

# Neutronics Code Development at Argonne National Laboratory

2009 International Conference on Fast Reactors and Related Fuel Cycles

December 7-11, 2009

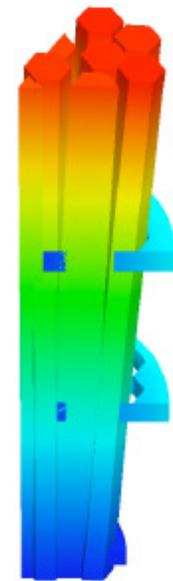
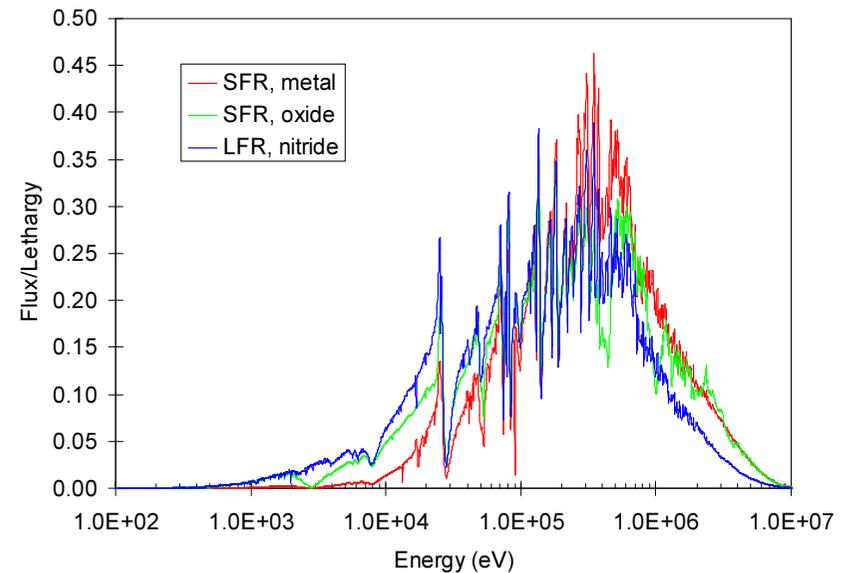
Kyoto, Japan

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Argonne National Laboratory

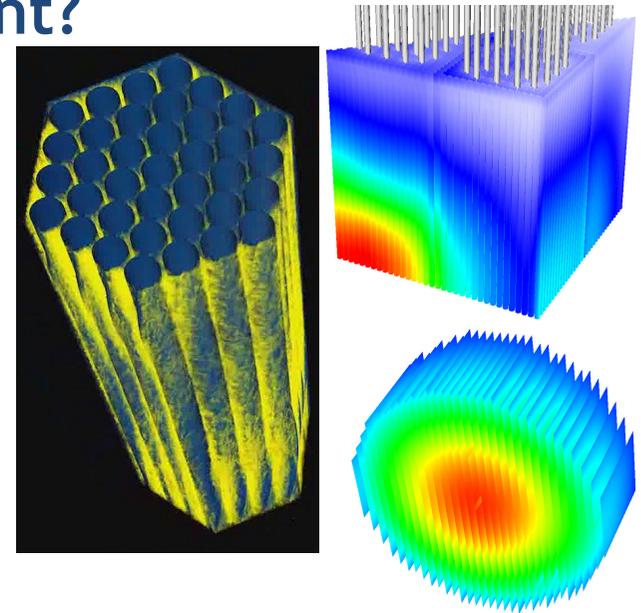
# Fast Reactor Modeling and Simulation Challenges

- Detailed energy modeling
  - Lack of a  $1/E$  spectrum as a basis for resonance absorption calculation
  - Inelastic,  $(n,2n)$ , anisotropic scattering are of great importance
- Long neutron mean free paths
  - Neutron leakage is enhanced, 25% at moderate sizes
  - Local reactivity effects impact entire core
- High leakage and heterogeneous core configurations challenge design methods
  - Transport effects are magnified
  - Spectral and directional transitions at the core and reflector interface are hard to model
  - Core reactivity is sensitive to minor geometric changes
    - Integration with thermal-hydraulics and structural mechanics analyses to account for reactivity feedbacks due to geometry deformation accurately



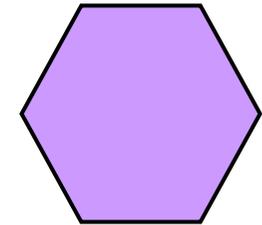
# High Fidelity Modeling, What is the point?

- The existing approach: Homogenized assembly
    - Vast reduction of space-angle-energy dofs
    - Focused on producing the global gradient
    - Reconstruct: local and global solution must be merged
  - Explicit geometry core calculations?
    - $>10^{10}$  degrees of freedom requires some parallelism
    - Few large problems have been attempted
  - Can we improve the existing calculation accuracy?
    - Not really concerned about depletion in short term
      - Errors in cross section data? Multi-group processing?
    - Material loading uncertainties
      - Are we solving a contrived problem; i.e. predicting the weather?
      - Not the case for ZPR and other similar benchmarks. Production reactors?
  - Safety analysis was identified as one area of weakness that can be improved
    - Radial thermal expansion is generally treated poorly in neutronics
    - Above core mixing (thermal induced stress) is poor in CFD
    - Modeling of seismic event impacts on core and plant?
- **Considerable development lead time before significant results can be achieved**

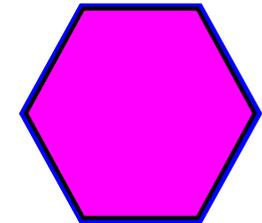


# Status of UNIC Code Development

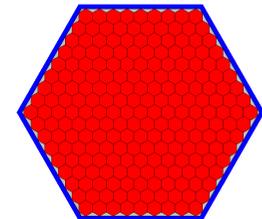
- “Allow the existing reactor analysis work to transition smoothly from assembly level homogenization to less crude homogenization and eventually to fully heterogeneous descriptions”
  - Diffusion theory structured geometry solver (NODAL)
    - Reproduce nodal diffusion capability in existing tools
    - Can be extended to 1<sup>st</sup> order  $S_N$  or VARIANT
  - Even-parity transport equation with spherical harmonics (PN2ND)
    - Immediate use on problems with significant homogenization
  - Method of Characteristics (MOCFE)
    - Long term deployment and use on problems without homogenization
  - Even-parity transport equation with discrete ordinate (SN2ND)
    - Modeling transition region between PN2ND and MOCFE solvers
    - Still has the second-order limitations (voids?)
    - We still prefer to homogenize similar regions
- MC<sup>2</sup>-3 module for in-line multi-group cross section generation
  - Hyperfine (~400,000) group transport capability for homogeneous mixture and 1-D slab and cylindrical geometries. Started 2-D work.



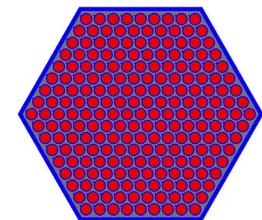
Homogenized  
assembly



Homogenized  
assembly internals



Homogenized  
pin cells

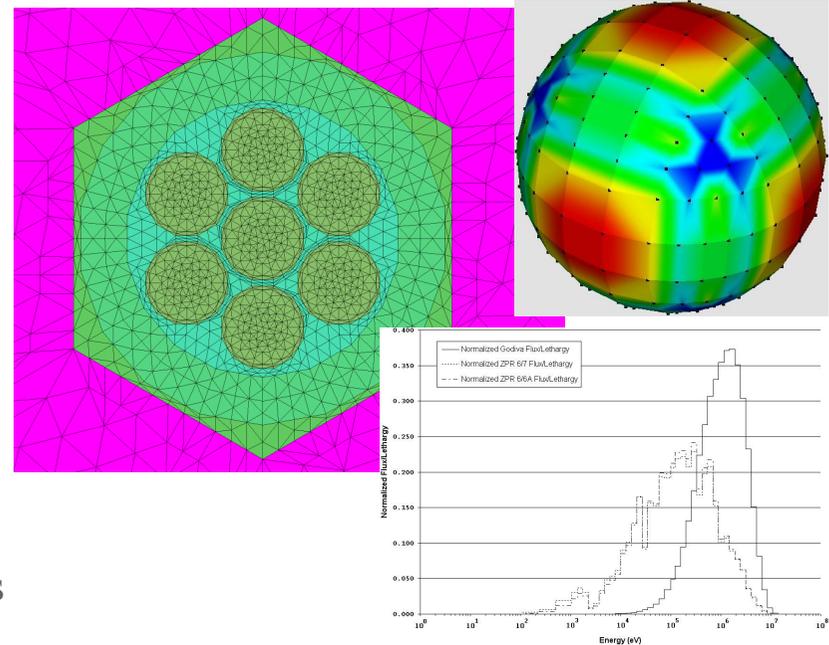


Fully explicit  
assembly



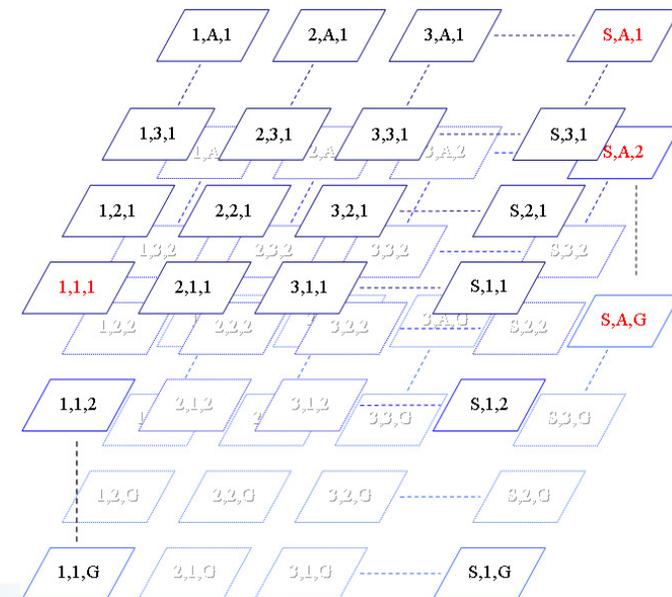
# Parallelism in UNIC

- Novel?
  - Parallel transport studied for well over a decade
    - LANL, Sandia, French, Japanese,...
  - Production tools?
    - Unstructured mesh capabilities?
    - Parallel capabilities?
- Lessons learned at ANL
  - Parallelization in space-angle-energy is necessary
  - There are small, medium, and large parallel machines
    - Spatial domain decomposition is not best for all
    - Angle decomposition for  $S_N$  is generally good up to a limit
    - We have not studied energy decomposition at this point
  - Focused parallelization of L is not necessarily best idea



$$\left\{ \begin{array}{ccc} A_1 & 0 & 0 \\ \vdots & \ddots & 0 \\ W_{1 \rightarrow G} & \cdots & A_G \end{array} \right\} + \left\{ \begin{array}{ccc} W_{1 \rightarrow 1} & \cdots & W_{G \rightarrow 1} \\ 0 & \ddots & \vdots \\ 0 & 0 & W_{G \rightarrow G} \end{array} \right\} \begin{bmatrix} \Psi_1 \\ \vdots \\ \Psi_G \end{bmatrix} = \begin{bmatrix} S_1 \\ \vdots \\ S_G \end{bmatrix}$$

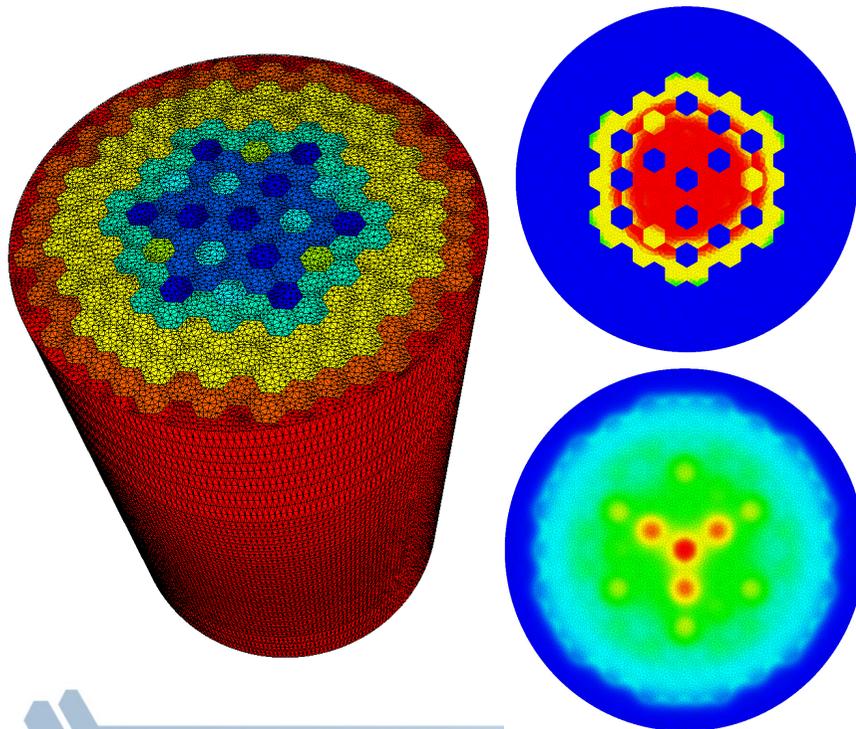
- Capabilities
  - PN2ND: 500-3,000 processors (2007)
  - SN2ND: 1,000-300,000+ processors
  - MOCFE and NODAL: unknown



# Existing Approach (Assembly Homogenization)

- Typical approach used in fast reactor physics today
  - VARIANT residual error is due to  $P_N$  order and source approximation
    - Used 4<sup>th</sup> order source, 8<sup>th</sup> order flux, and 3<sup>rd</sup> order leakage
  - PN2ND residual error is due to  $P_N$  order and spatial mesh refinement
    - Used 109,740 hexahedral elements with 461,219 vertices
  - SN2ND residual error is due to spatial mesh refinement
    - Used Carlson even-moment (level symmetric) cubature

## ABTR 33 group (120 periodic)



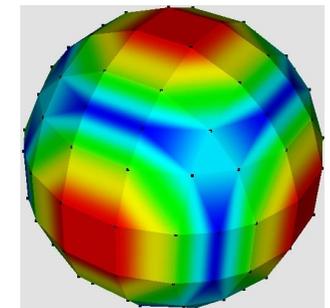
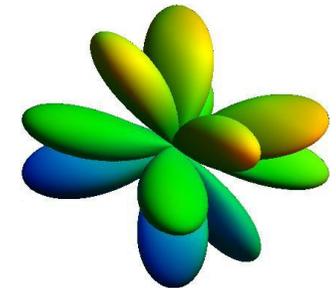
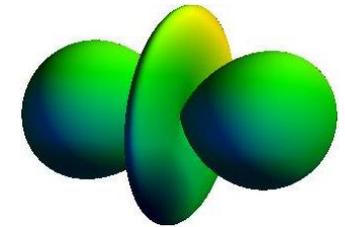
Eigenvalue error (pcm)

Angular Resolution	VARIANT	PN2ND	SN2ND
1	-1588	-1594	-192
2	-237	-249	-1
3	-91	-109	-69
4	-47	-70	-47
5		-55	-51

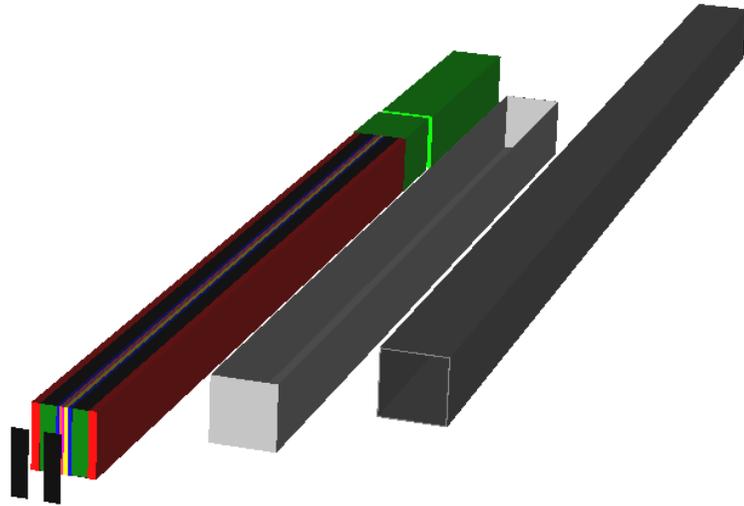


# Assembly Level Homogenization (cont...)

- VARIANT can easily out perform PN2ND and SN2ND
  - Uses hybrid finite element (nodal) combined with spherical harmonics
    - Spatial approximation includes discontinuities in even- and odd-parity flux
    - Defines much fewer degrees of freedom in assembly homogenized problems
  - Not currently ideal for all problems
    - 1/6 hexagonal ABTR with 230G,  $P_5$ - $S_5$  requires 14 hours of cpu time ( $5 \cdot 10^8$  dofs)
    - ZPR drawer homogenized problems have convergence problems
    - Cannot treat void or pure scattering regions
- PN2ND uses UFE combined with spherical harmonics
  - Even-parity unstructured mesh treatment assumes continuous even-parity flux
    - Requires careful boundary layer meshing (key weakness of method)
    - Increased memory storage relative to VARIANT and bandwidth limited flop rate
  - Uses a parallel CG operation on the WG space-angle system
    - Preconditioner is just diagonal angular sub-system
    - Use SSOR in parallel CG solver from PETSc on each angular sub-system
- SN2ND uses UFE combined with discrete ordinates
  - Mesh related problems are identical to PN2ND
  - Uses a scattering source iteration on WG space-angle system (CG on  $L^{-1}$ )
    - Uses diagonal angular sub-system preconditioner
    - Uses SSOR via parallel CG solver in PETSc
    - Started development of multi-level h multi-grid preconditioner



# ZPR6 Assembly 6A



Single ZPR6 Drawer

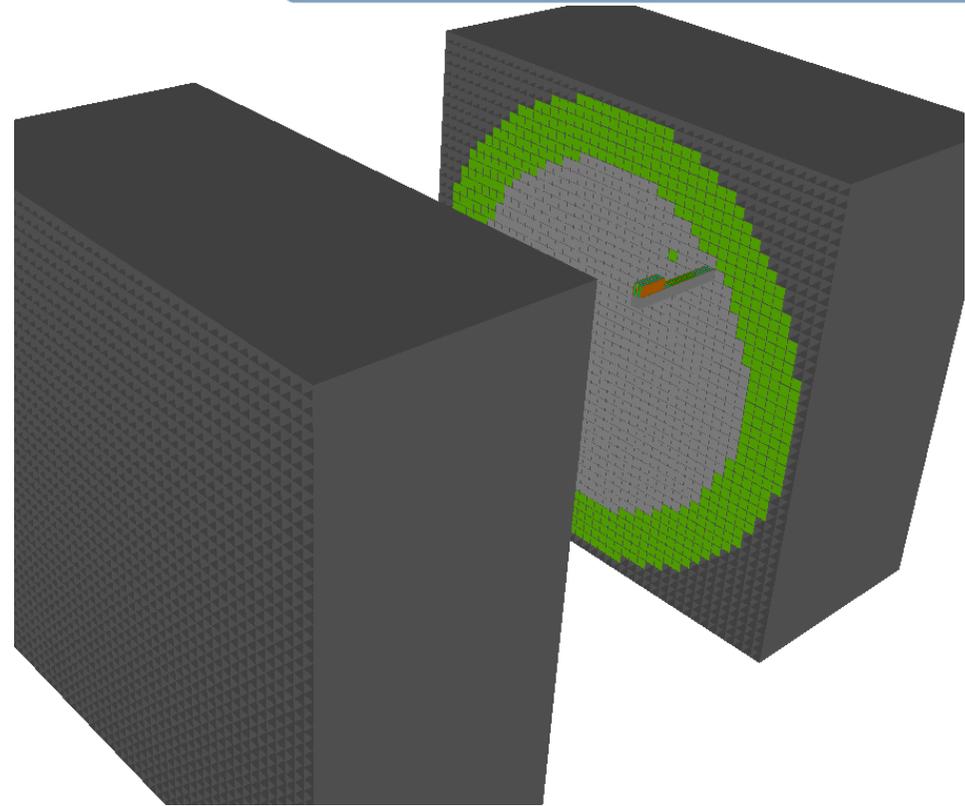
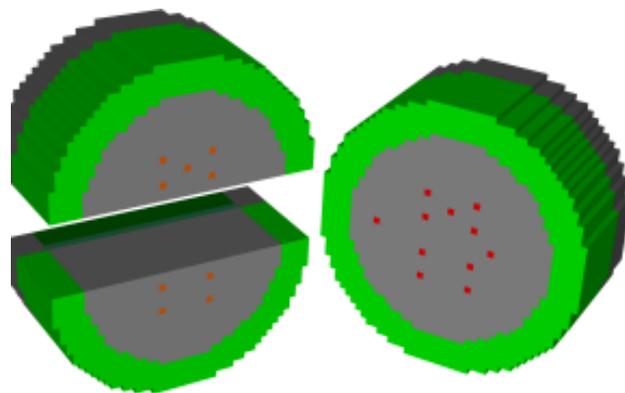


Plate by Plate ZPR6 Geometry

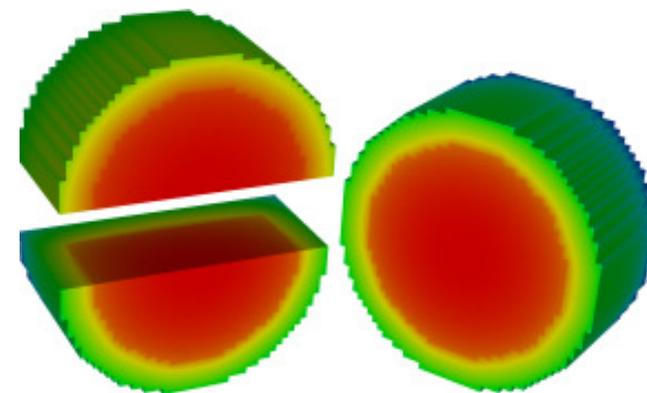
- Over a period of 30 years, more than a hundred ZPR critical assemblies were constructed at Argonne National Laboratory: ZPR-3, ZPR-6, ZPR-9 and ZPPR.
- The geometrical information for selected loadings is now widely available (ICSBEP)
- Materials are very well known compared with existing production reactors.
- In addition to experimental validation we can compare with CE MCNP/VIM solutions
- No concerns for multi-physics coupling

# Standard Homogenized Approach

- Used 1-D “equivalent” lattice cell calculation to generate cross sections in MC<sup>2</sup>-3
  - Homogeneous solution only gives the global gradient
  - Done to capture foil reaction rates and compare other reactor physics parameters
  - Need to combine global gradient with lattice cell calculation to extract solution
- Reference solution is experiment (i.e. critical)
  - SN2ND: 0.99966 VIM: CE 0.99981 ± 0.00025
  - Ignoring plate heterogeneity
    - SN2ND: 0.99344 VIM CE: 0.99400 ± 0.00020
- We have obtained similar results on ZPR 6/7 and ZPPR-15
- We are focused on using 2-D MOC for future cross section generation



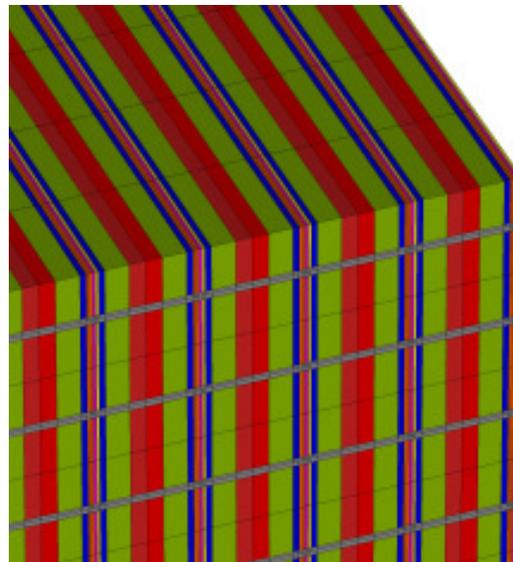
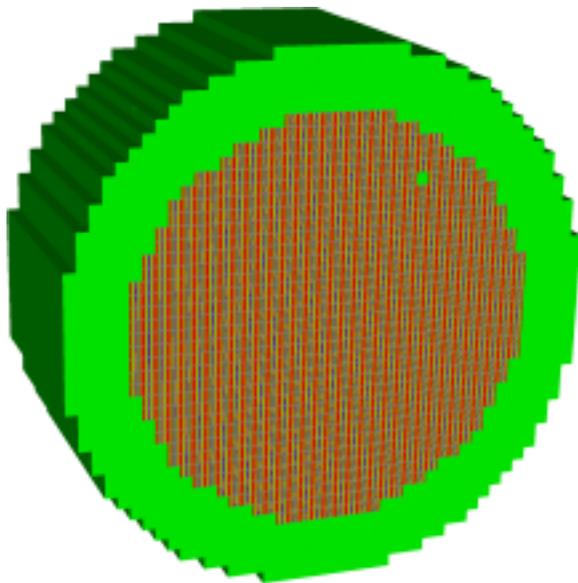
Geometry



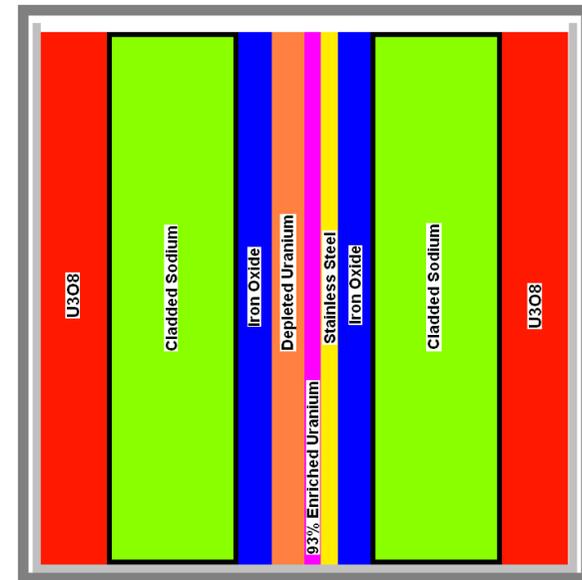
Power on a Log Scale

# Plate-by-Plate ZPR6 Assembly 6A

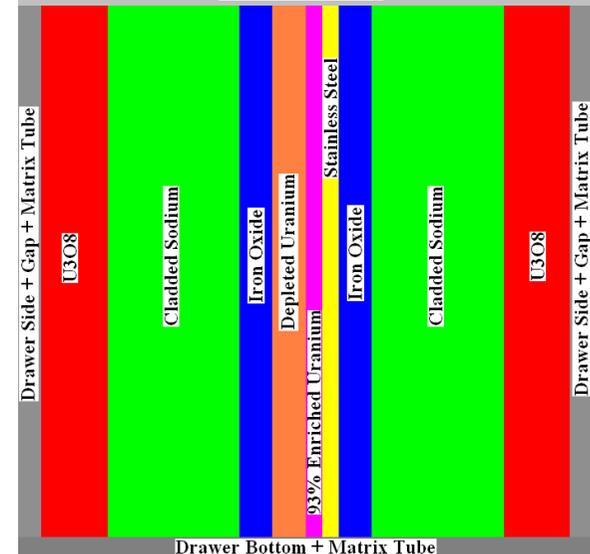
- SN2ND cannot handle explicit voids
  - Not really an issue for this problem
  - Development:  $2 \cdot 10^6 \rightarrow +50 \cdot 10^6$  vertex mesh
  - 33 group calculation requires  $\sim 40$  minutes on full parallel machine ( $\sim 700$  billion dof)
- Cross sections generated with 1-D lattice cell
  - The implementation of these cross sections in the explicit geometry model is not consistent.
  - The cross section data representation is inaccurate



## Exact Geometry

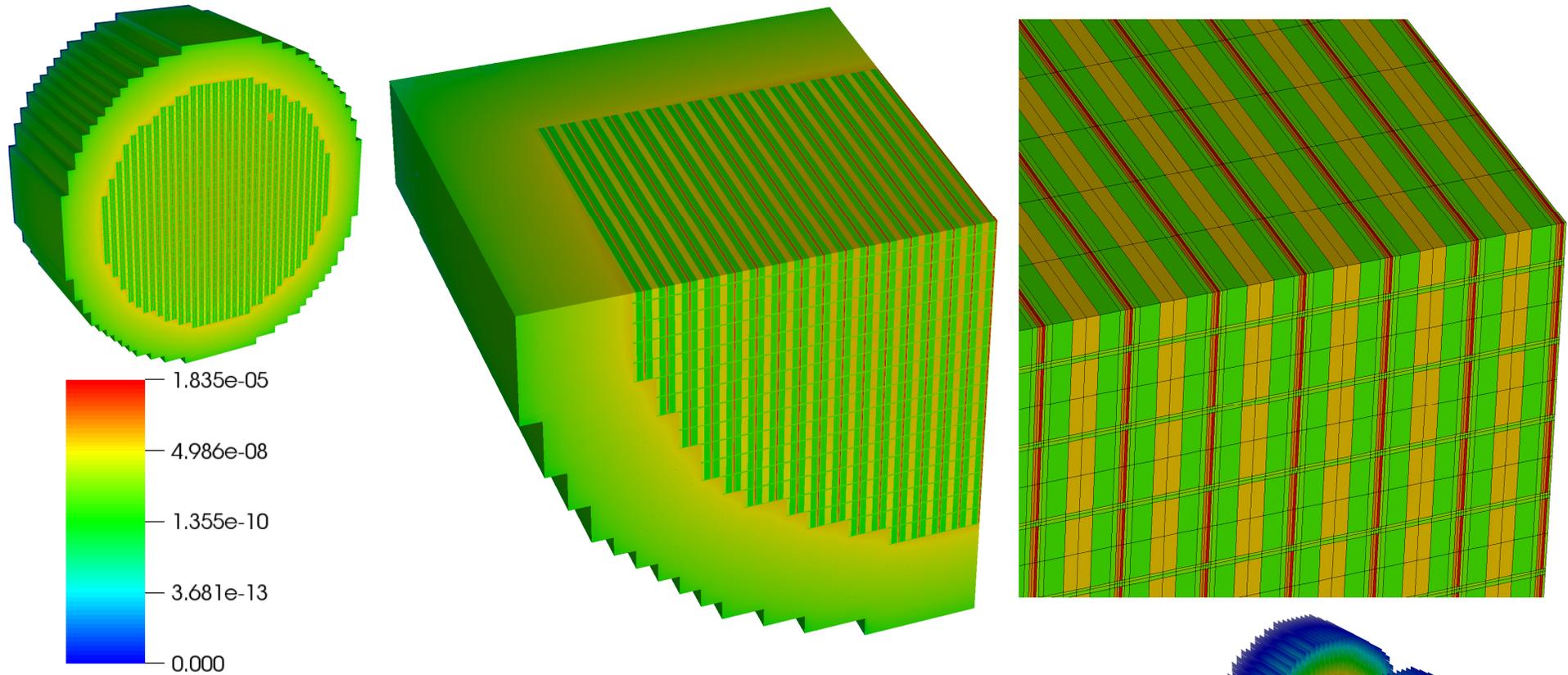


## Matrix Tube + Gap

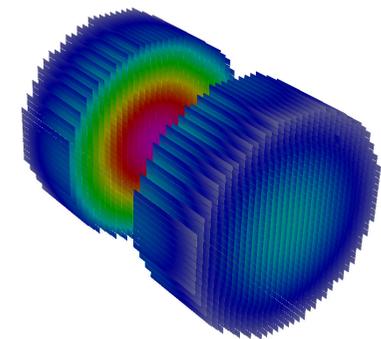


## SN2ND Geometry

# Plate by Plate ZPR-6 Assembly 6A, cont...

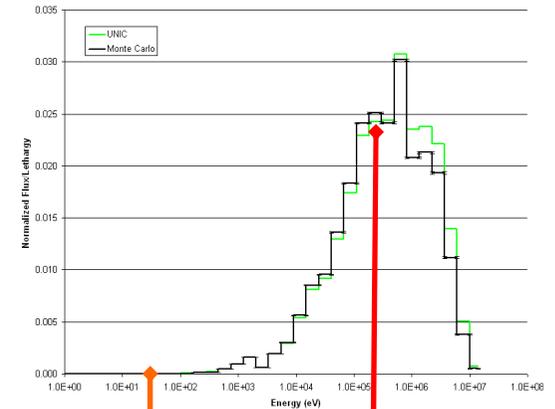
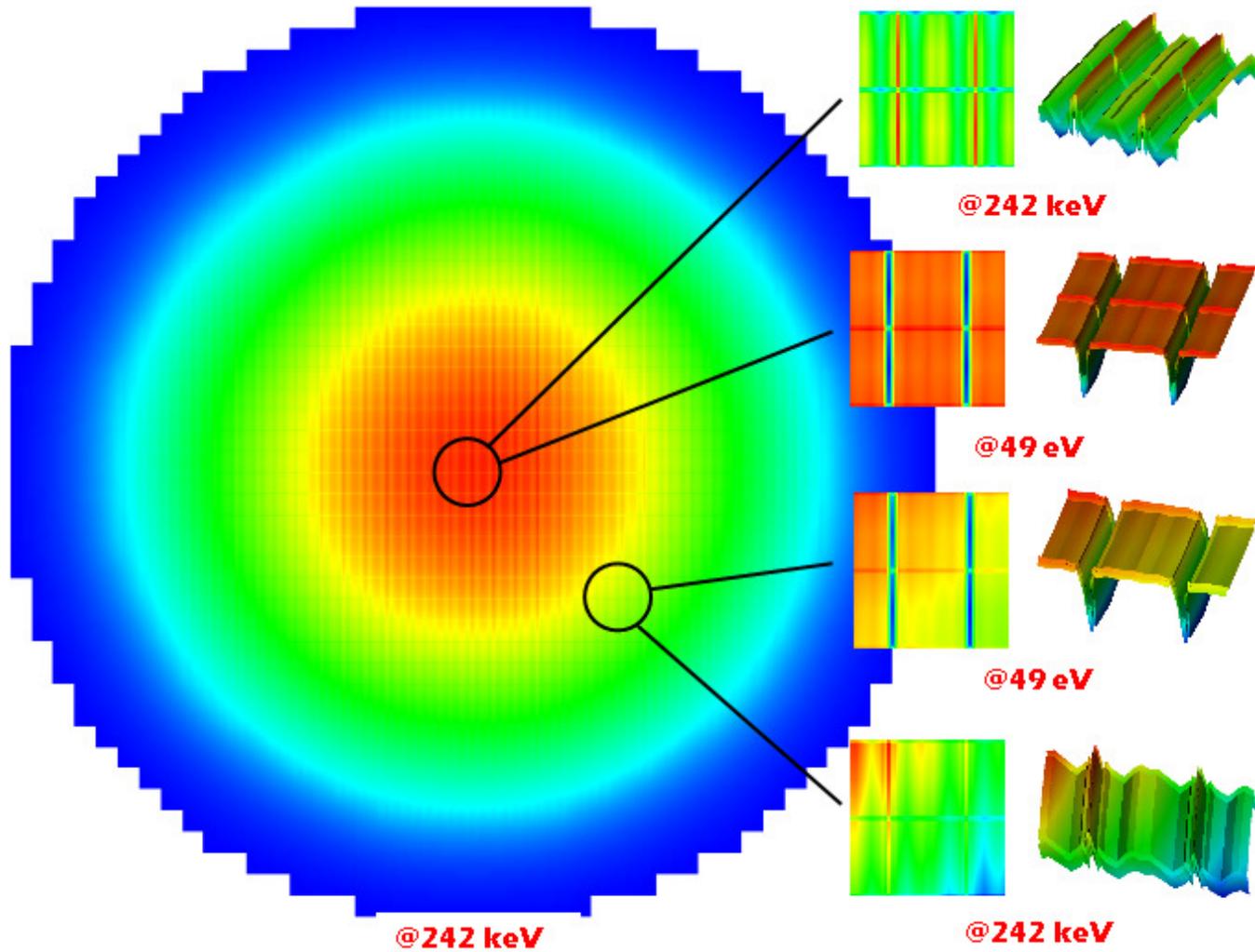


- Maximum of 116 group with  $P_5$  scattering (9, 33, 70, 116)
- Maximum 50,000,000 vertex mesh (cubic hexahedrons)
- Maximum  $S_{28}$ , (LT or DLT)



Just EU plates

# Flux Solution for ZPR6 Assembly 6A Experiments



49 eV      242 keV

- Local gradients on drawers exhibit global gradient
- Resolved spatial gradients should result in better foil reaction rates



## SN2ND Parallel Performance

- Strong spatial scaling of 94% on BlueGene/P-ANL

Total Cores	Vertices/ Process	Total Time (seconds)	Parallel Efficiency
8,192	7,324	2,402	100%
16,384	3,662	1,312	92%
24,576	2,441	873	92%
32,768	1,831	637	94%

Mainly measurement of PETSc

Strong scaling in angle is <75%

Diffusion equation needs further partitioning

- Weak angle scaling of 75% on XT5. 76% on BlueGene/P 294,912 cores JSC

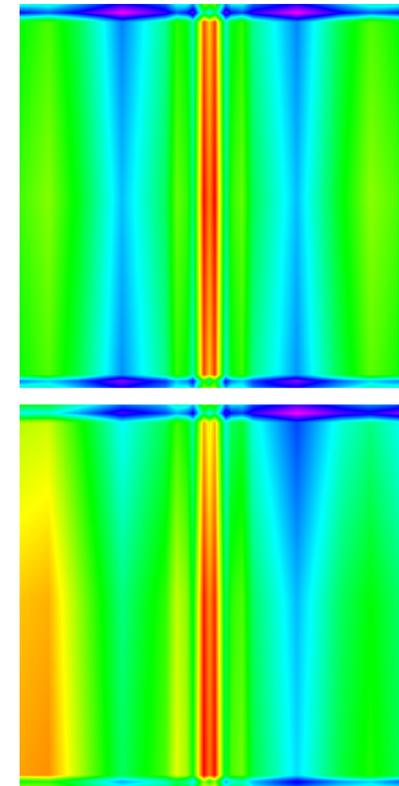
Total Cores	4 $\pi$ Angles	Total Time (seconds)	Weak Scaling
16,512	32	1891	100%
37,152	72	1901	99%
66,048	128	1829	103%
103,200	200	2050	92%
148,608	288	2298	82%
222,912	432	2517	75%

Weak scaling in space means mesh refinement for us

This can be good and bad. Refinement of bad aspect ratio elements produced >95%

# Lessons Learned from ZPR

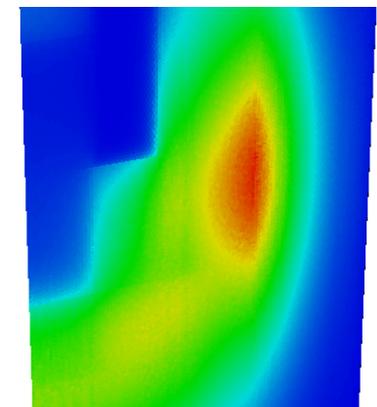
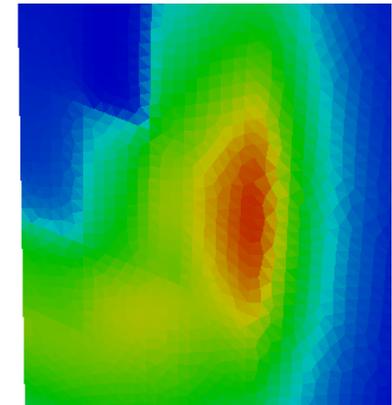
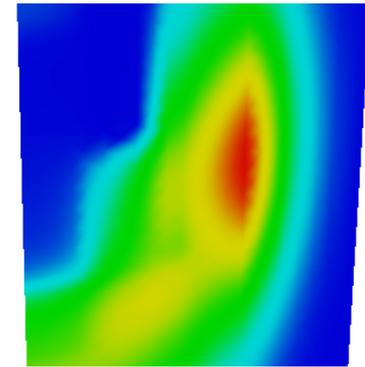
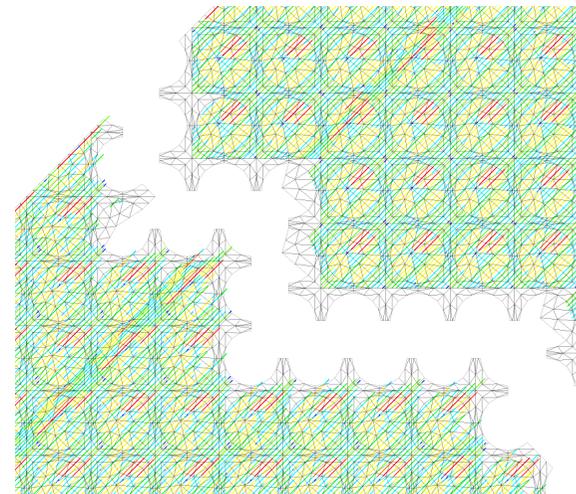
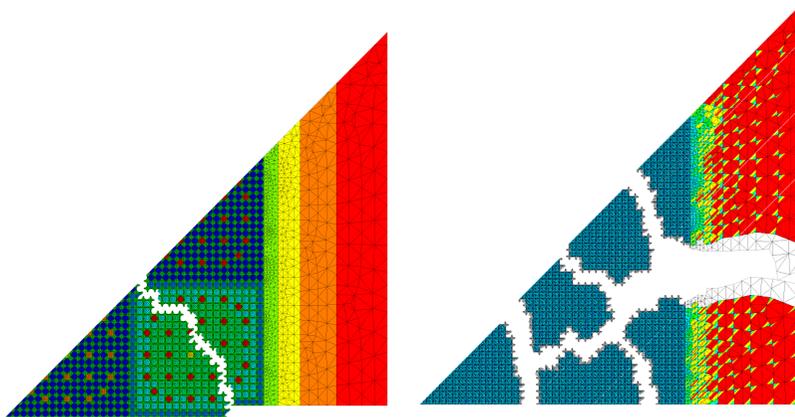
- Cross sections are not sufficiently accurate
  - 1-D model is appropriate and proves to be accurate for drawer average cross sections
  - Equivalence theory used to generate self-shielded ultrafine group cross sections is approximate
    - A hyperfine group (i.e., pointwise) calculation can help
  - Plate-by-plate cross sections may reduce the error, but the fundamental issue is that the global gradient is not seen in the cell lattice problem (either 1-D slab or 2-D MOC)
- New approach: Improve accuracy of legacy methodology
  - Incorporate global and local gradients via a 2-D MOC solution
    - Generate drawer homogenized cross sections
  - Use SN2ND or improved VARIANT to solve global homogenized problem
- With new capability we will research using plate-dependent cross sections in the radial plane



Flux at 243 keV  
on Log Scale  
Top is ~lattice calc.  
Bottom is real world

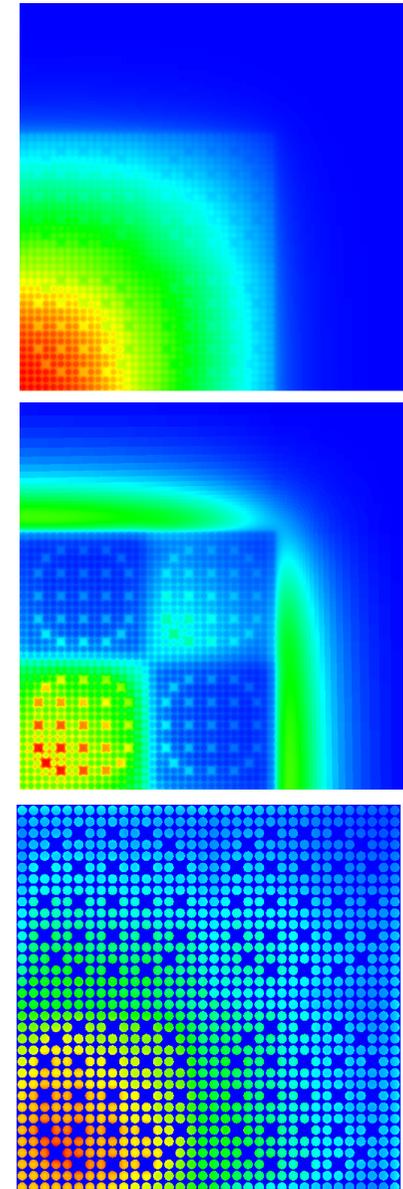
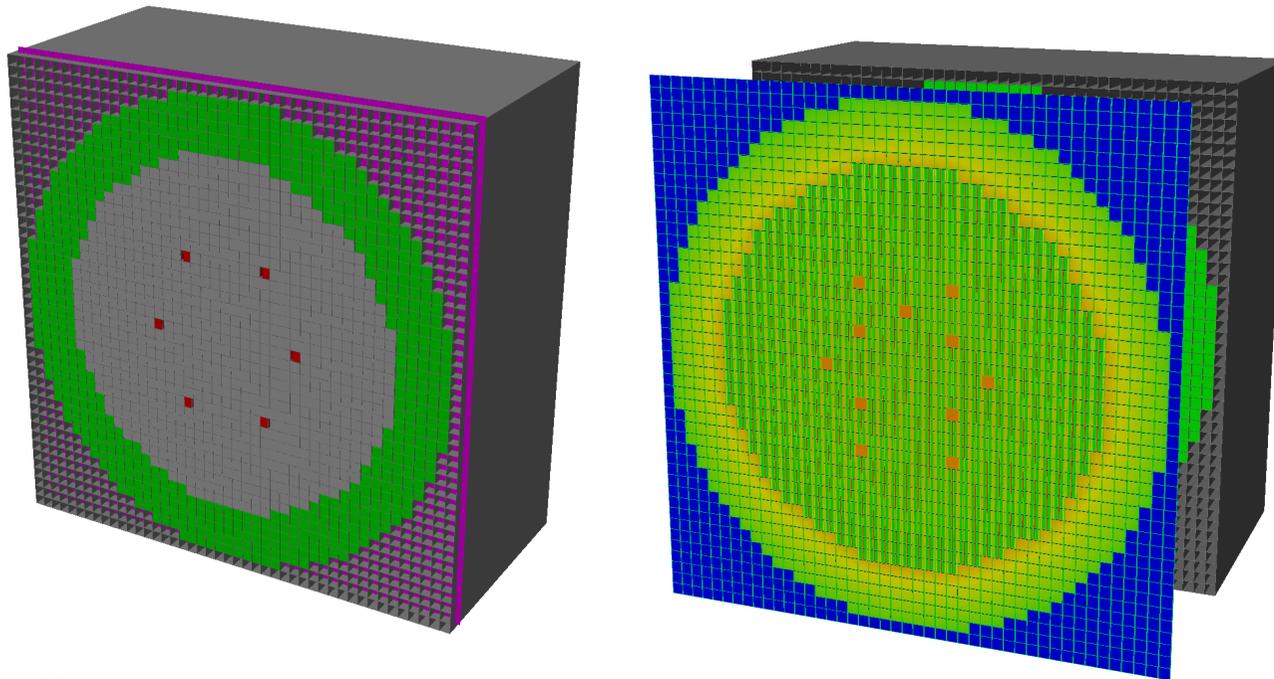
# The Future for Fast Reactor Cross Sections?

- In 2007 we researched a 3-D MOC for fine level solution
  - 10,000 to 1 element comparison with SN2ND
  - Parallel algorithm is relatively immature; ours was not scaling
- In 2009 we rebuilt 2D and 3D MOCFE solver
  - Easier to modify/maintain/develop
  - Faster ray tracing, exact domain surface discretization
  - Assumed a Krylov subspace method for spatial decomposition
    - More appropriate path for large scale parallelism
    - Assumes trajectory splitting and communication of trajectory flux
    - Needs research into good preconditioner (synthetic diffusion?)



# MOCFE continued

- New version is >10 times faster than old version
- Validated “accuracy” on C5G7, CANDU, ABTR geometries
- Working on PWR, BWR, VHTR, and ZPR geometries
- Haven’t tested out any parallel options
- Haven’t tested out the Krylov solver options
- Have no clue how well it compares to other MOC solvers



# Future Work and Key Issues

- SN2ND
  - Implement multi-level h-multigrid preconditioner scheme
  - Implement error estimator for intelligent mesh refinement and accuracy assessment
  - Investigate parallel decomposition of energy with Krylov subspace methodology
  - Even with ~300,000 cores, direct whole core transport calculations are not practical yet
- Cross Section Generation
  - Optimize MC<sup>2</sup>-3 code for speed and investigate parallel execution of work
  - Fully validate 1-D, 2-D, and 3-D MOCFE for parallel execution of space-angle-energy
  - Investigate option to use localized hyperfine-group spectrum calculation with fine-group whole core transport calculation
- “Intermediate” fidelity methods to perform routine design calculations (<<1000 processors)
  - 2D MOC calculation for cross section generation
    - New homogenization and group collapsing schemes
  - PN2ND or SN2ND calculation with homogenized pin-cell
  - Improved NODAL based code with assembly homogenization
    - Is there a potential for 2D/1D coupled schemes like DeCART?

