

The Multi-Dimensional Analysis Method Development for Pool of KALIMER-600 using MARS-LMR CODE

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KAIST

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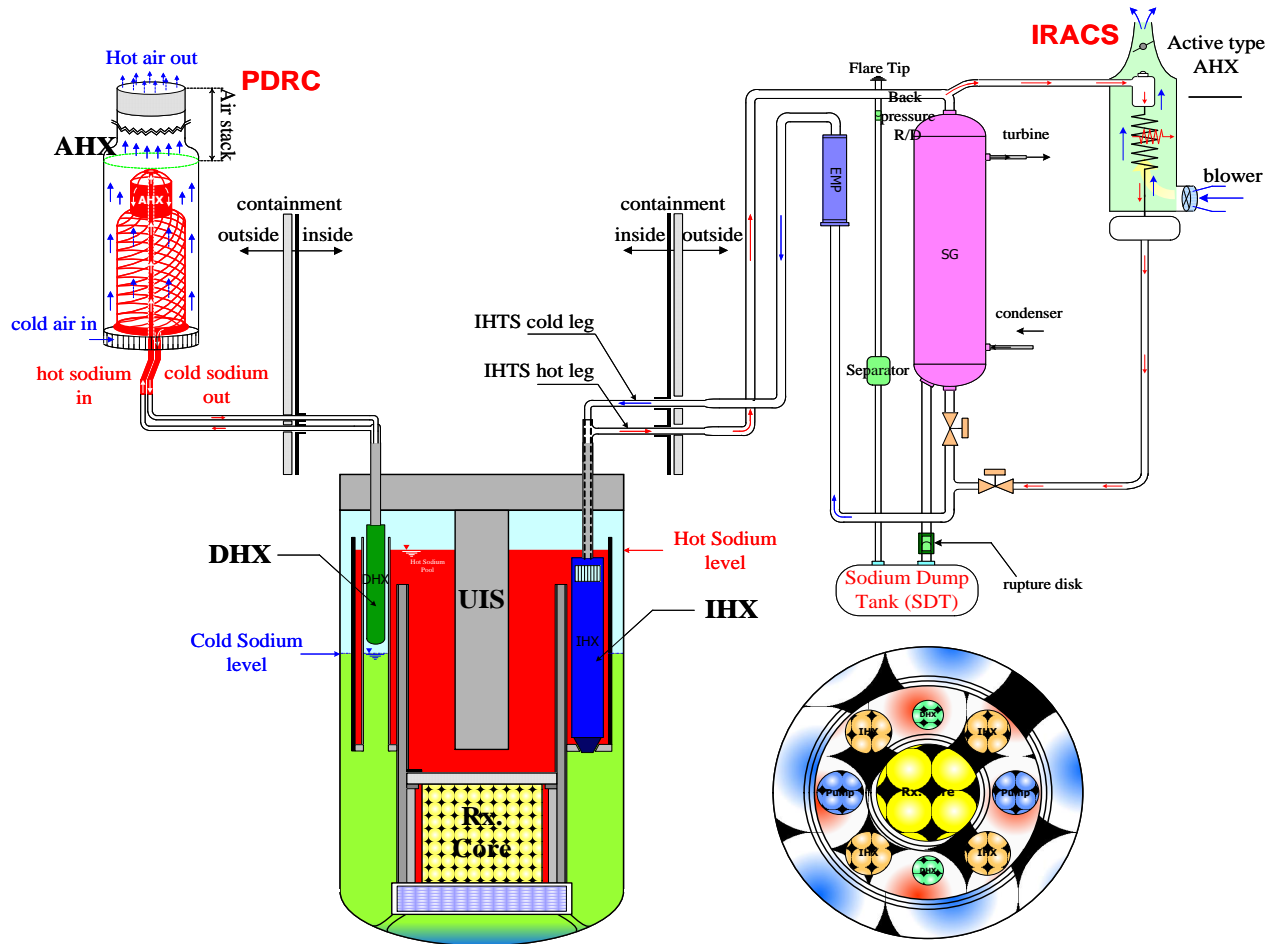
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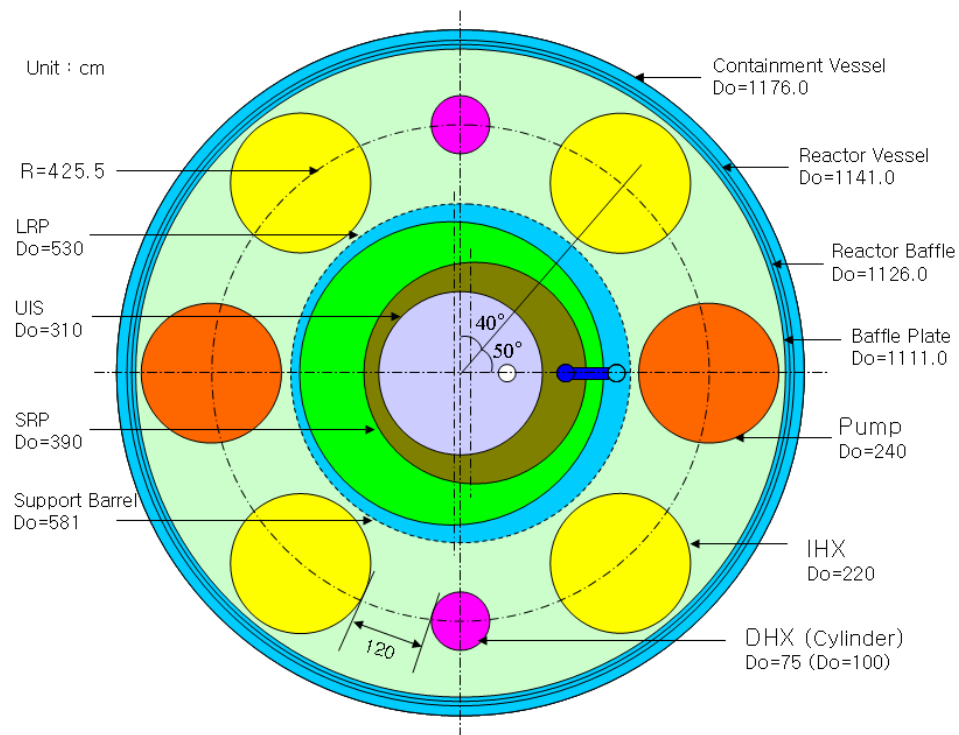
Discussion

SFR



SFR *KALIMER-600

SFR



		SFR (KALIMER-600)
Power[th]		1523.4MWt
Power[e]		637.5MWe
Net Eff.		39.4%
Pressure		about 1 atm
IHX Temp.	Inlet	544.8
	Outlet	385.9
IHX		4
PUMP		2
DHX		2

◎ **CODE Structure**

- Fortran 90 Modular Type Routine

◎ **Analysis Scope**

- 1D & Multi-D System Analysis Capability
- COBRA-TF Sub channel analysis Capability

◎ **Coupling with other functional code(DLL)**

- 3D Kinetics Code : MASTER and COREDAX
- Containment Code : CONTAIN & CONTEMP
- Severe Accident Code : MIDAS

◎ **Graphical User Interface**

◎ **Support New models**

- GEN-IV

MARS CODE

$$\frac{\partial}{\partial t}(\alpha_v \rho_v) + \frac{\partial}{\partial z}(\alpha_v \rho_v v_v) = \Gamma_{iv}$$

$$\frac{\partial}{\partial t}(\alpha_l \rho_l) + \frac{\partial}{\partial z}(\alpha_l \rho_l v_l) = \Gamma_{il}$$

$$\alpha_v \rho_v \frac{\partial v_v}{\partial t} + \alpha_v \rho_v v_v \frac{\partial v_v}{\partial z} = -\alpha_v \frac{\partial P}{\partial z} + \alpha_v \rho_v B_z - F_{VM} - F_{iv} - F_{Wv} + \Gamma_{iv} v_v$$

$$\alpha_l \rho_l \frac{\partial v_l}{\partial t} + \alpha_l \rho_l v_l \frac{\partial v_l}{\partial z} = -\alpha_l \frac{\partial P}{\partial z} + \alpha_l \rho_l B_z + F_{VM} - F_{il} - F_{Wl} + \Gamma_{il} v_l$$

$$\frac{\partial}{\partial t}(\alpha_v \rho_v U_v) + \frac{\partial}{\partial z}(\alpha_v \rho_v U_v v_v) = -P \frac{\partial \alpha_v}{\partial t} - P \frac{\partial}{\partial z}(\alpha_v v_v) + q_{Wv} + Q_{iv} + DISS_v$$

$$\frac{\partial}{\partial t}(\alpha_l \rho_l U_l) + \frac{\partial}{\partial z}(\alpha_l \rho_l U_l v_l) = -P \frac{\partial \alpha_l}{\partial t} - P \frac{\partial}{\partial z}(\alpha_l v_l) + q_{Wl} + Q_{il} + DISS_l$$

$$\frac{\partial}{\partial t}(\alpha_v \rho_v X_n) + \frac{\partial}{\partial z}(\alpha_v \rho_v X_n v_v) = 0$$

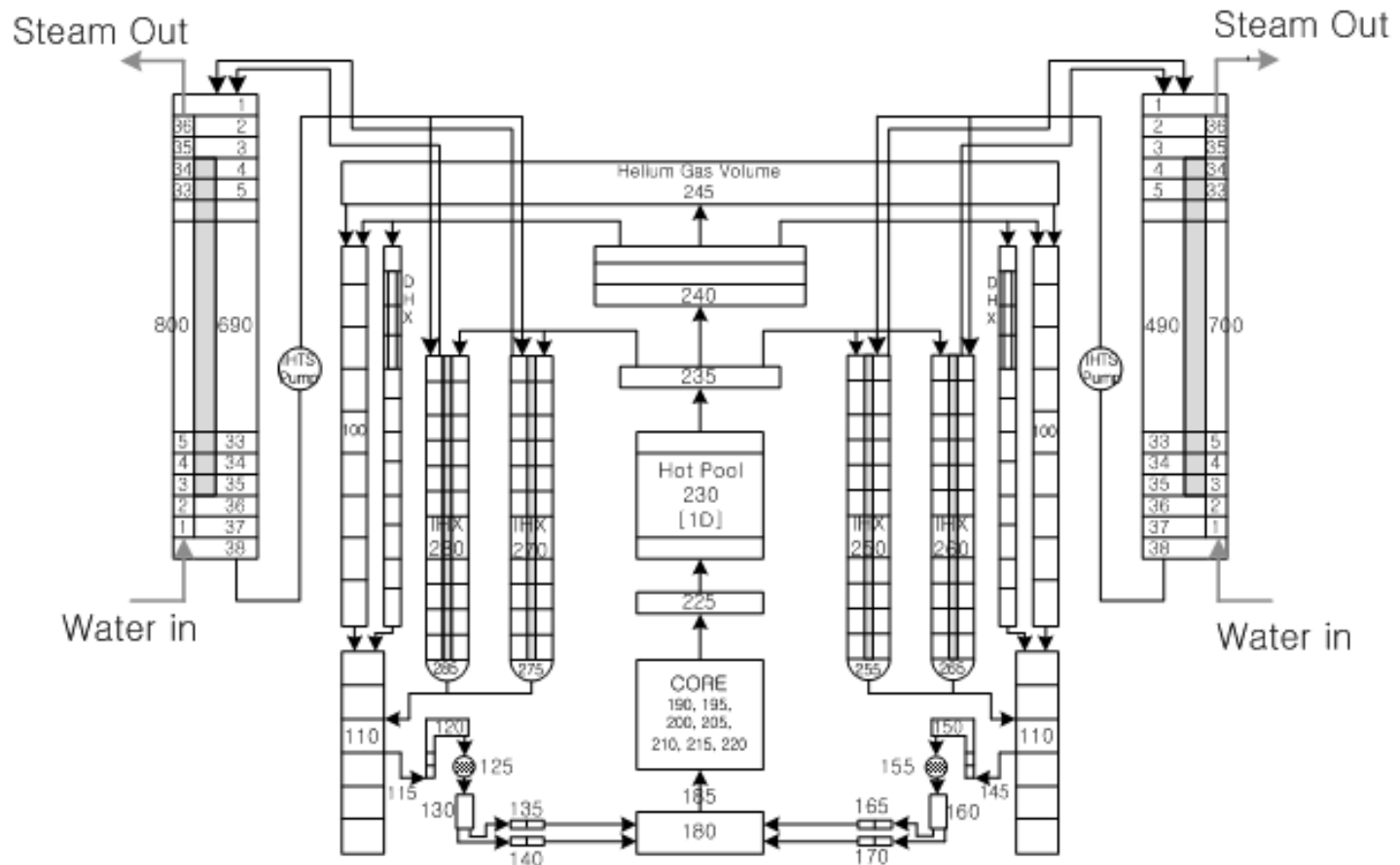
$$\frac{\partial \rho_B}{\partial t} + \frac{\partial}{\partial z}(\rho_B v_l) = 0$$

$$\Gamma_{iv} = -\Gamma_{il}$$

$$F_{iv} = -F_{il}$$

$$Q_{iv} = -Q_{il}$$

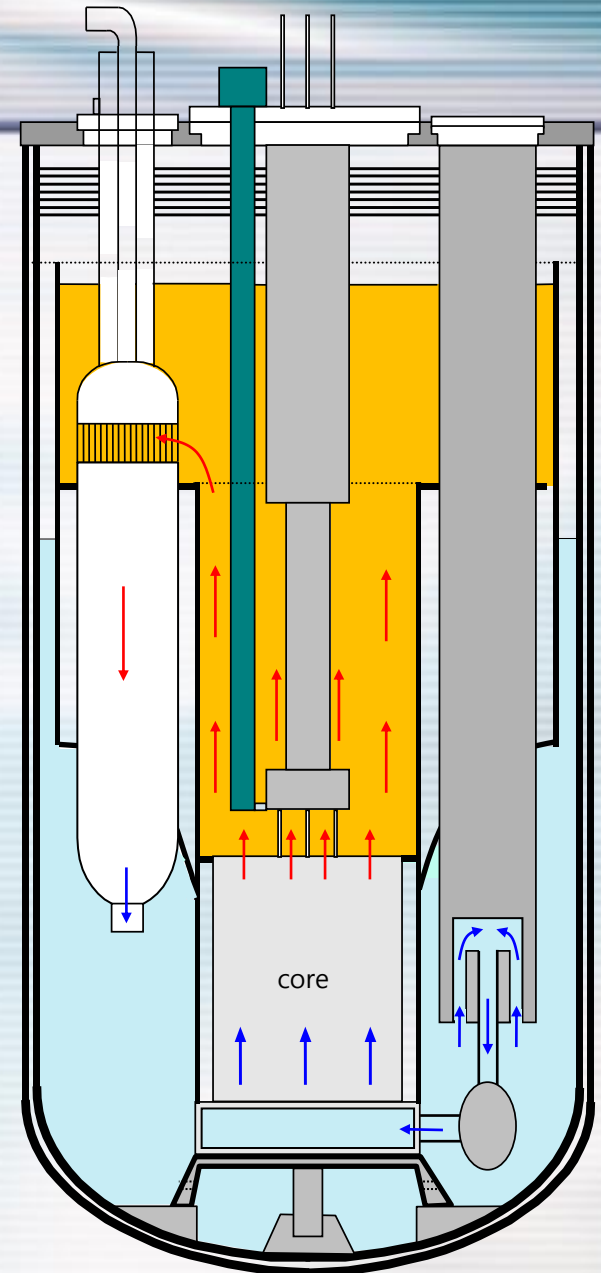
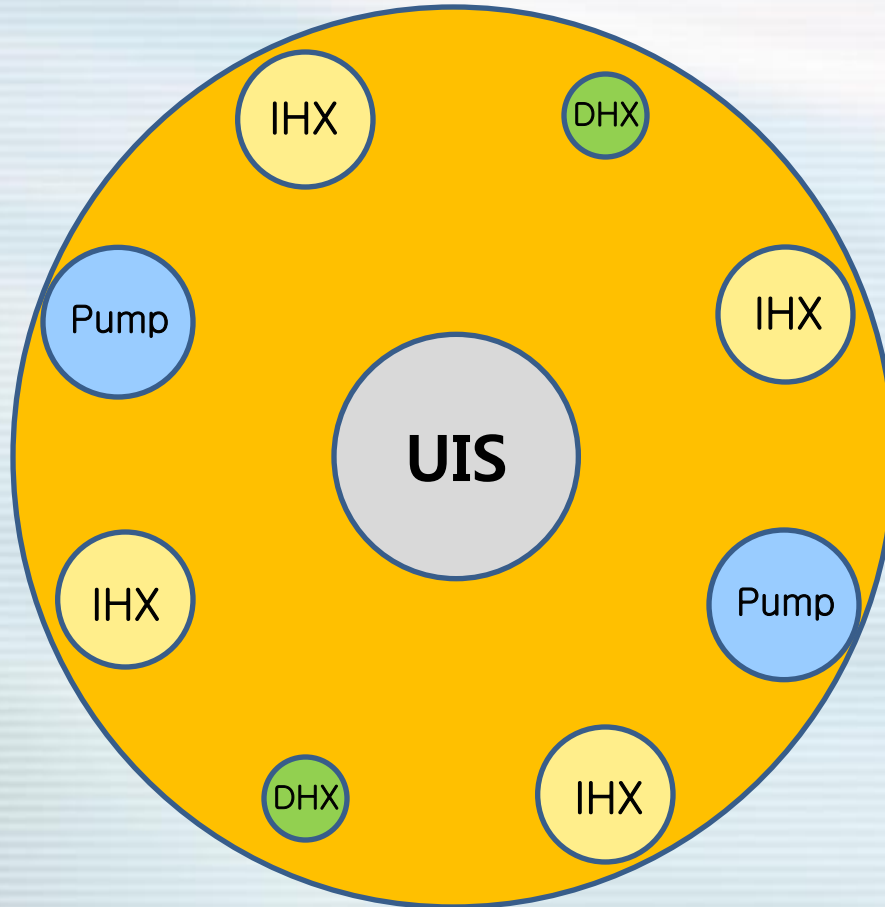
Multi-D Modeling



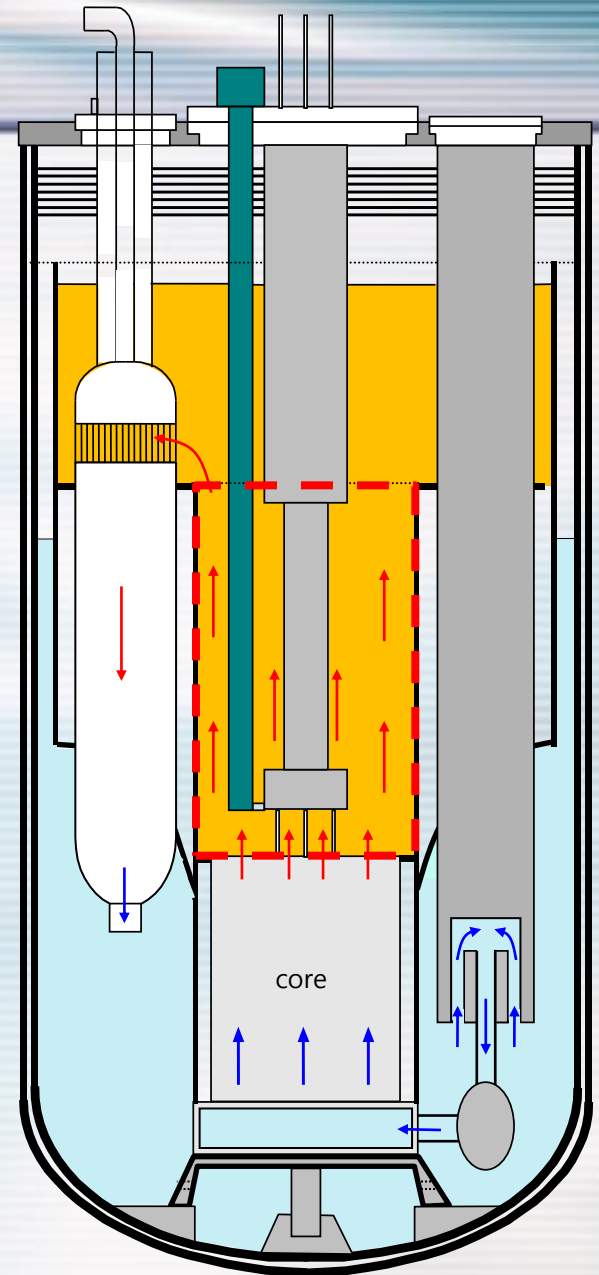
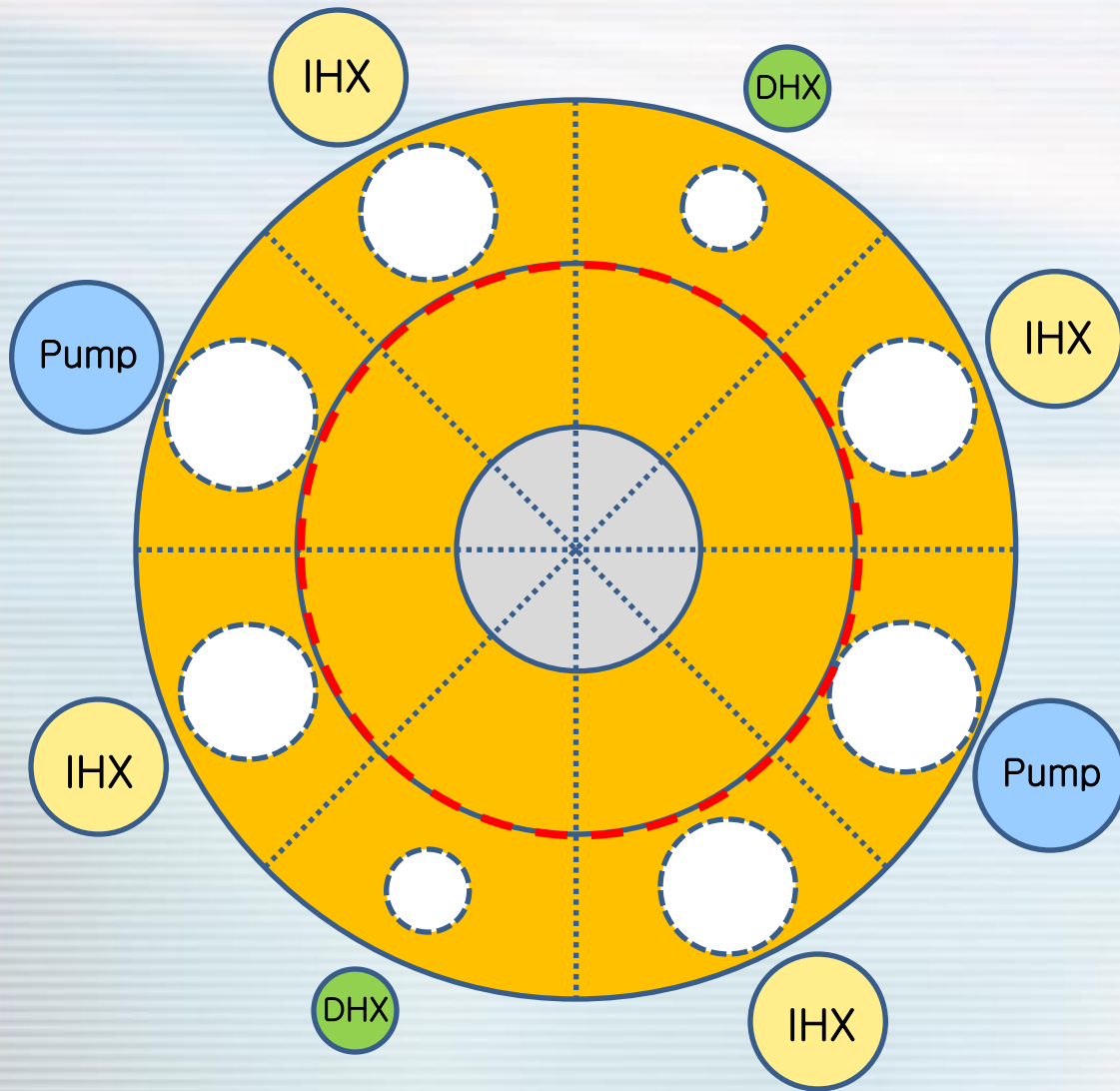
Multi-D Modeling

- **Development of Multi-Dimensional Analysis**
- **Evaluation of whole SFR System with MARS**
- **Hot Pool Coolant Temp. Distribution**
- **Pressure, Velocity & Flow direction**
- **More Accurate Evaluation of Safety**

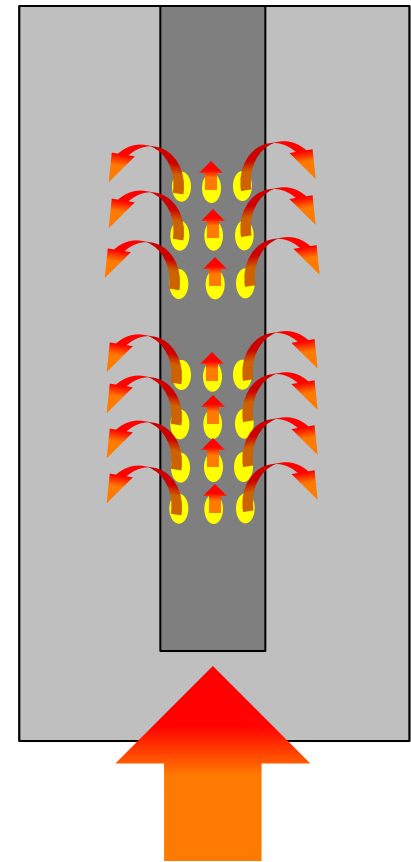
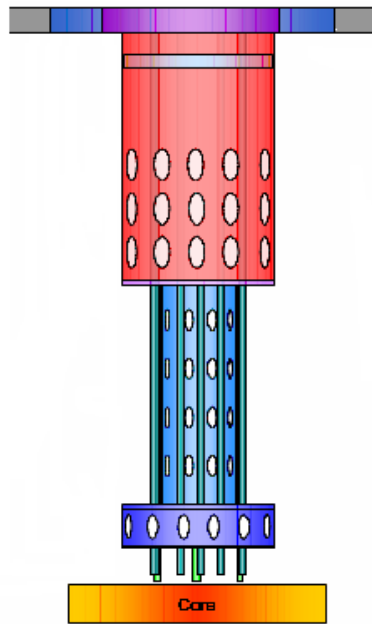
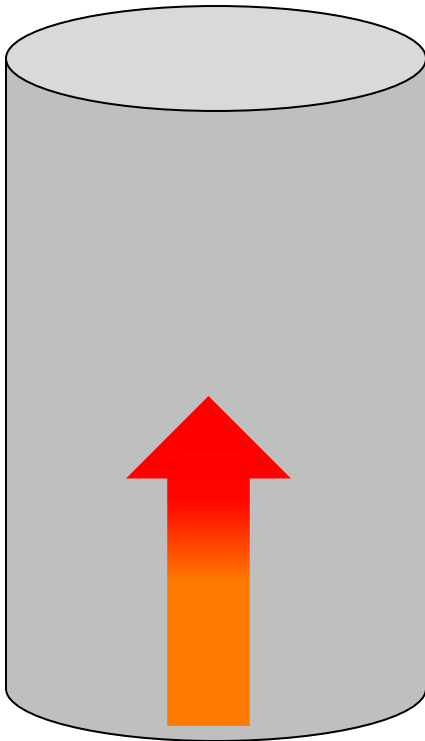
Multi-D Modeling



Multi-D Modeling



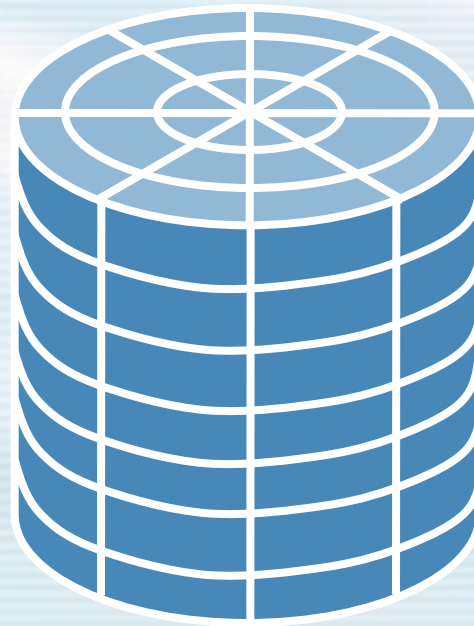
Multi-D Modeling



Multi-D Modeling

Angle	[°]
θ	45°

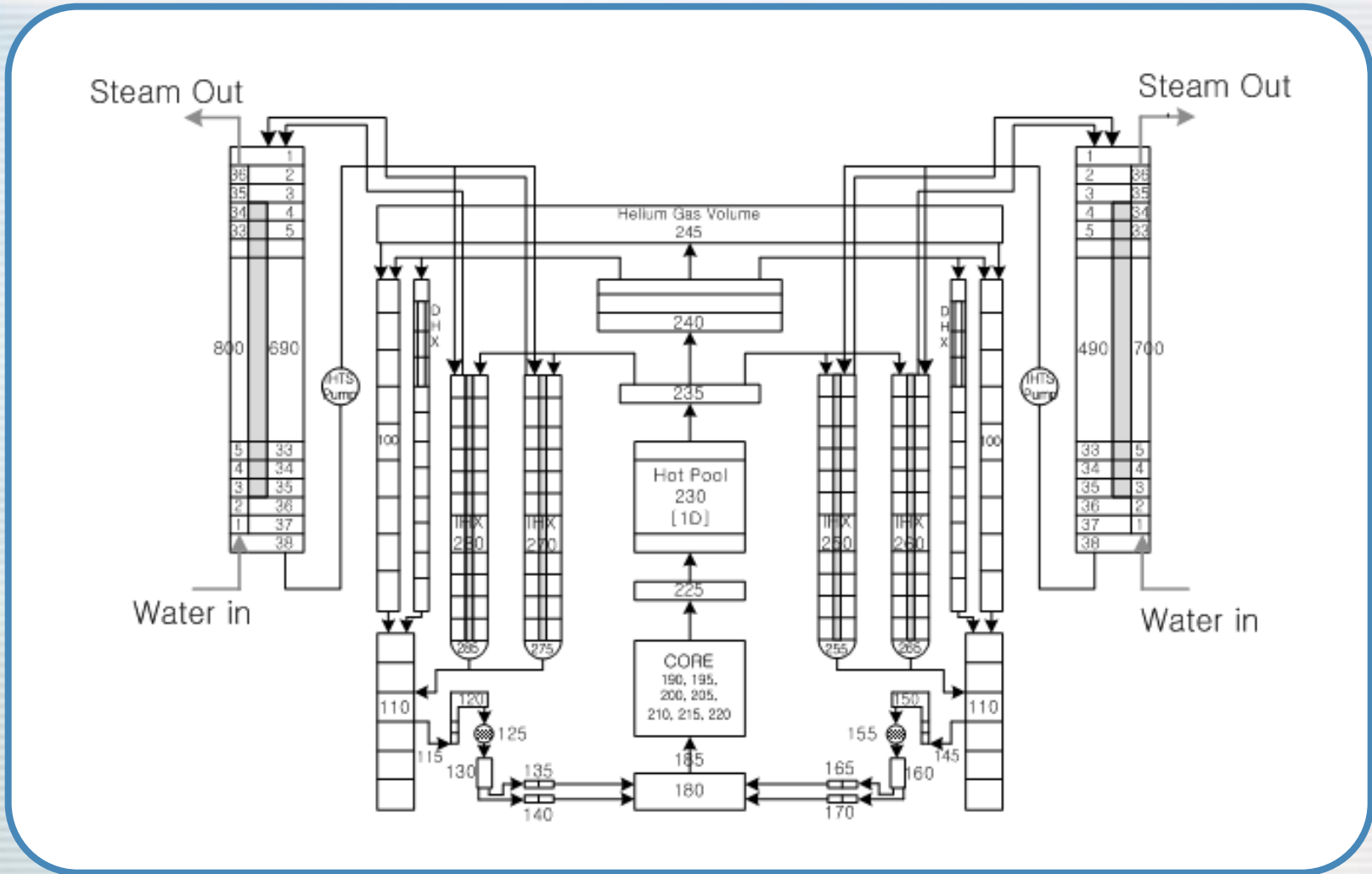
Height	[m]
Z7	0.3
Z6	0.67
Z5	0.795985
Z4	0.795985
Z3	0.795985
Z2	0.795985
Z1	0.795985



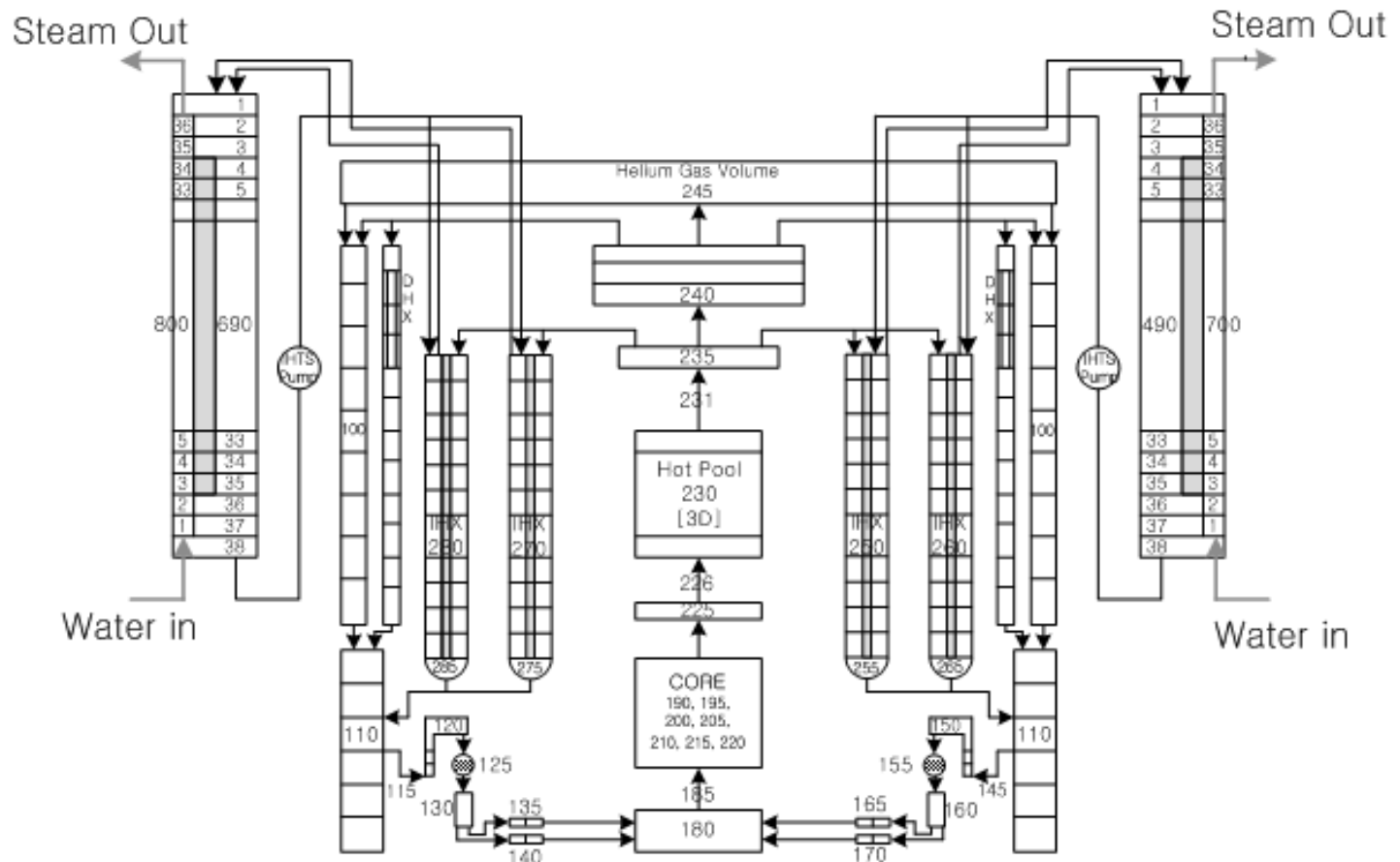
Radius	[m]
R1	0.6→1.5
R2	1.6→1.0
R3	0.8→0.32



Multi-D Modeling

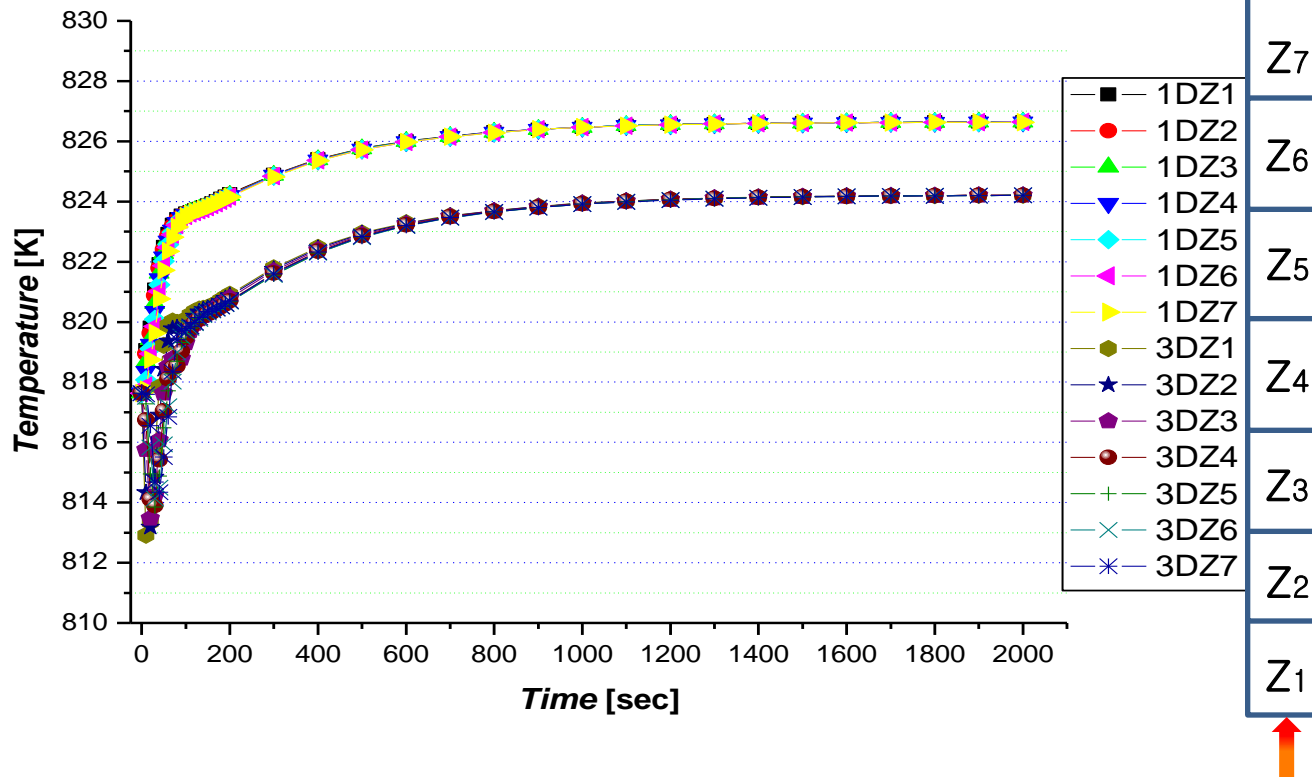


Multi-D Modeling



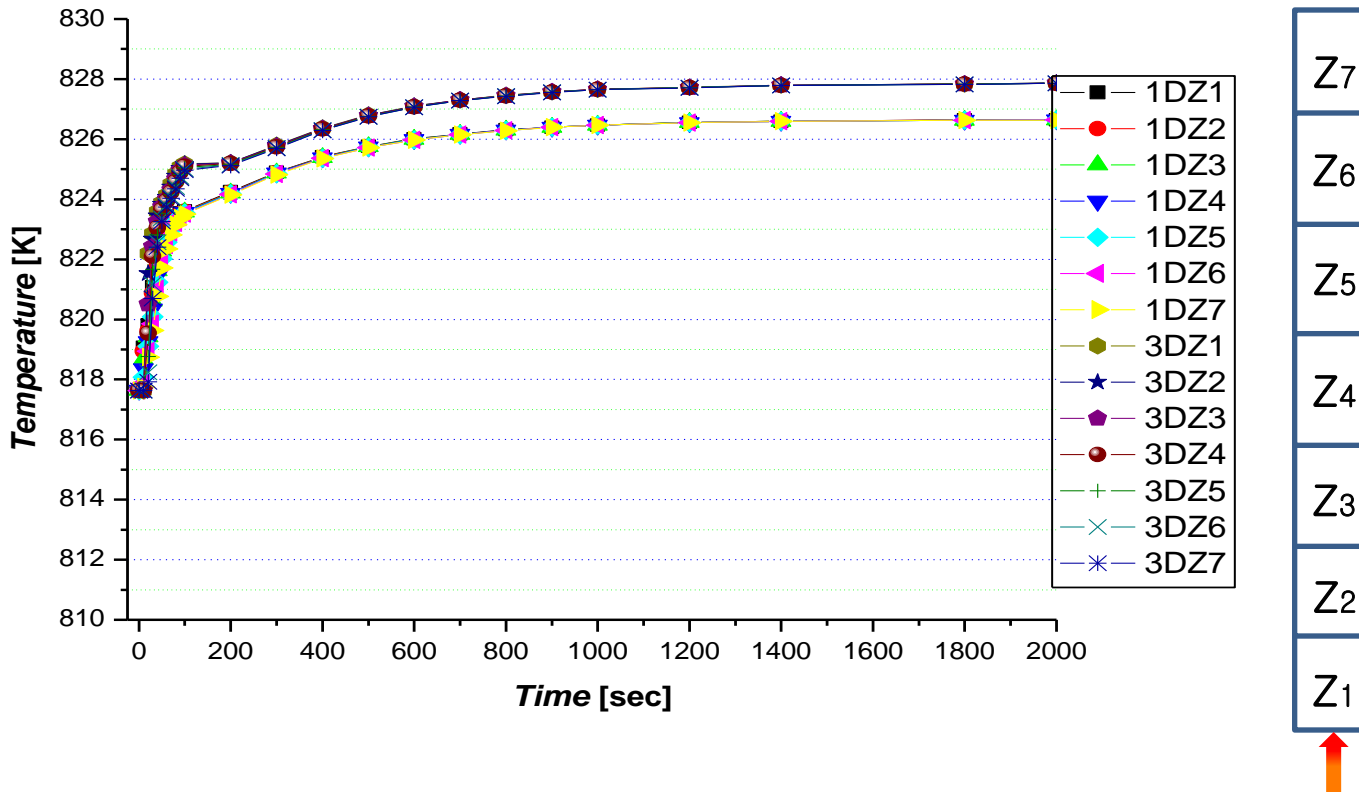
Result

Temp-Pre



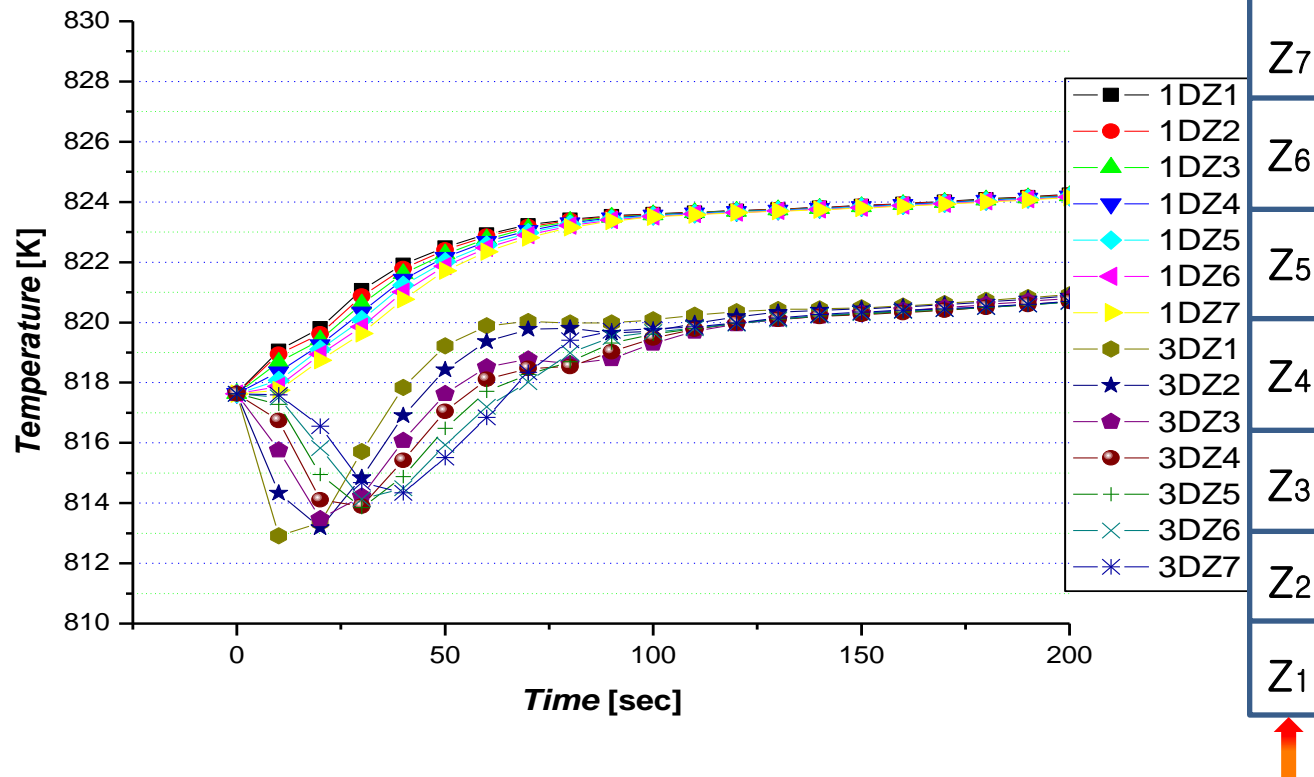
Result

Temperature



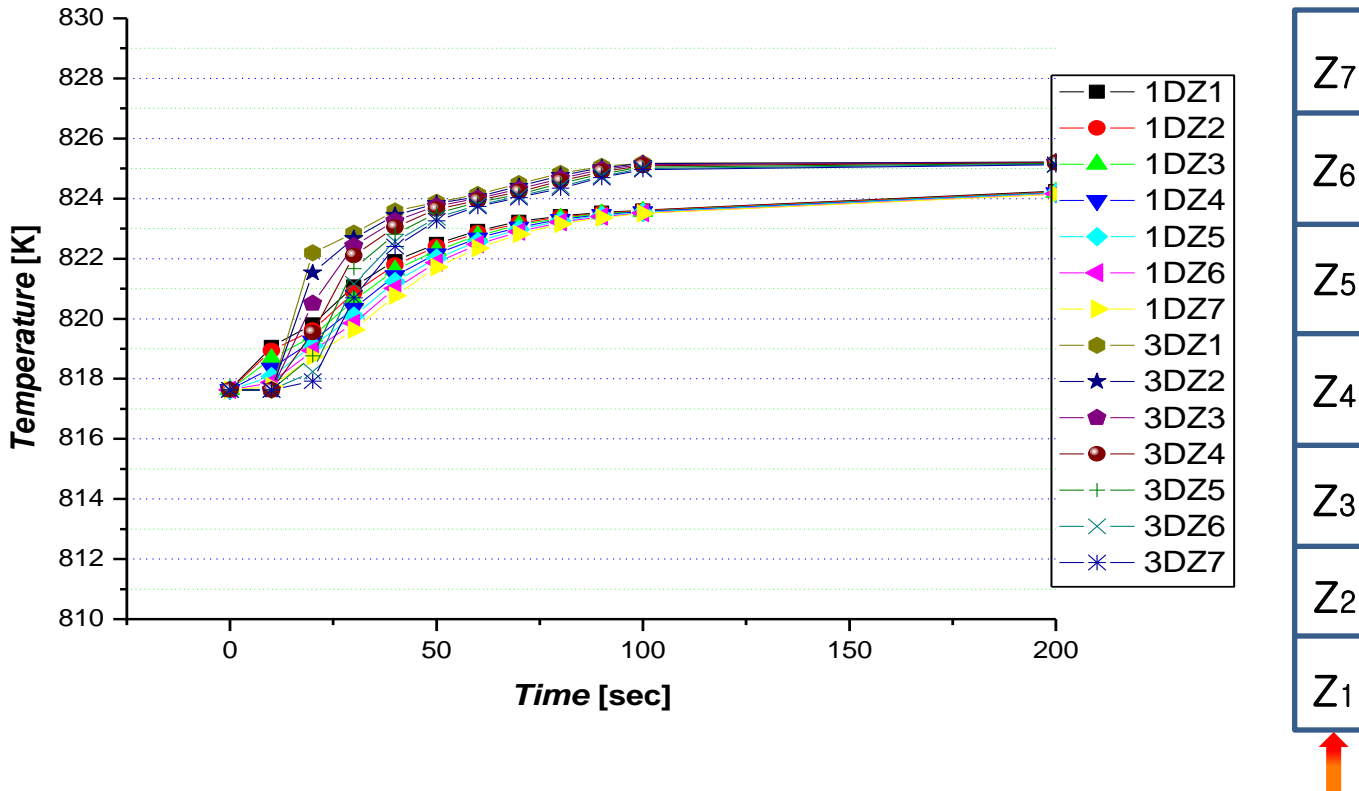
Result

Temp-Pre



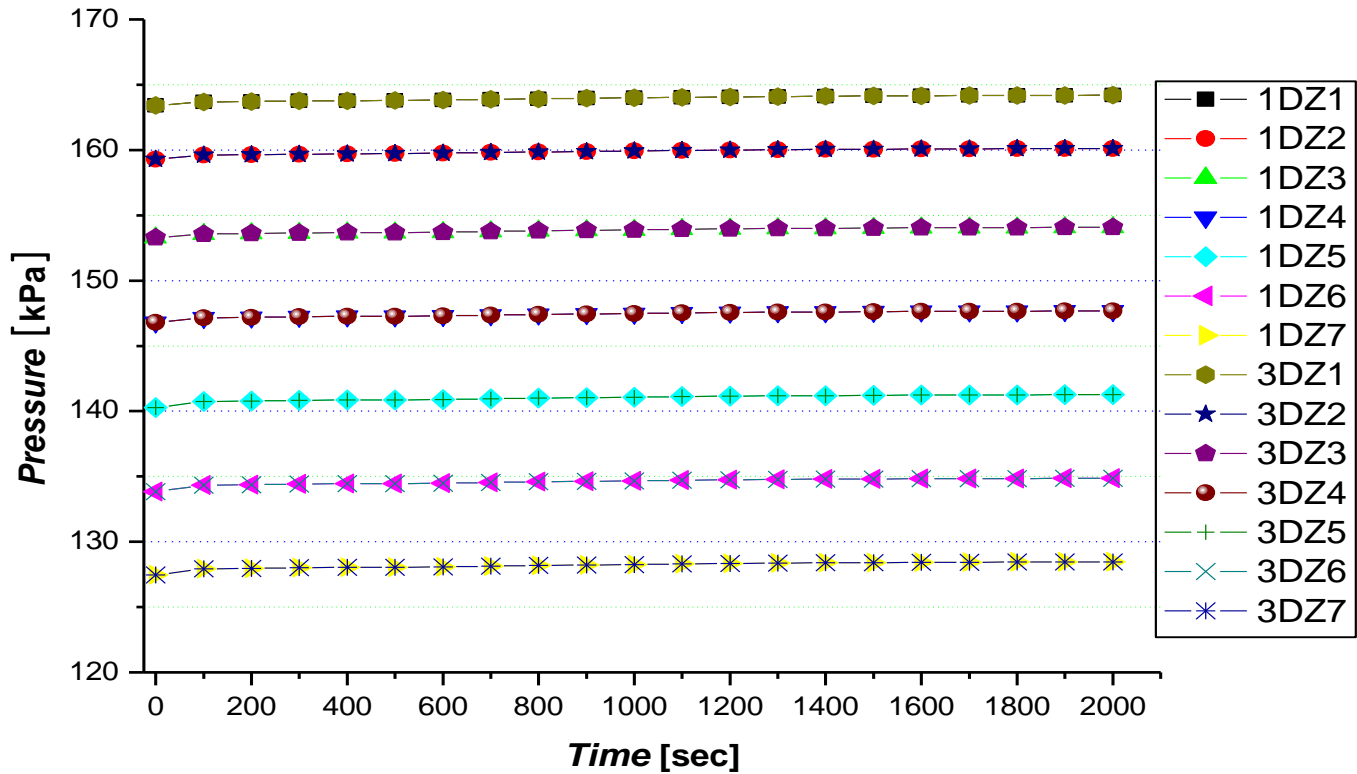
Result

Temperature



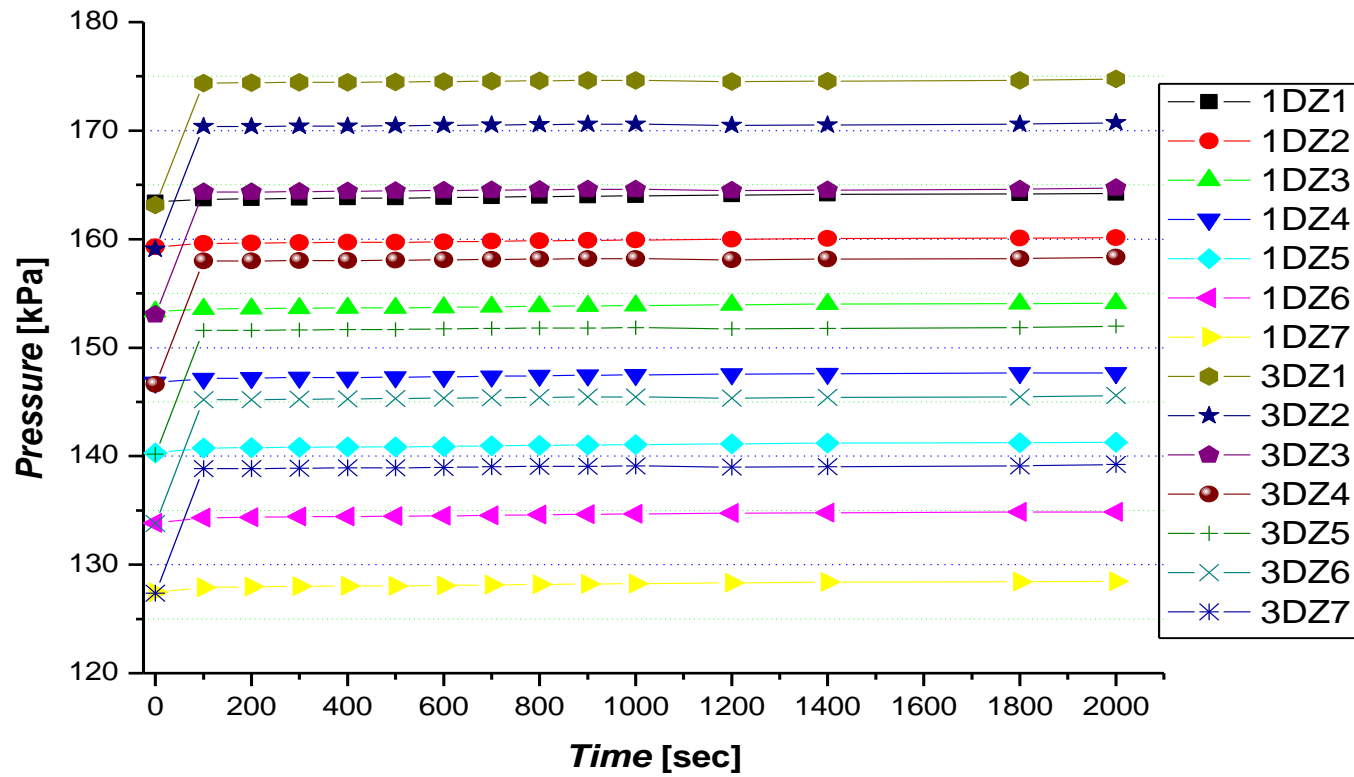
Result

Pres.-Pre



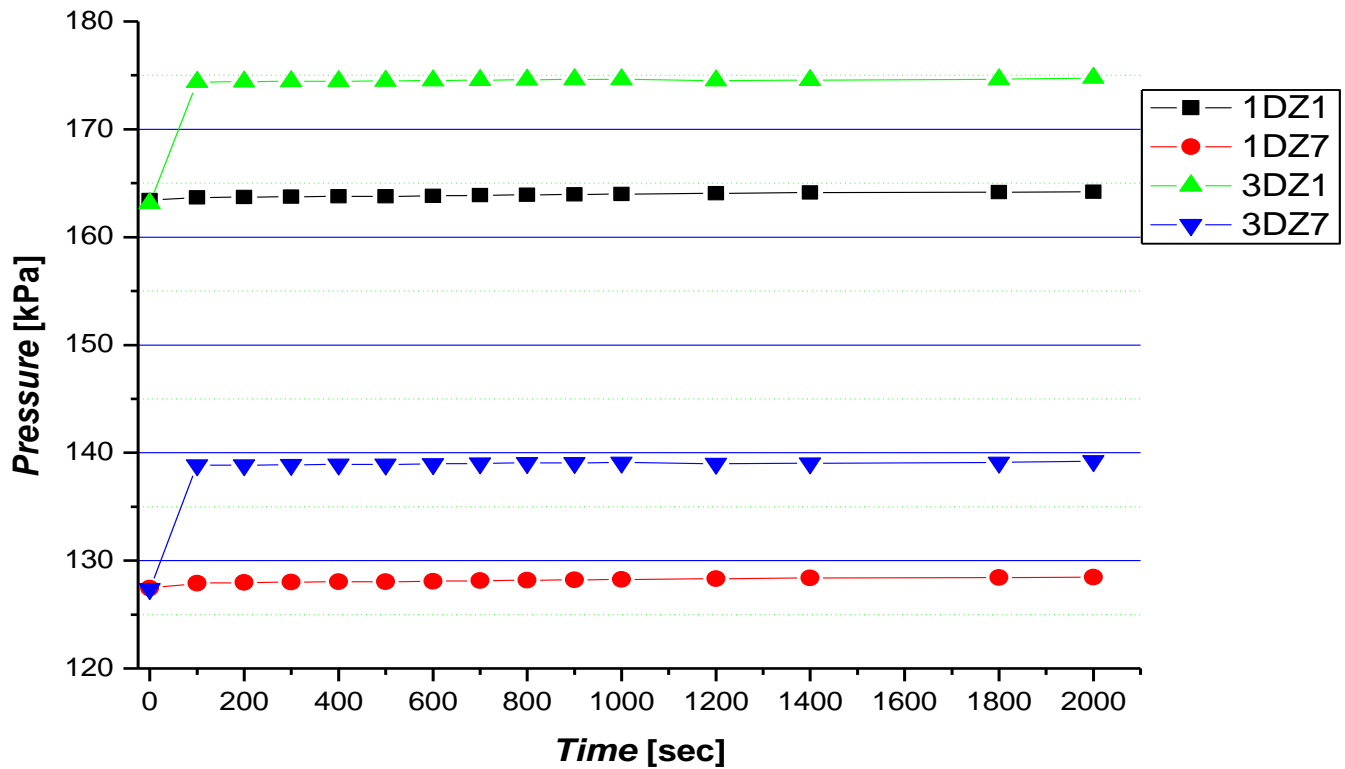
Result

Pressure



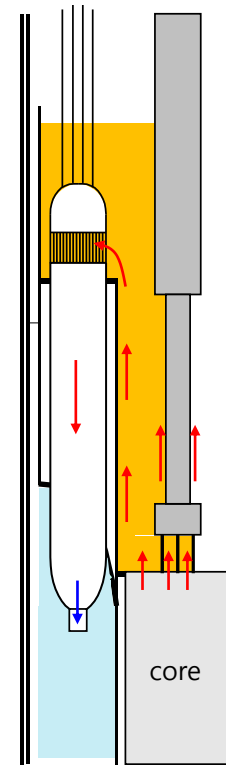
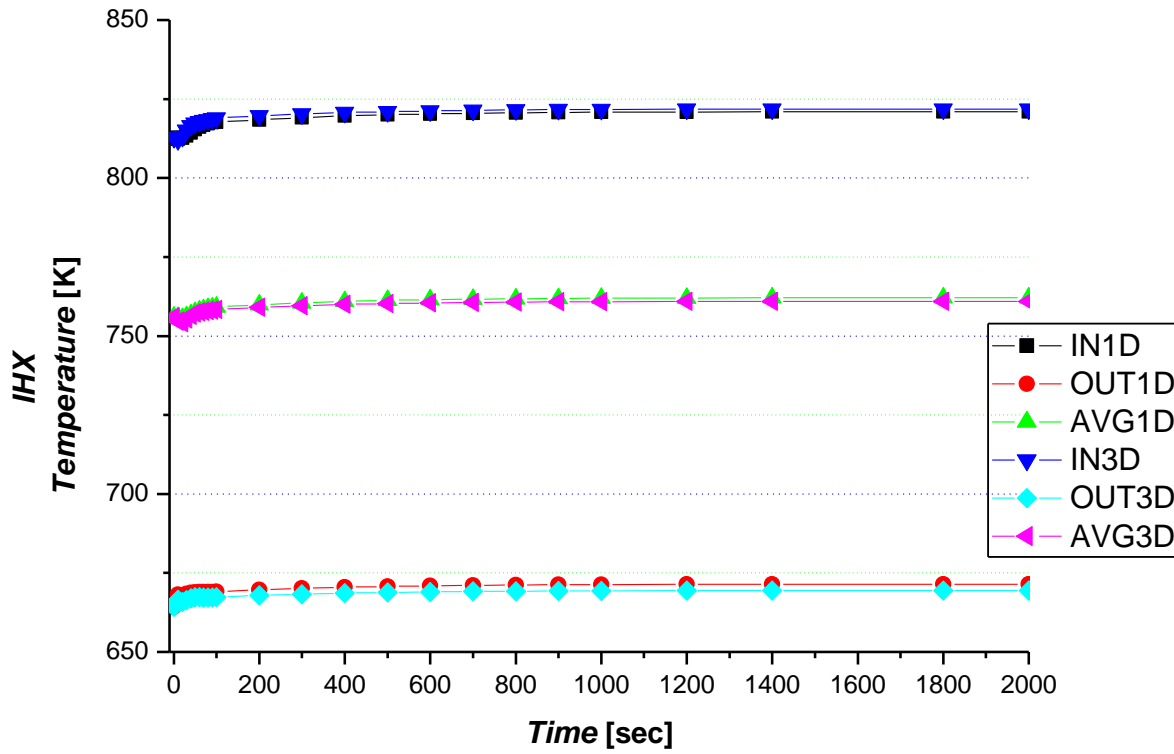
Result

Pressure



Result

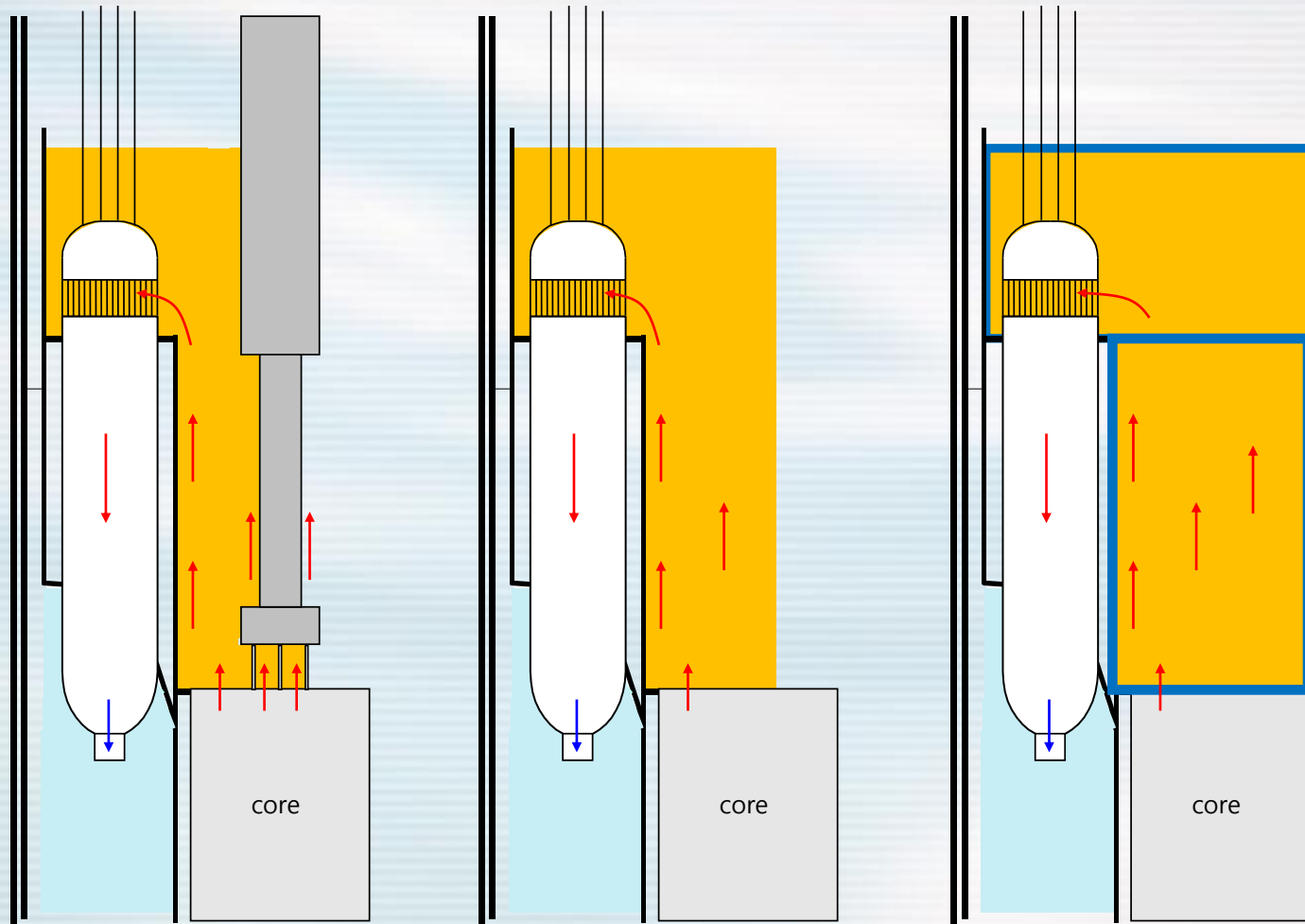
IHX



Discussion

- **Replace to 3D Hot pool & Consideration of UIS**
- **Temperature, Pressure and flow distribution**
- **Study about Multi-D of MARS CODE**
- **Modify to One Hot pool model**
- **Analysis of Transient condition**
 - **UTOP** (Unprotected Transient OverPower events)
 - **ULOF** (Unprotected Loss of Flow)
 - **ULOHS** (Unprotected Loss of Heat Sink events)
(Loss of the intermediate Loop)

Discussion



END

Thank you for your attention