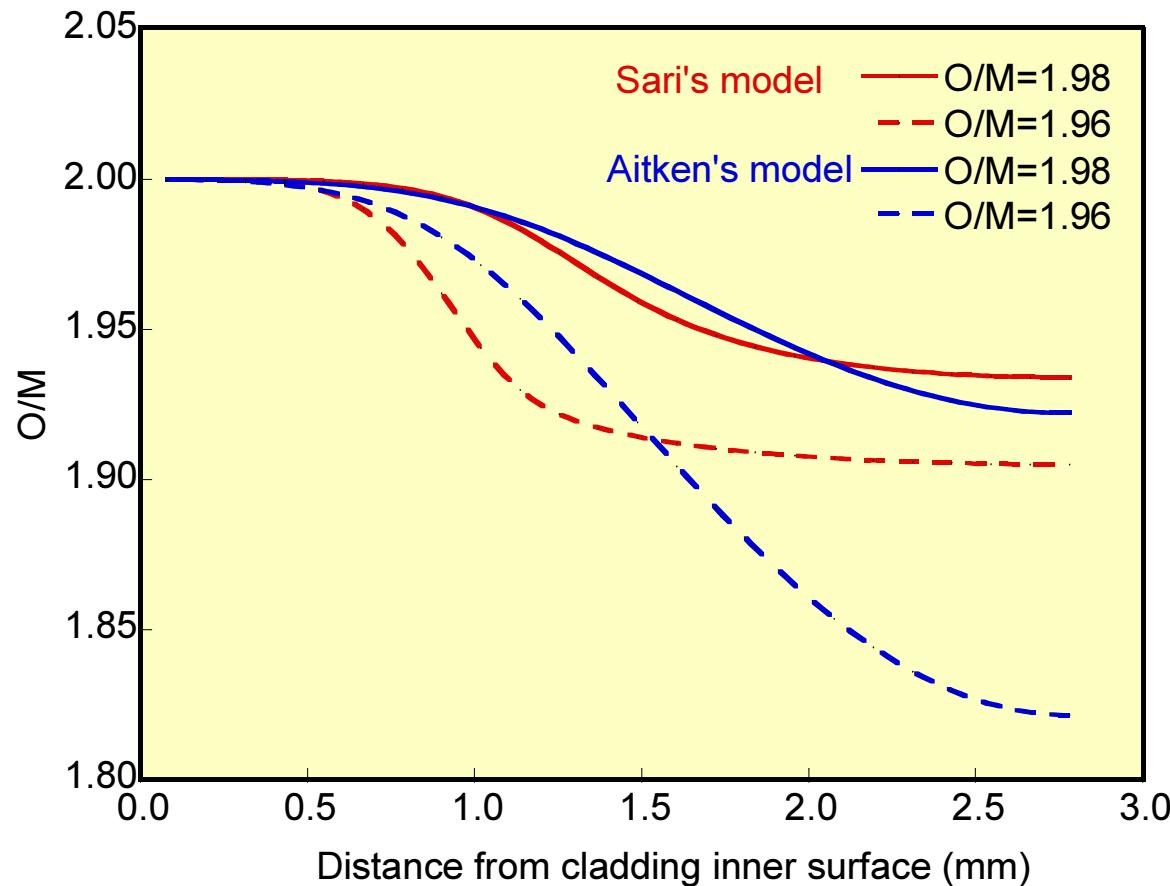
Analysis Procedure



Analysis Procedure



O/M Redistribution

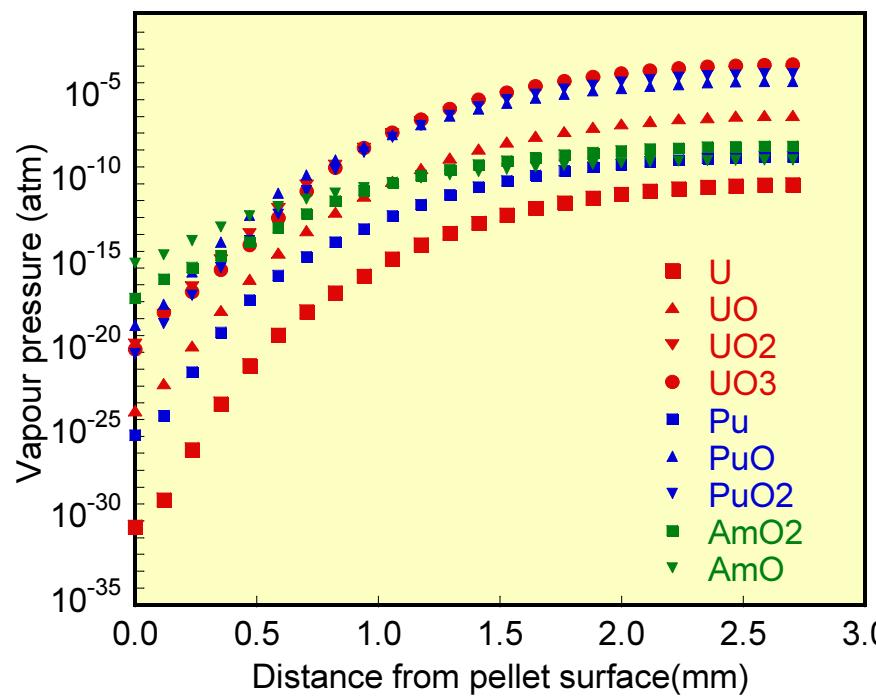


O/M ratio distribution in the radial direction

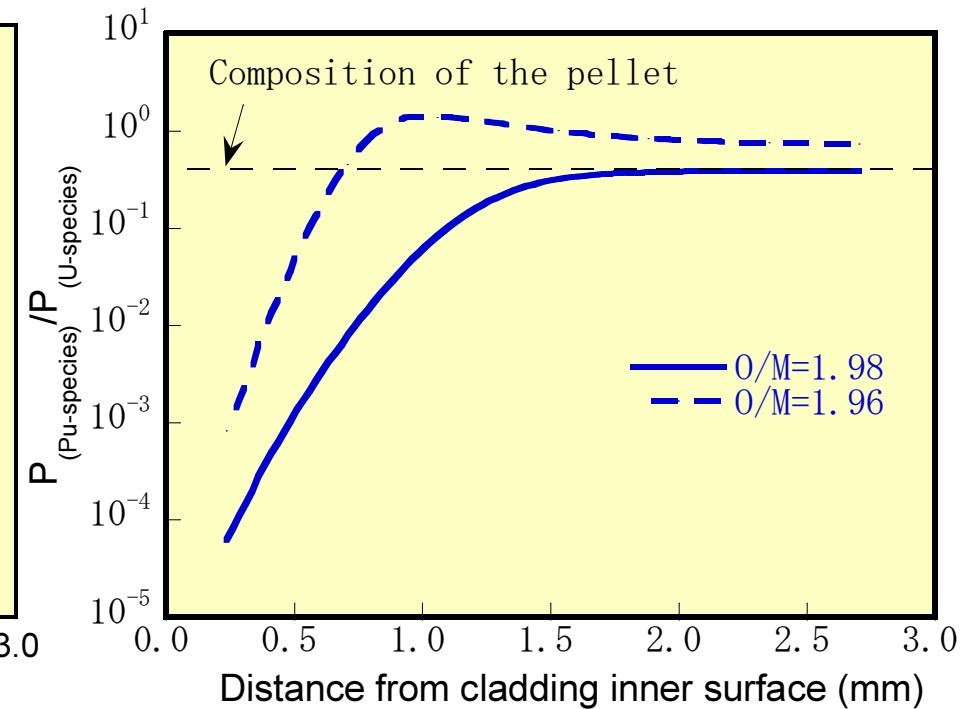
Results

1. Both models gave almost the same result in high O/M pellets.
2. The results of low O/M pellets differed according to models.
3. Sari's model was employed.

Evaluation of vapour pressure



Variation of vapor pressure

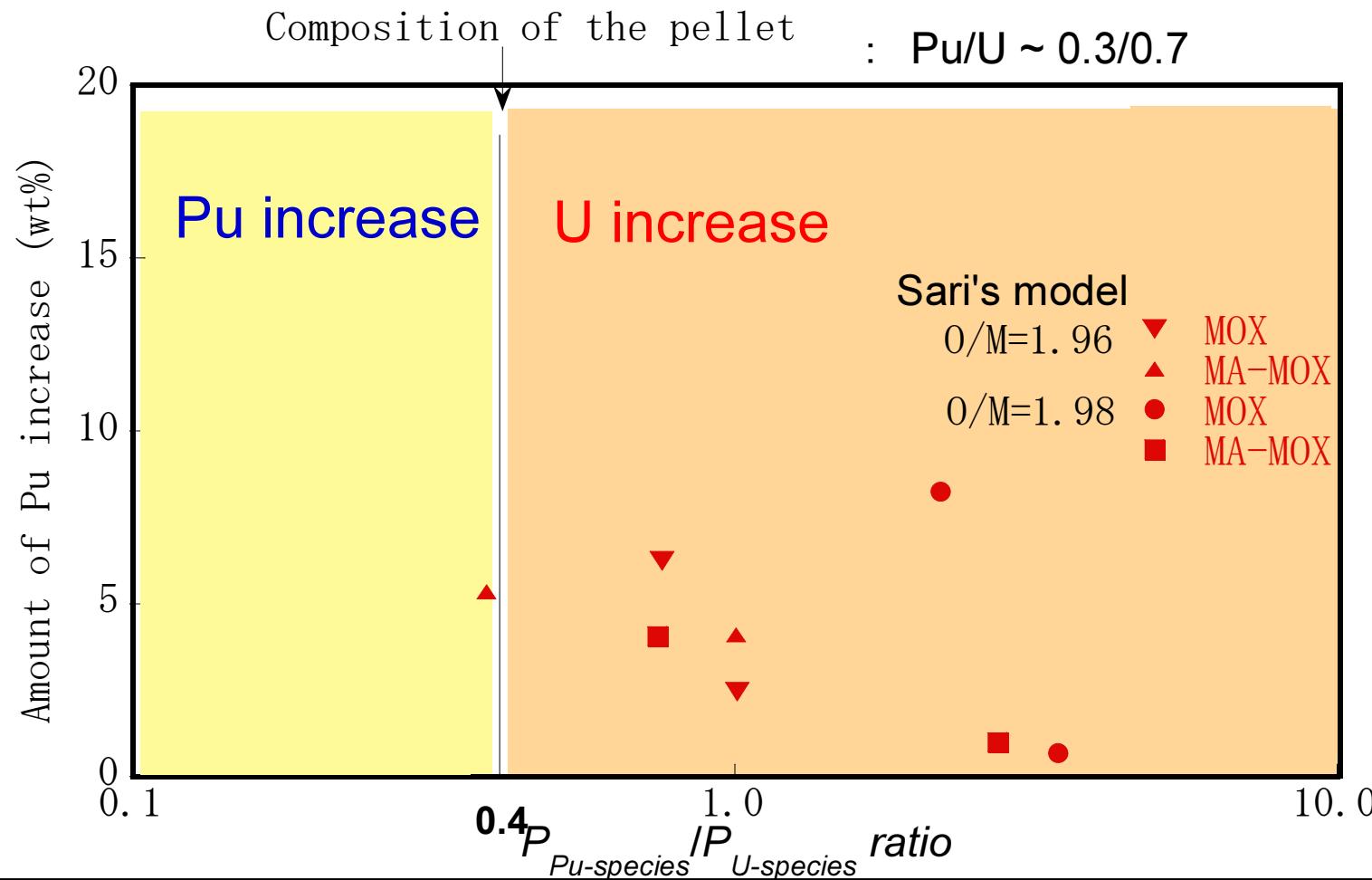


Variation of Pu/U- species

Result

1. Variation of vapor pressure ratio of Pu/U-species was evaluated using Rand –Markin model.

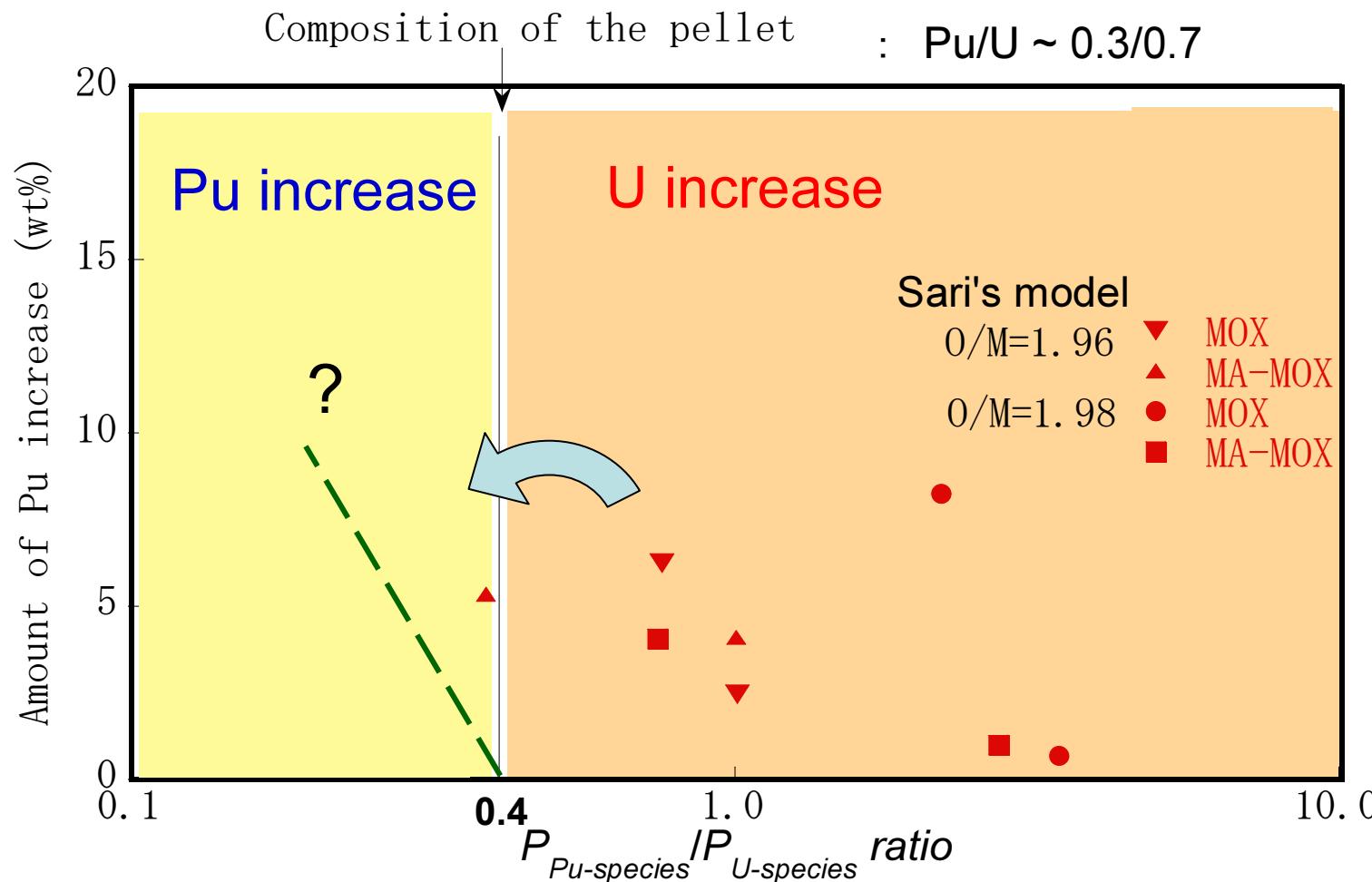
Evaluation of Pu redistribution



Result

1. Calculation result shows that U content increases at pellet center.

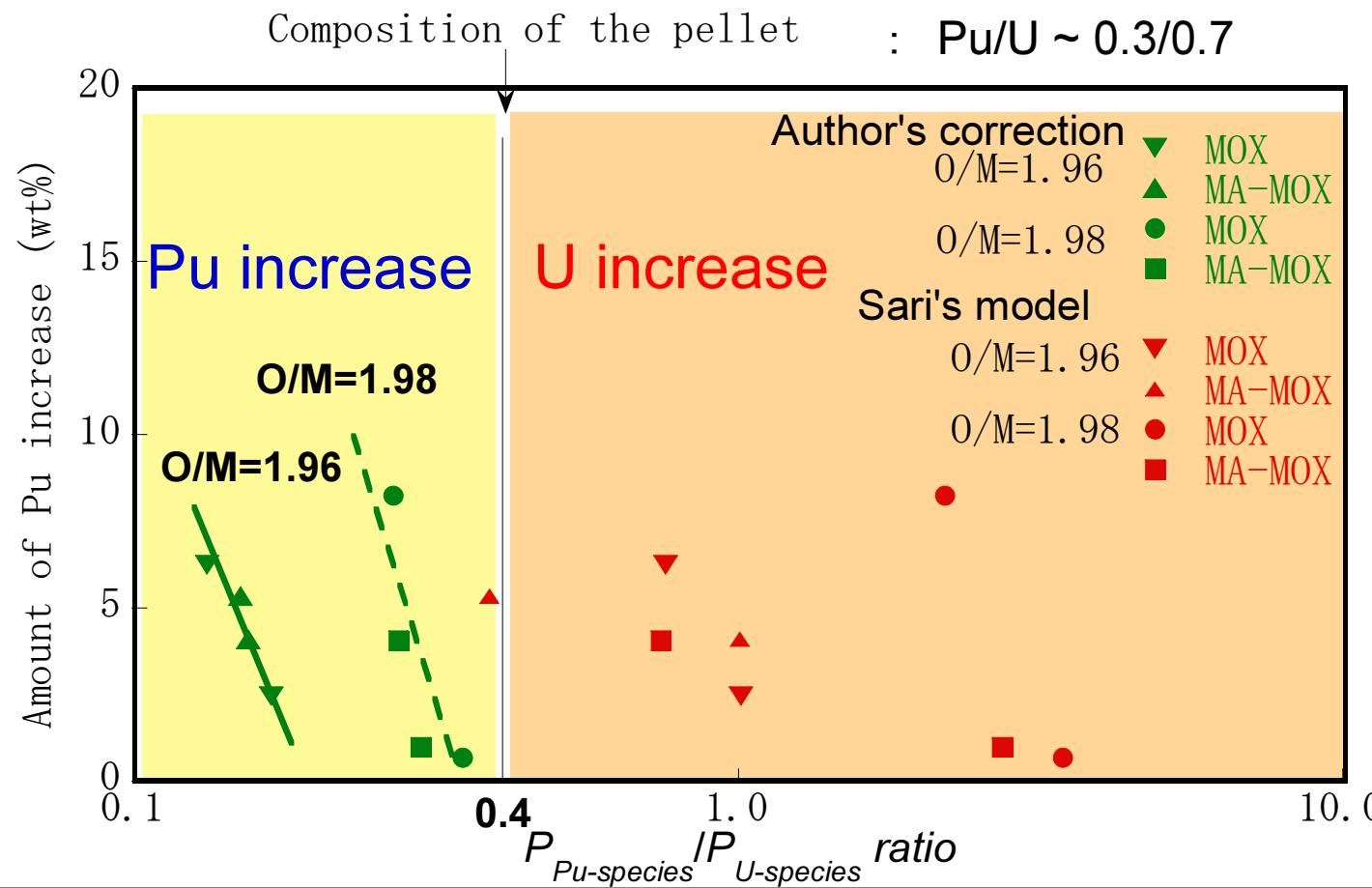
Evaluation of Pu redistribution



Expectation

Increment of Pu should be increased with decreasing the $P_{\text{Pu-species}}/P_{\text{U-species}}$.

Evaluation of Pu redistribution



Results

1. Calculation results show that Pu content increase at pellet centre.
2. Two lines were obtained depending on O/M ratio.

Reviewing of the model for O/M redistribution



Sari's model for O/M redistribution

$$\ln\left(\frac{x_1}{x_2}\right) = \frac{Q^*}{R} \left(\frac{1}{T_2} - \frac{1}{T_1} \right)$$

$$Q^* = -9.45 \times 10^5 + 5.66 \times 10^5 V_{Pu} - 8.5 \times 10^4 V_{Pu}^2$$

X: deviation in $(U,Pu)O_{2-x}$

T: temperature

R : gas constant,

Q* : the molar effective heat of transport

V_{Pu} : Pu valence

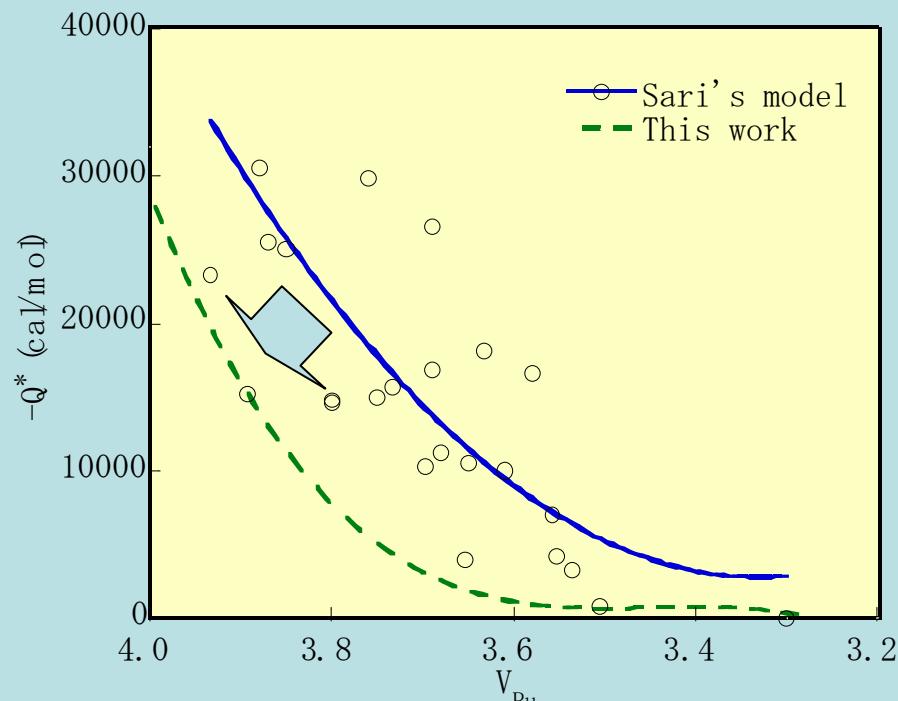
Evaluation of equation for Q*

Calculation of O/M Redistribution, temperature and vapour pressure

Evaluation of the relationship between the $P_{\text{Pu-species}}/P_{\text{U-species}}$ and the Pu increase

Corrected Eq.

$$Q^* = -7.01 \times 10^6 + 6.1012 \times 10^6 V_{Pu} - 1.7705 \times 10^6 V_{Pu}^2 - 1.7122 \times 10^5 V_{Pu}^3$$



Reviewing of the model for O/M redistribution

Sari's model for O/M redistribution

$$\ln\left(\frac{x_1}{x_2}\right) = \frac{Q^*}{R} \left(\frac{1}{T_2} - \frac{1}{T_1} \right)$$

$$Q^* = -9.45 \times 10^5 + 5.66 \times 10^5 V_{Pu} - 8.5 \times 10^4 V_{Pu}^2$$

Evaluation of equation for Q^*

Calculation of O/M Redistribution, temperature and vapour pressure

Evaluation of the relationship between the $P_{\text{Pu-species}}/P_{\text{U-species}}$ and the Pu increase

Corrected Eq.

$$Q^* = -7.01 \times 10^6 + 6.1012 \times 10^6 V_{Pu} - 1.7705 \times 10^6 V_{Pu}^2 - 1.7122 \times 10^5 V_{Pu}^3$$

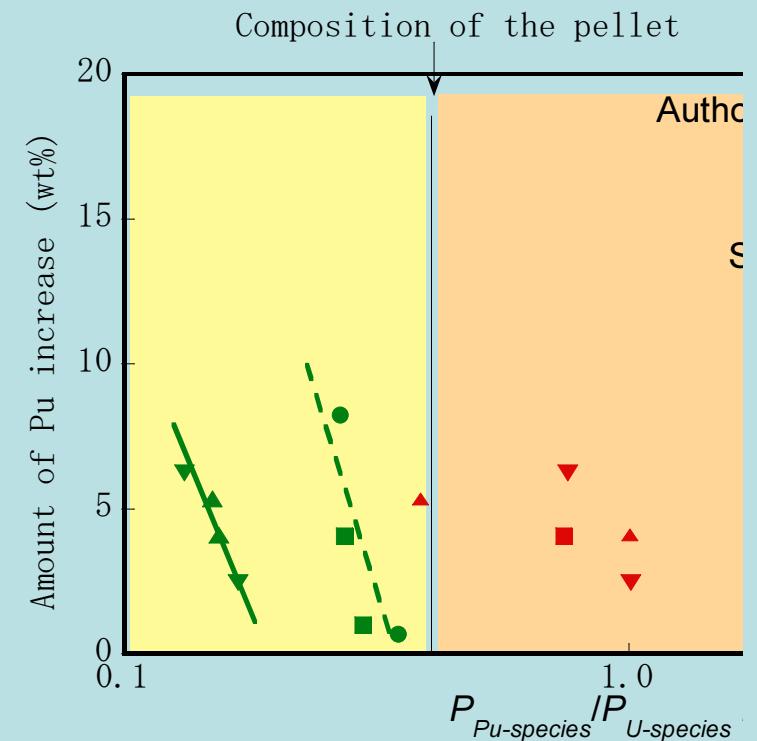
X: deviation in $(\text{U}, \text{Pu})\text{O}_{2-x}$

T: temperature

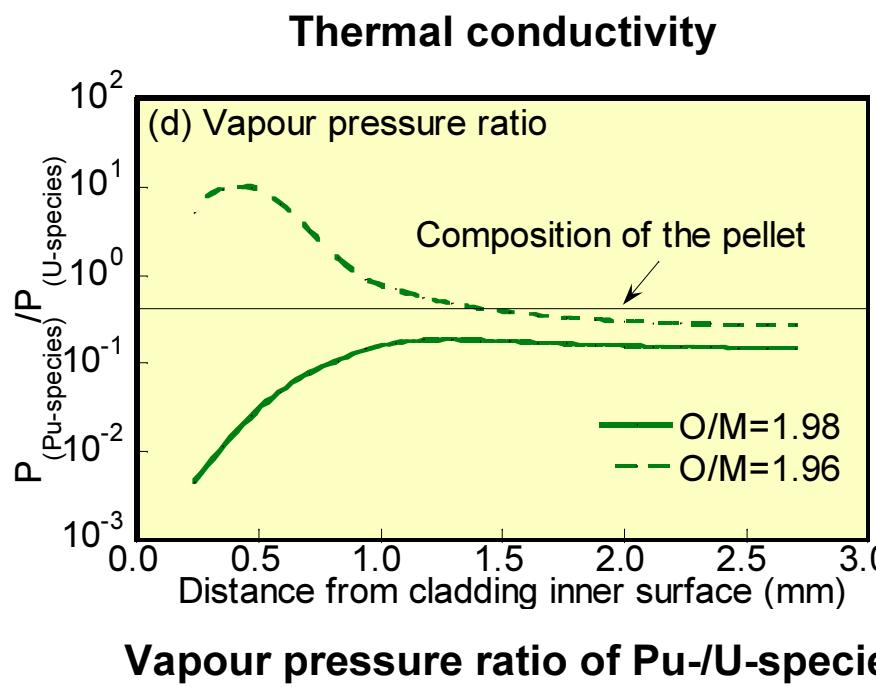
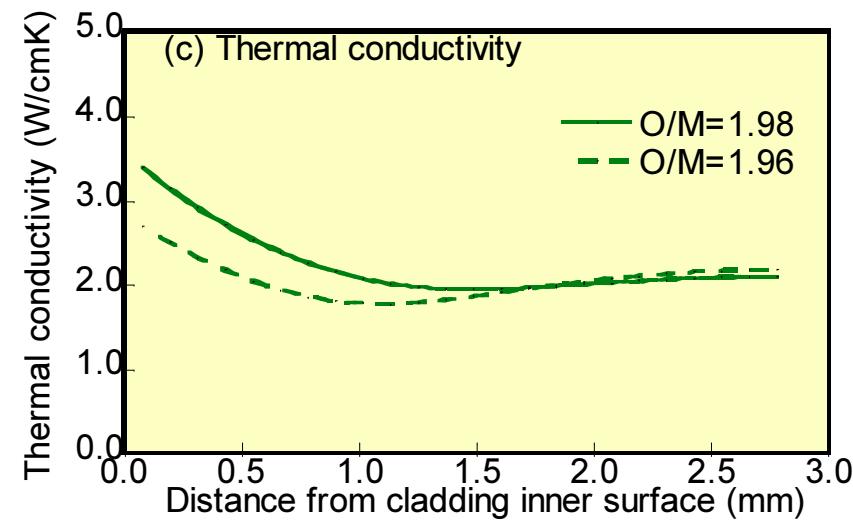
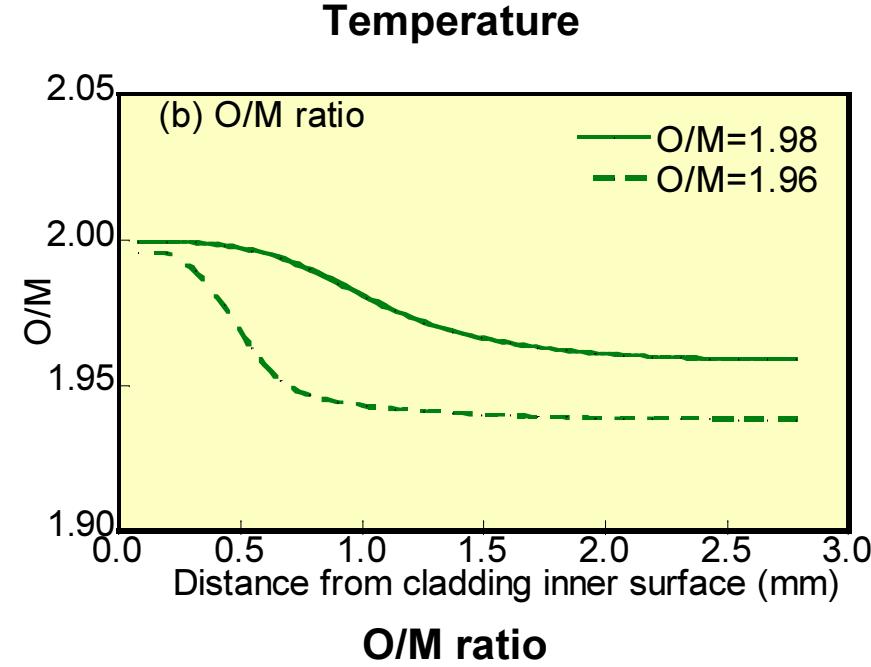
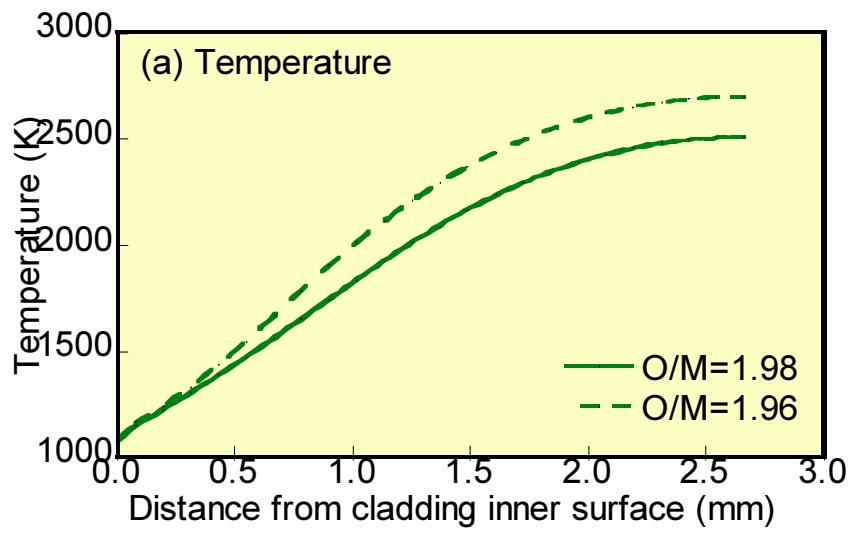
R : gas constant,

Q^* : the molar effective heat of transport

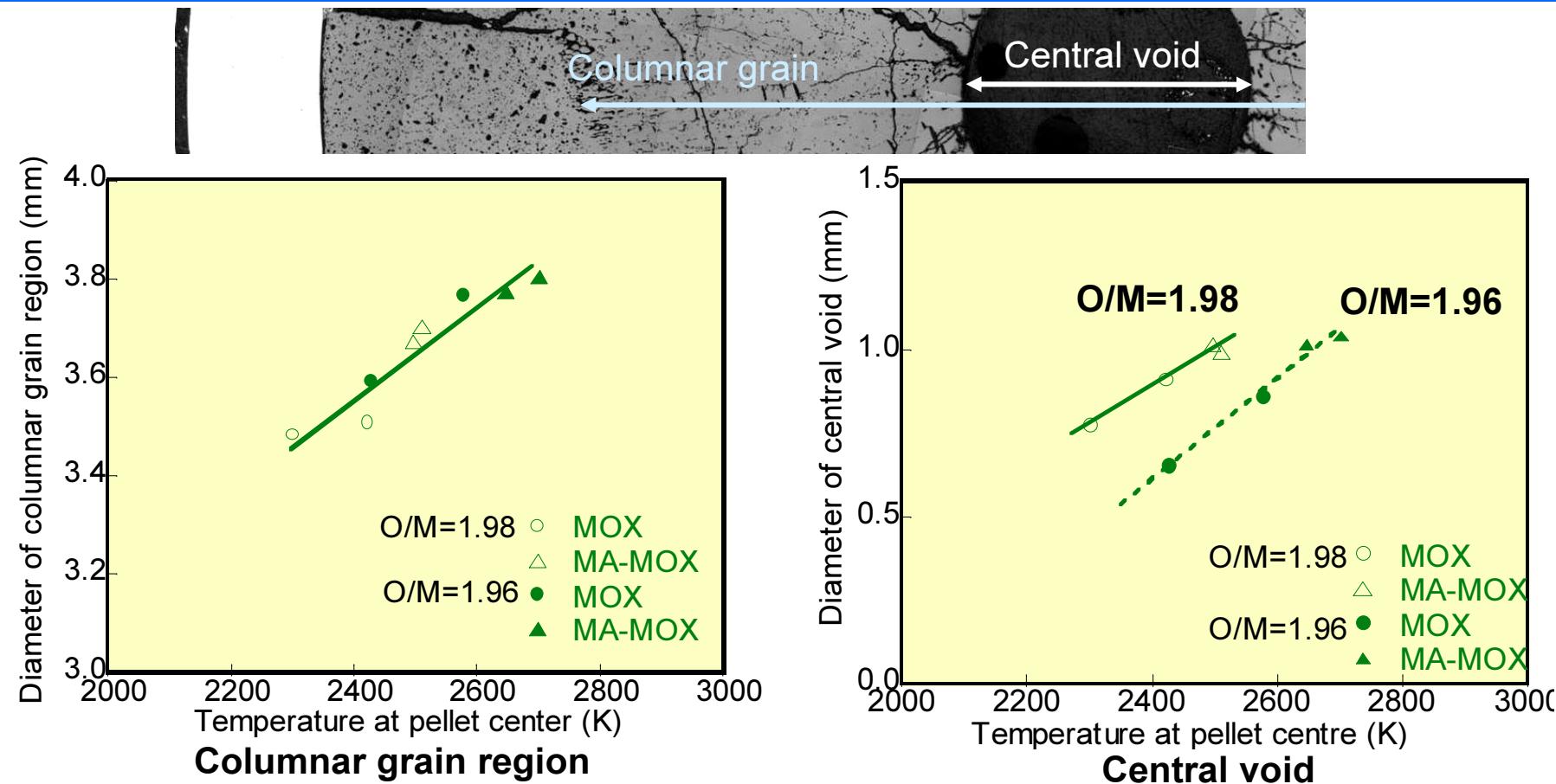
V_{Pu} : Pu valence



Calculation results in MA-MOX pellets



Microstructure change

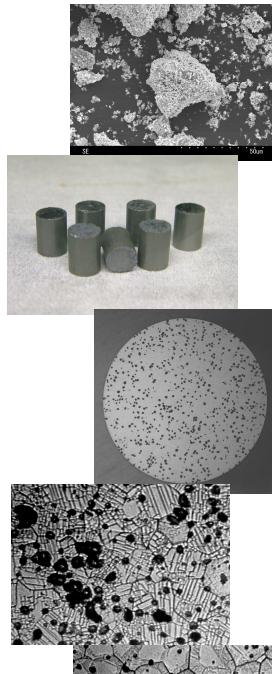


Results

1. The both region grew with temperature.
2. The central void of high O/M pellet is larger than that of low O/M pellets.

Summary

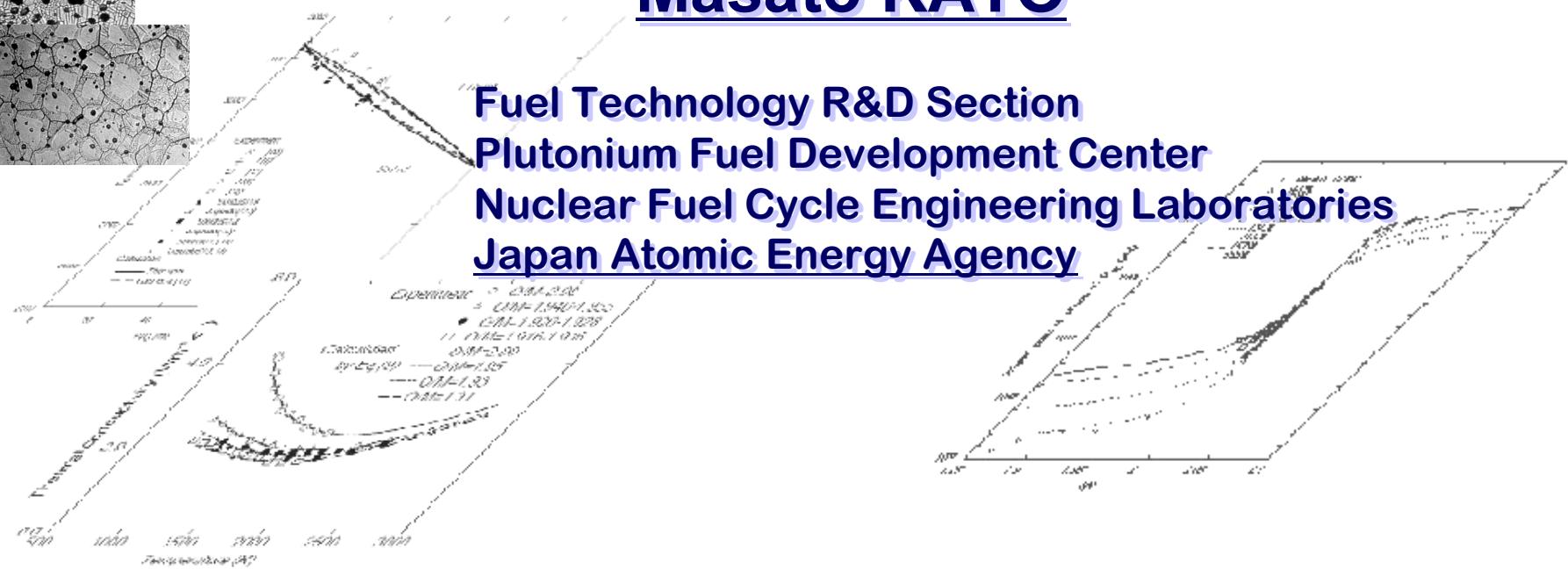
- 1. The physical properties of the Np/Am-MOX were evaluated, and the effect of Np/Am addition was negligibly small.**
- 2. The relation between the Pu redistribution and the vapor pressure was described by correcting Sari's model for O/M redistribution.**
- 3. The low O/M pellet attained higher temperature, however, the diameter of the central void was small as compared with the high O/M pellet.**
- 4. It is needed to measure experimental data and to derive advanced models for describing irradiation behavior of low O/M fuel.**



Development of Np and Am bearing MOX fuels for Japan sodium cooled fast reactors

Masato KATO

Fuel Technology R&D Section
Plutonium Fuel Development Center
Nuclear Fuel Cycle Engineering Laboratories
Japan Atomic Energy Agency



Japan Atomic Energy Agency