

## 14 MeV Neutron Irradiation Effect on Superconducting Properties of Nb<sub>3</sub>Sn Strand for Fusion Magnet

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**Abstract.** Using 14 MeV neutron source and fission reactors, neutron irradiation tests of Nb<sub>3</sub>Sn strand were carried out. The maximum fluence was  $2.65 \times 10^{21}$  n/m<sup>2</sup> for 14 MeV neutron and  $4.3 \times 10^{24}$  n/m<sup>2</sup> for fission neutron. By the irradiation with 14 MeV neutron, increase of  $I_C$  (1.45 times at 14 T), no change of  $B_{C2}$  (under 100 mA) and degradation of  $T_C$  (0.2 K) were measured. Magnetization of irradiated samples at fission reactors suggested that  $1.0 \times 10^{21}$  n/m<sup>2</sup> irradiation would increase  $I_C$  but  $1.1 \times 10^{24}$  n/m<sup>2</sup> irradiation would degrade  $I_C$ . The irradiation of  $4.3 \times 10^{24}$  n/m<sup>2</sup> made Nb<sub>3</sub>Sn strand non superconductivity any more. These facts were considered to be caused by strengthening of pinning force and disordering of A-15 crystal with knock-on effect of fast neutron. Higher neutron fluence would increase  $I_C$  but destroy the crystal at the same time.

### 1. Introduction

Large scale fusion devices such as ITER and JT-60SA being under construction [1,2] require large current superconductors working in high magnetic field to produce strong magnetic field to confine high performance plasma certainly. Since they will produce 14 MeV neutrons by deuterium-tritium (D-T) reaction or 2.45 MeV neutrons by deuterium-deuterium (D-D) reaction and the generated neutrons will go out of the plasma vacuum vessel and reach superconducting magnets, though neutron shielding systems like a blanket and a double-wall vacuum vessel with water will be installed, irradiation effects of fast neutrons on superconducting properties must be understood clearly.

Since the Nb<sub>3</sub>Sn strands have been planned to apply to ITER magnets and other fusion applications, some important investigations on the irradiation effects have been performed based on individual and separated programs [3-6]. Therefore, the knowledge on the effect and the mechanisms on the change in superconductivity are fragmentary and limited. In order to promote better understanding on the neutron irradiation effect on superconducting properties of Nb<sub>3</sub>Sn strands and to pile up the data base systematically for the design and the construction of the fusion magnets, a collaboration network has been established in Japan [7,8] and the neutron irradiation and post irradiation test facilities have been designed and installed step by step. One of the fruitful results of this network activity is an installation of a 15.5 T superconducting magnet with thermal conduction cooling at a radiation control area in Oarai branch of Institute for Materials Research (IMR), Tohoku University [9]. The high magnetic field tests of activated samples will start at the end of 2010 fiscal year.

This paper presents the changes in the superconducting properties of Nb<sub>3</sub>Sn strands after 14 MeV neutron irradiation and magnetization property after fission neutron irradiation and the mechanisms for the property changes are discussed.

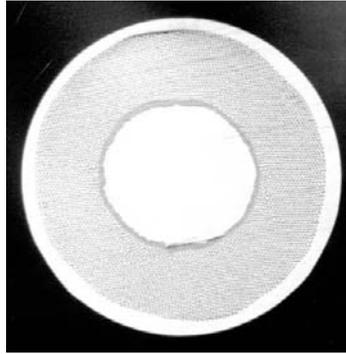


FIG.1. Cross section of  $Nb_3Sn$  strand used.

## 2. Test materials and procedures

Tested superconducting strand is a bronze route  $Nb_3Sn$  wire. The cross section is shown in Fig.1. The outer diameter of the strand is 0.7 mm and the matrix is niobium. The filament diameter is about 4.6  $\mu m$  and number of filaments is about 4,900. The center part and the surrounding area are pure copper and the copper area ratio is about 20.5%. The residual resistance ratio (RRR) of copper is about 500. The straight strand was cut into about 45 mm long and heat treated to generate  $Nb_3Sn$  phase in vacuum.

Irradiation tests were carried out at three facilities, i.e. Fusion Neutronics Source (FNS) in Japan Atomic Energy Agency (JAEA), Japan Research Reactor No.3 (JRR-3) in JAEA, and Belgian Reactor No.2 (BR2) in Belgium. FNS equips a rotating target to produce 14 MeV pure neutrons by D-T reaction. The flux is about  $7.2 \times 10^{12}$  n/s. The temperatures of the samples during the irradiation were 4.5 K using GM refrigerator and RT on the cryostat surface. The samples were set in a certain distance from the D-T point and the maximum neutron fluence of  $2.65 \times 10^{21}$  n/m<sup>2</sup> was achieved in total at RT. The JRR-3 has a Rabbit system with cooling water to irradiate materials. Samples are set in an aluminum alloy capsule with aluminum foil and sent to a suitable position in the JRR-3 core. The system allows taking out the samples even when the reactor is under operation. The water temperature is controlled at 30 C and the sample temperature during irradiation is around 100 C. The fast neutron flux of over 0.1 MeV is  $1.4 \times 10^{16}$  or  $1.7 \times 10^{16}$  n/m<sup>2</sup>/s., depending on the location in the core. The BR2 has larger nuclear power than the JRR-3 and the higher neutron flux is possible. The maximum neutron fluence achieved in this study is  $4.3 \times 10^{24}$  n/m<sup>2</sup>. The samples cut out of the same wire were delivered to these facilities and the neutron irradiation was conducted.

The irradiated samples at FNS were sent to High Field Laboratory for Superconducting Materials (HFLSM) in IMR, and the critical current ( $I_C$ ) and the critical magnetic field ( $B_{C2}$ ) were measured using 28 T hybrid magnet. The criterion of the  $I_C$  determination was 1  $\mu V/cm$  and the  $B_{C2}$  was evaluated by sweeping the magnetic field at the rate of 3.2 T/min under 100 mA of transfer current. The critical temperature ( $T_C$ ) was measured using GM refrigeration system installed at FNS by raising the temperature to 20 K at the rate of 0.1 K/min and recording the voltage with a span of about 10 mm under +/- 50 mA. The magnetization of the samples irradiated at the JRR-3 and the BR2 was evaluated using Magnetic Property Measurement System (MPMS-5, Quantum Design Inc.) installed at Oarai branch of IMR. Diagrams of magnetization against magnetic field (+/- 5 T) were obtained at 4.5 K and diagrams of magnetization against temperature were done under 0.005 T. A sample tested

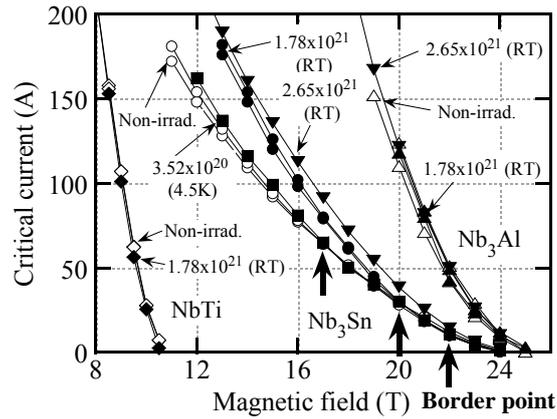


FIG.2. Change in  $I_C$  of  $Nb_3Sn$  strand by neutron irradiation.

was a few millimeters long and cut out of the about 45 mm long strand. To avoid an electrical circuit, both ends of the sample were polished with emery papers. All tests with the activated samples were carried out according to the rules on radioactive isotopes.

### 3. Results and discussion

#### 3.1 Critical current, critical field and critical temperature

The dependence of  $I_C$  of the  $Nb_3Sn$  strand on the magnetic field is shown in Fig.2. The results of the  $NbTi$  and  $Nb_3Al$  strands are also presented for a comparison. The  $Nb_3Sn$  strand showed significant increase in the  $I_C$  after the 14 MeV neutron irradiation. The increase occurred in the lower magnetic field first and then the change expands to the higher magnetic field. When the border point is defined as the field where the  $I_C$  of the irradiated sample got away from the  $I_C$  curve of the non-irradiated one, the border point moves to the higher magnetic field as the neutron fluence increased. It means that the irradiation damage density would have the effect on the pinning force which affects the increase of  $I_C$  discussed later. The results of  $B_{C2}$  measurement are shown in Fig.3. At the neutron fluence of  $2.65 \times 10^{21} \text{ n/m}^2$ , the  $B_{C2}$  under 100 mA did not change. The  $B_{C2}$  is related to three parameters, normal state resistivity ( $\rho_n$ ), electronic specific heat coefficient ( $\gamma$ ) and critical temperature ( $T_C$ ). As mentioned later.  $T_C$  drops a little, but there are no clear information on  $\rho_n$  and  $\gamma$ . So, the detailed discussion on the  $B_{C2}$  is very hard at present. To discuss the effect of the neutron fluence on the  $I_C$ , the ratio of the  $I_C$  of irradiated sample to the  $I_C$  of non irradiated one ( $I_{C0}$ ) is calculated and plotted

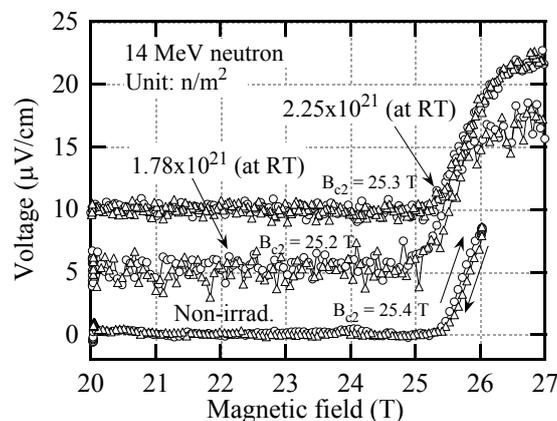


FIG.3. Results of  $B_{C2}$  measurements of  $Nb_3Sn$  strand under 100 mA.

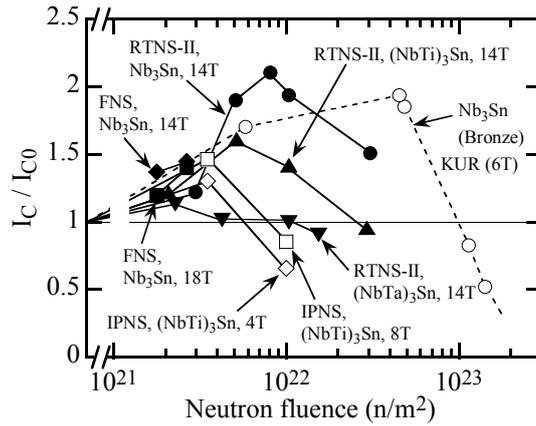


FIG.4.  $I_C/I_{C0}$  of  $Nb_3Sn$  strand against neutron fluence ( $> 0.1$  MeV) [3-5].

against the neutron fluence as shown in Fig.4 [3-5]. As the general tendency, the  $I_C$  increases once and decreases to below  $I_{C0}$  when the neutron fluence increased. As discussed above (Fig.2), the degree of the  $I_C$  increment depends on the magnetic field and there is a tendency that the ratio becomes large in the lower field. The present results are plotted on a little bit higher ratio region than those reported before.

The results of  $T_C$  measurements are shown in Fig.5. After the  $2.65 \times 10^{21}$   $n/m^2$  irradiation, it was found that  $T_C$  decreased by 0.2 K. It means that the disturbance of long range ordering starts already even though the  $I_C$  is in an increasing phase. The ratio of  $T_C/T_{C0}$  presented in

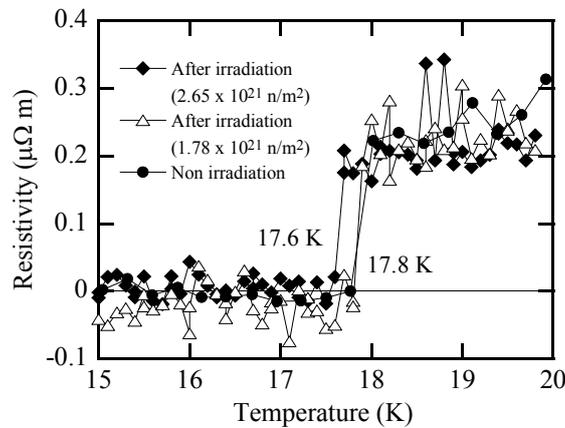


FIG.5. Results of  $T_C$  measurement of  $Nb_3Sn$  strand.

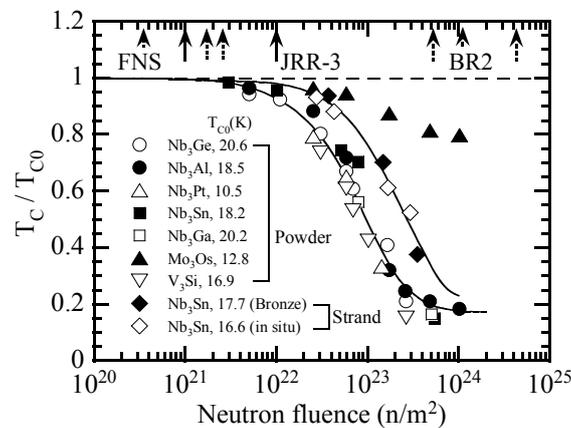


FIG.6.  $T_C/T_{C0}$  of A-15 powders and  $Nb_3Sn$  strands against neutron fluence ( $> 0.1$  MeV) [3,6].

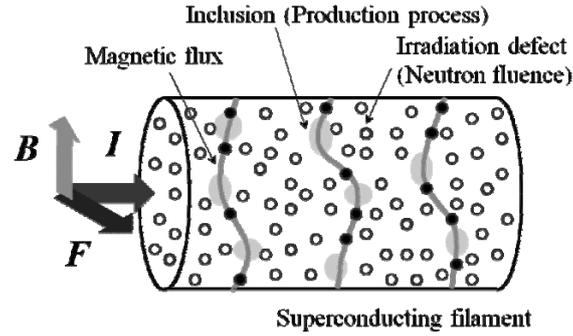


FIG.7. Schematic drawing of pinning sites in irradiated  $Nb_3Sn$  filament.

published papers was plotted against neutron fluence as shown in Fig.6 [3,6].  $T_C$  is  $T_C$  of the irradiated sample and  $T_{C0}$  is  $T_C$  of the non-irradiated one. The  $T_C$  begins to decrease at the fluence range of  $10^{21}$  to  $10^{22}$   $n/m^2$ . In the reference papers, the  $T_C$  of A-15 powders were evaluated by magnetization method [6] and the strands were studied by transferring current method [3]. Therefore, there might be some differences in  $T_C/T_{C0}$ . In the present study, the  $T_C$  is 17.6 K and the  $T_{C0}$  is 17.8 K, and the ratio becomes 0.988 at  $2.65 \times 10^{21}$   $n/m^2$  irradiation. This result is consistent with the data in Fig.6. The arrows in Fig. 6 show the performed neutron fluence in each neutron source and some magnetization results will be shown later.

A schematic image of the strengthening mechanism of pinning sites is shown in Fig. 7. The  $I_C$  is strongly related to pinning condition of the magnetic flux. In the case of  $Nb_3Sn$  strand, the magnetic flux passes through inclusions on grain boundaries and pinned there. When the current runs into  $Nb_3Sn$  filament, electro-magnetic force acts on the flux so that it would be moved to the vertical direction of the current. Therefore, the  $I_C$  is considered as a current when the pinned fluxes start to move gradually. When the strand is irradiated with neutrons, irradiation damage such as interstitials and vacancies installed by knock-on effect of the fast neutron would be generated, and when the irradiation defects are installed on the flux or near the flux, they would support and strengthen the flux pinning force resulting in the increase of the  $I_C$ . Since the irradiation defects would have small ability to pin the flux, the large density of the irradiation damage will be needed to increase the  $I_C$ . However, when the large density of the damage is installed, the disordering of the A-15 crystal would occur and the degradation of the  $T_C$  will start. Since the inclusions are initiated during the fabrication process of the strand, the effect of the irradiation damage (change in the pinning force) will be different depending on the production process. In addition, there will be effects of the neutron spectrum and the irradiation temperature.

### 3.2 Magnetization property

Diagrams of the magnetization against the magnetic field are shown in Fig.8. There are three diagrams, non-irradiated one, after the irradiation of  $1.0 \times 10^{22}$   $n/m^2$ , and after the irradiation of  $1.1 \times 10^{24}$   $n/m^2$ . The irradiation of  $1.0 \times 10^{22}$   $n/m^2$  increased the hysteresis and makes the slope at around 2 to 5 T gentle. It suggests that the  $I_C$  and the  $B_{C2}$  would increase. However, the irradiation of  $1.1 \times 10^{24}$   $n/m^2$  made the hysteresis very small and it means the very small  $I_C$ . From the change in  $T_C/T_{C0}$  shown in Fig.6, it is noticed that the  $1.1 \times 10^{24}$   $n/m^2$  irradiation would make  $T_C/T_{C0}$  around 0.2.

The enlarged diagram of  $1.1 \times 10^{24}$   $n/m^2$  irradiated sample is shown in Fig.9 together with the results of  $4.3 \times 10^{24}$   $n/m^2$  irradiation. The magnetization is very small comparing with Fig. 8

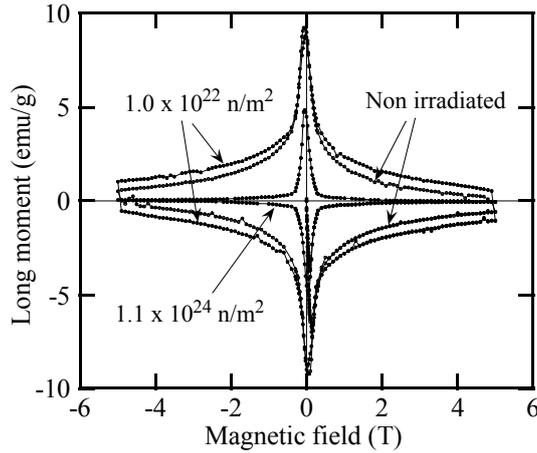


FIG.8. Magnetization of non-irradiated and irradiated  $Nb_3Sn$  strands.

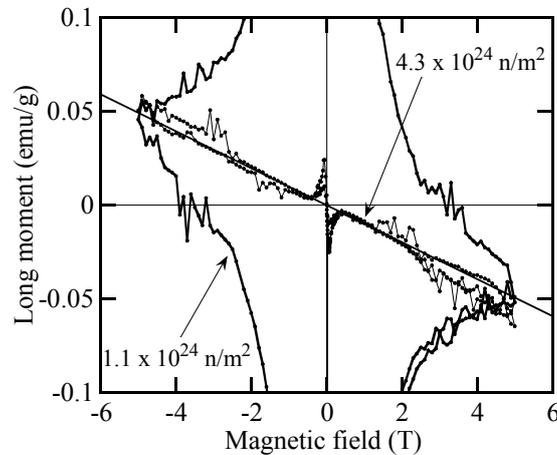


FIG.9. Magnetization diagrams of irradiated  $Nb_3Sn$  strands to  $1.1$  and  $4.3 \times 10^{24}$   $n/m^2$ .

and the vertical axis is enlarged by 100 times. It is clear that the  $1.1 \times 10^{24}$   $n/m^2$  irradiated sample still shows weak superconducting and diamagnetism. The same diamagnetism is observed in the results of  $4.3 \times 10^{24}$   $n/m^2$  irradiation and it is considered that the copper caused this diamagnetism which was used for a stabilizer in the strand. The sample irradiated to  $4.3 \times 10^{24}$   $n/m^2$  shows no superconducting, but very small indication of the magnetization is seen in the region of  $\pm$  about 0.3 T. This would be caused by pure niobium used for producing  $Nb_3Sn$  phase. It is recognized that niobium remained still in superconducting even when  $Nb_3Sn$  already became normal.

The diagrams of the magnetization against the temperature are shown in Fig.10. Non irradiated sample shows the  $T_C$  of 17.7 K and it is a good agreement with the results shown in Fig.5 (17.8 K). In the case of the resistivity-temperature relation (Fig.5), the resistivity changed sharply and it was easy to define the  $T_C$ . However, the magnetization changes gradually against temperature, so there is small uncertainty to determine the  $T_C$ . The magnetization profile of the non irradiated one presents three critical temperatures. The lowest is about 9.2 T which is the  $T_C$  of pure niobium. The second is about 15 K and it may be the  $T_C$  of other Nb-Sn phase. The third is the  $T_C$  of  $Nb_3Sn$  phase. The irradiation to  $1.0 \times 10^{22}$   $n/m^2$  drops the  $T_C$  to 17.3 K and the profile is almost same as the non irradiated one. The ratio of  $17.3/17.7$  ( $T_C/T_{C0}$ ) becomes 0.977 and this figure is good agreement with Fig.6 when it is plotted against the fluence of  $1.0 \times 10^{22}$   $n/m^2$ . The degradation of  $T_C$  at this fluence also suggests the disordering of the crystal even though the  $I_C$  is still increasing. After the

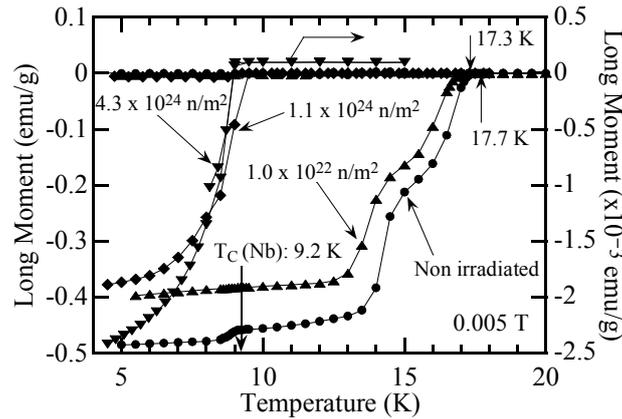


FIG.10.  $T_C$  measurement results of irradiated  $Nb_3Sn$  strand by SQUID.

irradiation to  $1.1 \times 10^{24} \text{ n/m}^2$ , the  $T_C$  dropped to about 9 K which was the  $T_C$  of niobium. In the engineering sense, this situation is no use for operation and it is very difficult to detect the change in  $T_C$  during the operation under the neutron irradiation. The evaluation method for the degradation of the superconductivity under the operation must be investigated, otherwise the quench should occur suddenly and it would not be recovered. The irradiation to  $4.3 \times 10^{24} \text{ n/m}^2$  makes the strand isolator and very weak superconductivity of niobium remains.

#### 4. Summary

The irradiation effect of the 14 MeV and the fission neutrons on the superconductivity of the  $Nb_3Sn$  strand was studied. The maximum fluence achieved was  $2.65 \times 10^{21} \text{ n/m}^2$  for 14 MeV neutron and  $4.3 \times 10^{24} \text{ n/m}^2$  for fission neutron. The main results are summarized as follows:

1. By the irradiation tests with 14 MeV neutron, the increase of  $I_C$  by 1.45 times at 14 T, no change of  $B_{C2}$  under 100 mA transport current and the degradation of  $T_C$  by 0.2 K were measured. Also, it is clarified that the increase of  $I_C$  occurs at the lower magnetic field first and the border point, where the  $I_C$  gets away from the  $I_C - B$  curve of the non irradiated one, moves to the higher magnetic field side as an increase of the fast neutron fluence. Therefore, it is expected that the  $B_{C2}$  will increase when the neutron fluence increases more and the border point passes the original  $B_{C2}$ . Since the irradiation tests with 14 MeV neutron will continue, the increase of  $B_{C2}$  will be demonstrated empirically in the near future.
2. The qualitative explanation on the  $I_C$  change was attempted based on the irradiation defects which would strengthen the flux pinning force. Also, the tiny degradation of the  $T_C$  (0.2 K) was recognized as the indication of the disordering of the crystal caused by the knock-on effect. Higher neutron fluence would increase the  $I_C$  but destroy the crystal at the same time. The balance of the strengthening and the disordering would determine the superconducting status under the neutron irradiation.
3. Magnetization of irradiated samples at fission reactors suggested that  $1.0 \times 10^{21} \text{ n/m}^2$  irradiation would increase  $I_C$  but  $1.1 \times 10^{24} \text{ n/m}^2$  irradiation would degrade  $I_C$ . The irradiation of  $4.3 \times 10^{24} \text{ n/m}^2$  would make  $Nb_3Sn$  strand non superconductivity any more. When the  $Nb_3Sn$  crystalline becomes isolator, the pure niobium still keeps the superconductivity but it becomes very weak because of the heavy irradiation.

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