



# CARBON RECYCLE HYDROGEN CARRIER SYSTEM USING NUCLEAR POWER

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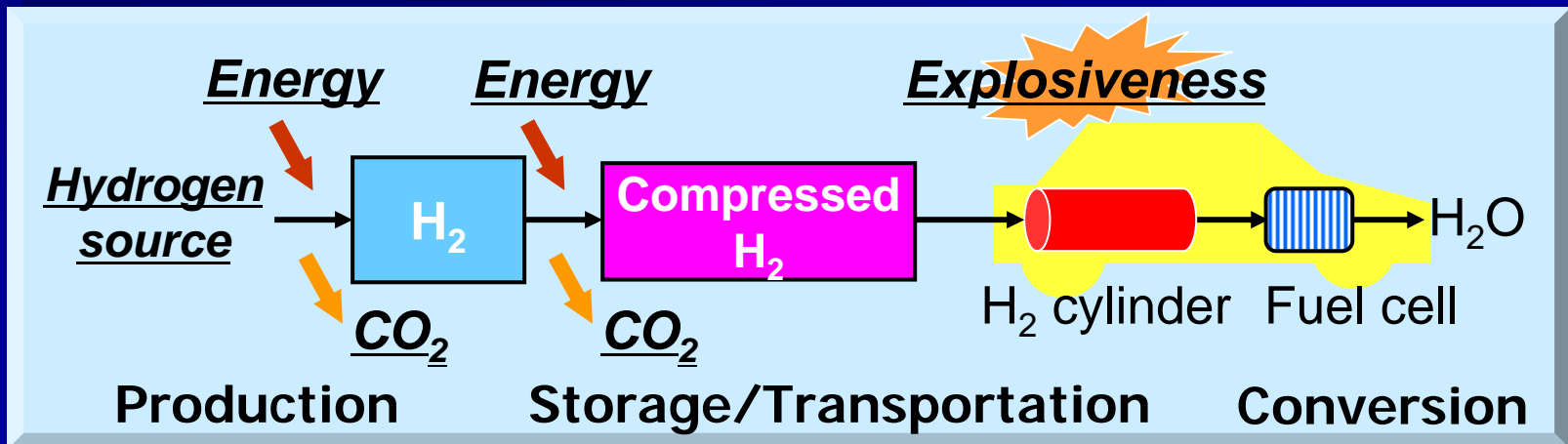
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# Hydrogen supply for fuel cell vehicles

# Hydrogen as an energy carrier

- Hydrogen(H<sub>2</sub>) is vital as a non-electricity energy carrier
- H<sub>2</sub> is a promising energy source for vehicles
  - Fuel for fuel cells
  - Liquefaction of tar-sand, crude-oil, coal and bio-mass.  
Hydro-cracking:  $C_nH_m + nH_2 \rightarrow nCH_4$
- Issues for H<sub>2</sub> system: Production energy and delivery
  - Consistency from production to use

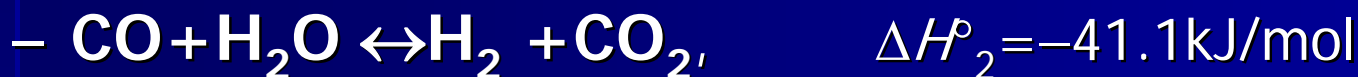


# **Carbon recycle hydrogen carrier system**

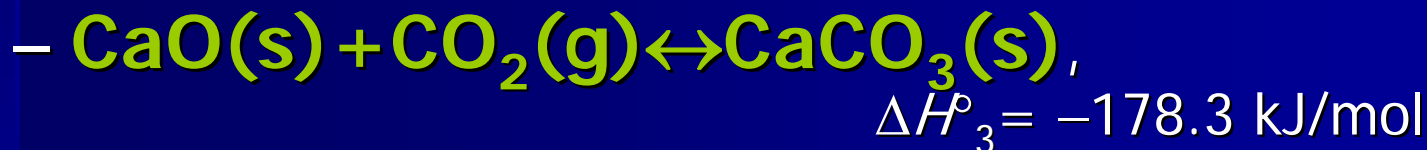
# Regenerative Reforming

## -Use of chemical absorption-

- Fuel reforming for methane

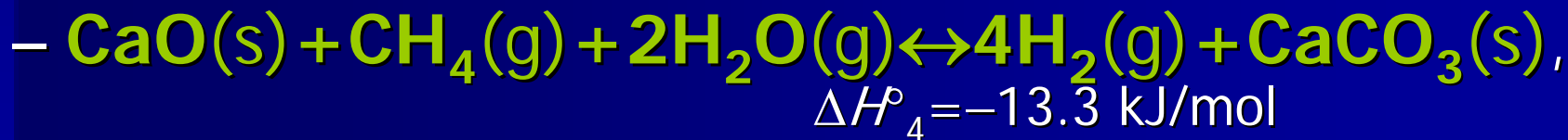


- CaO carbonation



- Regenerative reforming

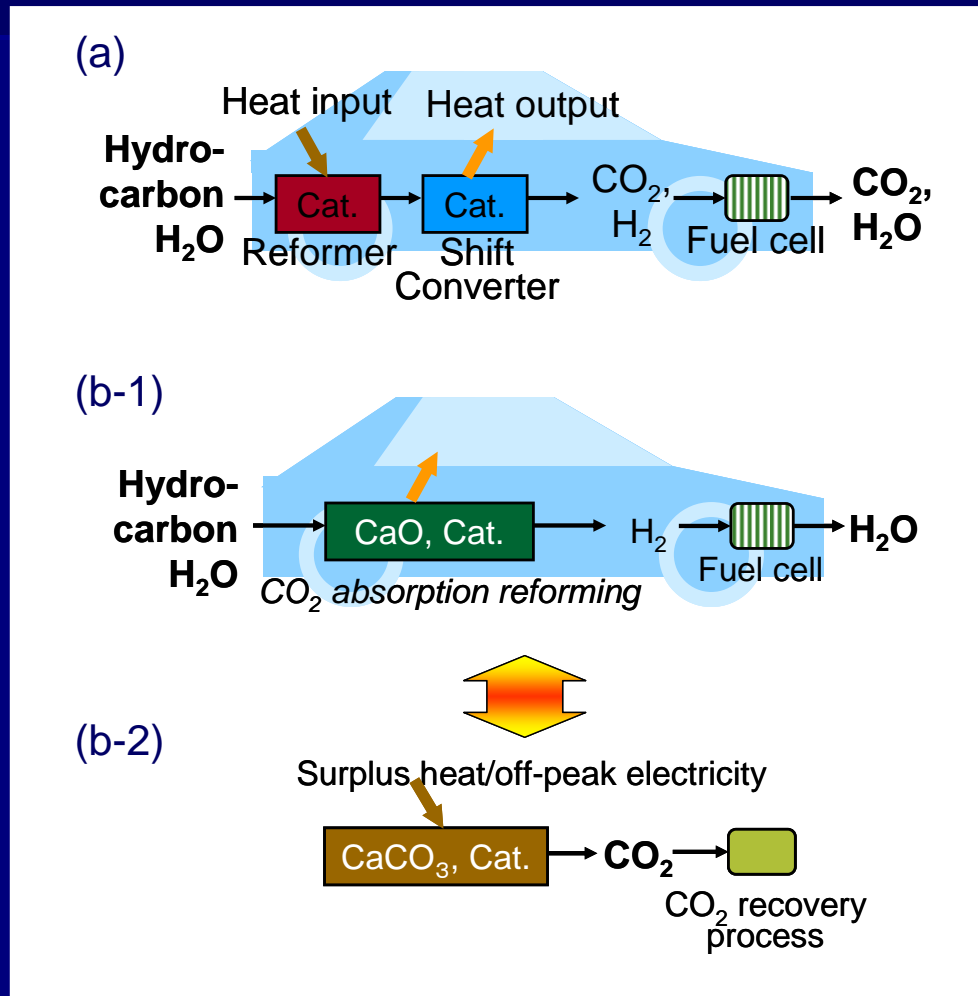
(CO<sub>2</sub> absorption reforming, self-heating)



# CO<sub>2</sub> zero-emission FC vehicle

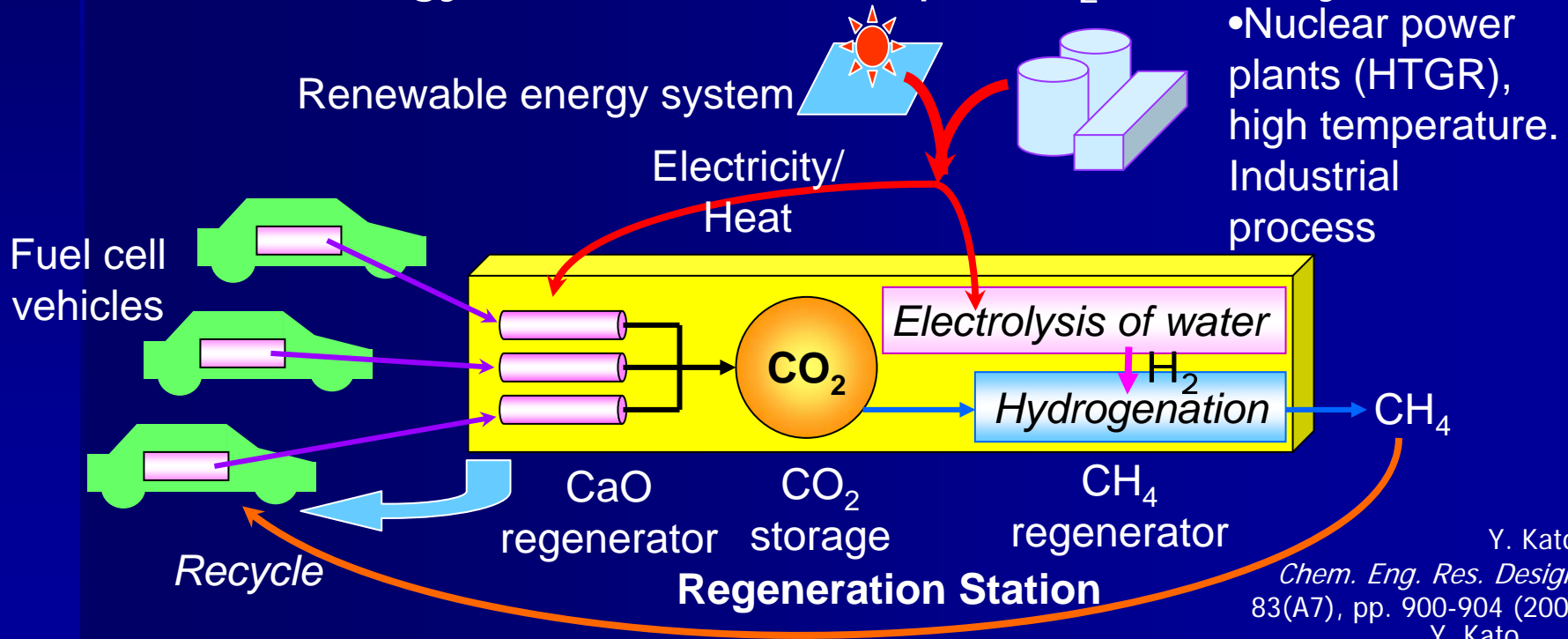
- Regenerative reforming
  - CO<sub>2</sub> recoverable, self heating, and simple reforming system
  - thermally regenerative
- CO<sub>2</sub> zero-emission FC vehicle
- Safety H<sub>2</sub> carrier system under low-pressure and high-density

Figure 1. Concept of a zero CO<sub>2</sub> emission FC vehicle using a thermally regenerative reformer; (a) conventional reforming, (b-1,2) proposed thermally regenerative reforming, (b-1) reforming mode, (b-2) regenerating and CO<sub>2</sub> recovering mode



# Carbon recycle type nuclear hydrogen carrier system

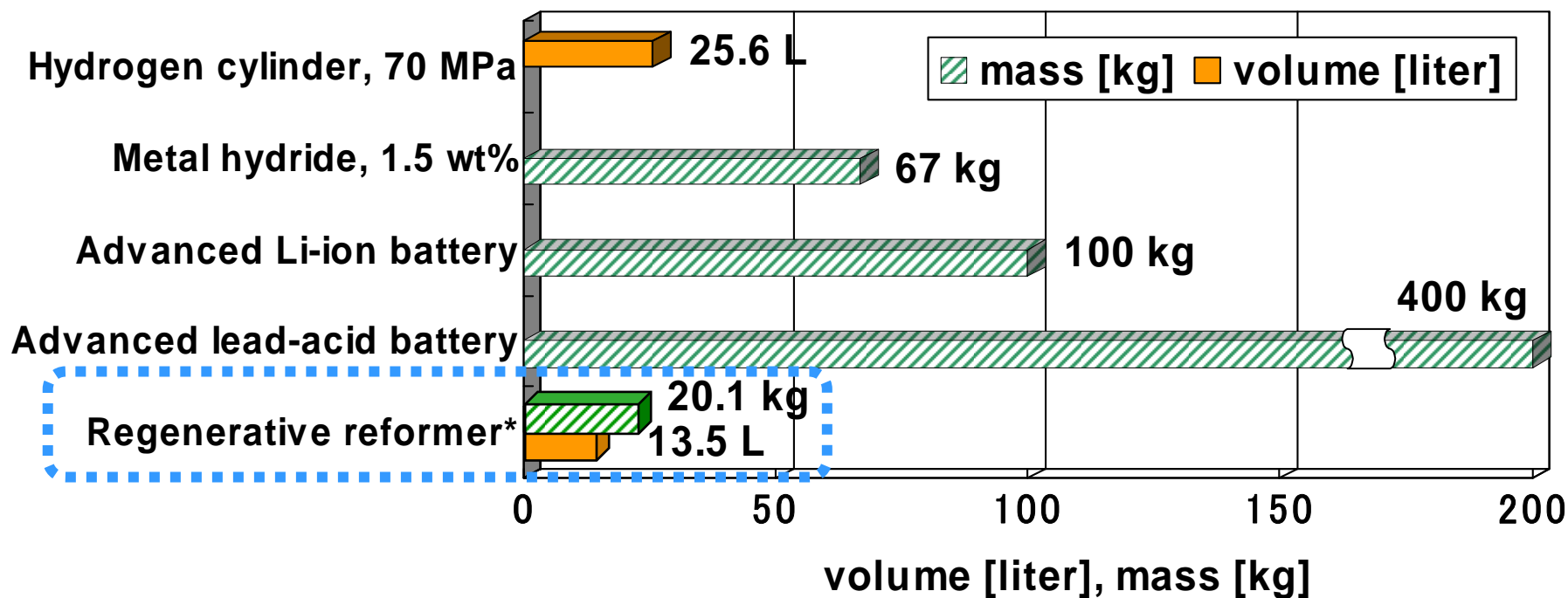
- $\text{CaO} + \text{CH}_4 + 2\text{H}_2\text{O} \rightarrow 4\text{H}_2 + \text{CaCO}_3$ :  $\text{CO}_2$ -free barge-mounted reforming
- Use of redundant output at off-peak from NPPs
- Safe, energy-efficient and compact  $\text{H}_2$  carrier systems





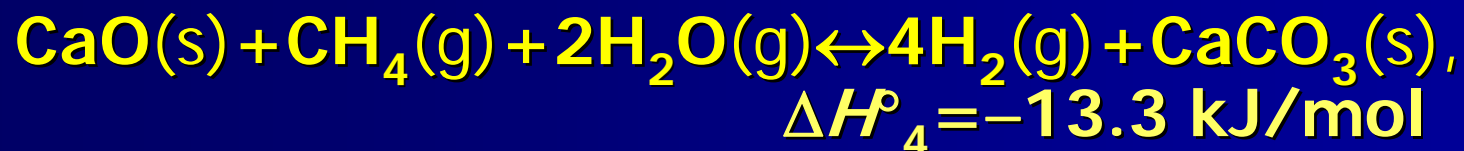
# Comparison between H<sub>2</sub> systems

Table: Scale of energy storage facilities for 100 km mileage, 14.7 kWh, 500 mol-H<sub>2</sub> (= Petroleum of 4 L, 2.8 kg)



(\*total reactant amount including CaO, H<sub>2</sub>O and liquefied CH<sub>4</sub> assuming under 3.86 MPa and at -88°C).

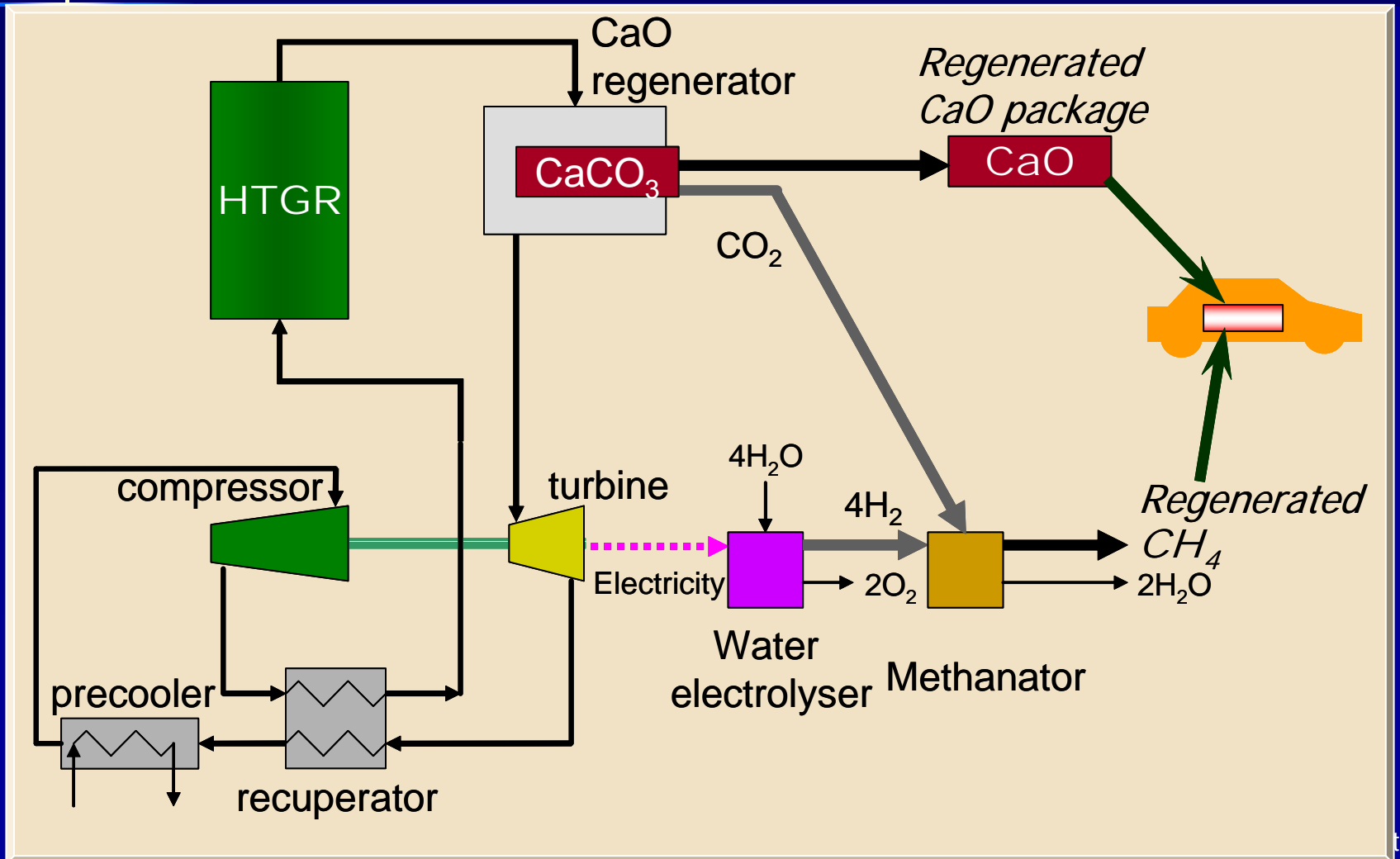
# Merits of Carbon recycle type H<sub>2</sub> carrier system



- CO<sub>2</sub> removing induces the reforming state into non-equilibrium
- Reaction enhancement by non-equilibrium
  - Enhancement of H<sub>2</sub> production yield
  - Reduction of reforming temperature
- Self heating
- CO<sub>2</sub> recoverable
- Elimination of compression work and explosion risk for hydrogen supply

# The hydrogen carrier system with HTGR

# Combination of the H<sub>2</sub> carrier system and HTGR



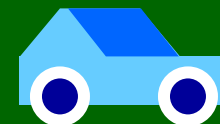
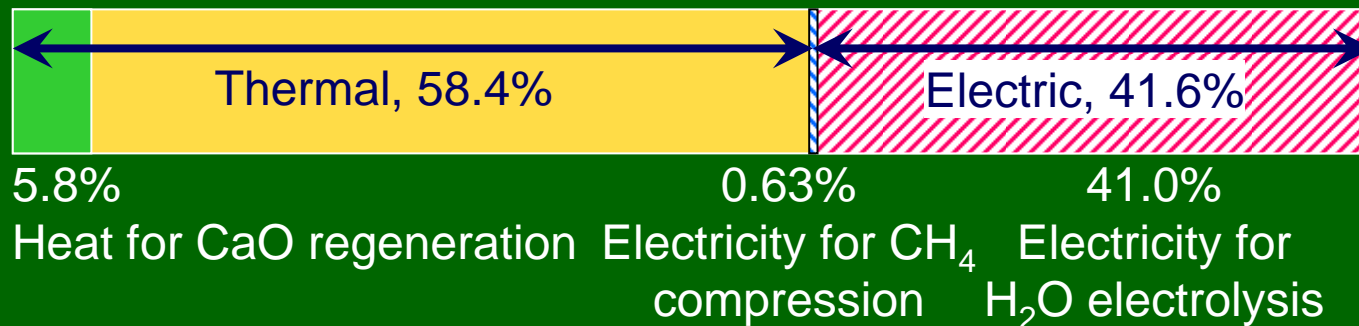
# The H<sub>2</sub> carrier vs. H<sub>2</sub>O electrolysis

## (2) HTGR system (GTHTR300)

	Proposed H <sub>2</sub> carrier system	Conventional water electrolysis system
HTGR thermal power <sup>1</sup>		600 MWt
Outlet coolant temperature from HTGR		850 °C
HTGR operation duration for hydrogen processes		8 h/day
Inlet/outlet coolant temperature for CaO	850 / 835 °C	-
Inlet/outlet coolant temperature for gas-turbine	835 / 587 °C	850 / 587 °C
Power input for CaO regeneration	34.8 MWt	-
Plant power input for gas-turbine power	565.2 MWt	600.0 MWt
Gas-turbine power efficiency <sup>2</sup>	44.3 %	45.0 %
Water electrolysis efficiency (□H base) <sup>3</sup>		90 %
Compression pressure	175 bar-CH <sub>4</sub>	700 bar-H <sub>2</sub>
Power for H <sub>2</sub> electrolysis	245.8 MWe	247.1 MWe
Power for compression	3.8 MWe-CH <sub>4</sub>	22.9 MWe-H <sub>2</sub>
H <sub>2</sub> production/equivalent	2.26E+07 H <sub>2</sub> -mol equ	2.27E+07 H <sub>2</sub> -mol
Number of FC vehicles for 100 km mileage each <sup>4</sup>	4.52E+04 -	4.54E+04 -

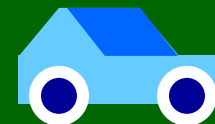
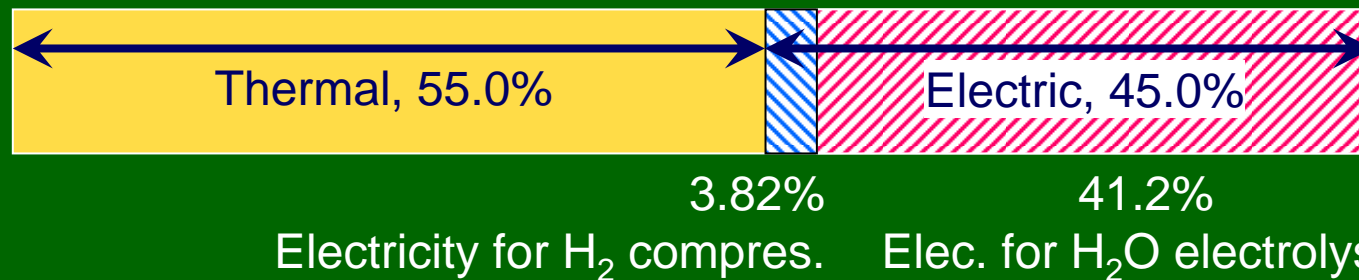
# Enthalpy balance of the H<sub>2</sub> carrier & H<sub>2</sub>O electrolysis systems based on HTGR

## Carbon recycle hydrogen carrier system



1.356x10<sup>5</sup> cars/day  
784 mol/s

## Conventional hydrogen production, Water electrolysis



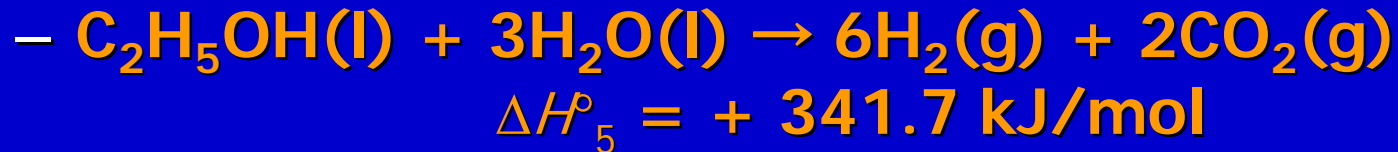
1.363x10<sup>5</sup> cars/day  
789 mol/s

**Fig. Enthalpy consumption ratio of HTGR output (600 MWt, 8h/day) for both systems**

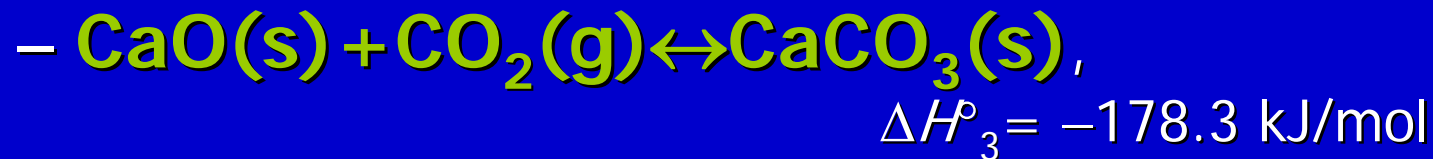
The carrier system : Reduction of compression pressure & work and transportation risk with consisting the same efficiency of conventional H<sub>2</sub> system  
> Safe and compact H<sub>2</sub> carrier system

# Application of the regenerative reforming to ethanol and biomass

## ■ Fuel reforming for Ethanol

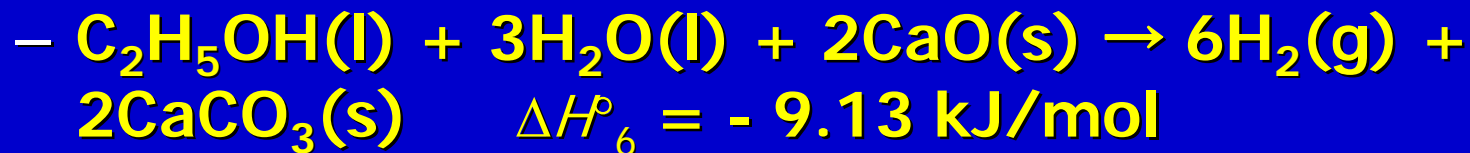


## ■ CaO carbonation



## ■ Regenerative reforming

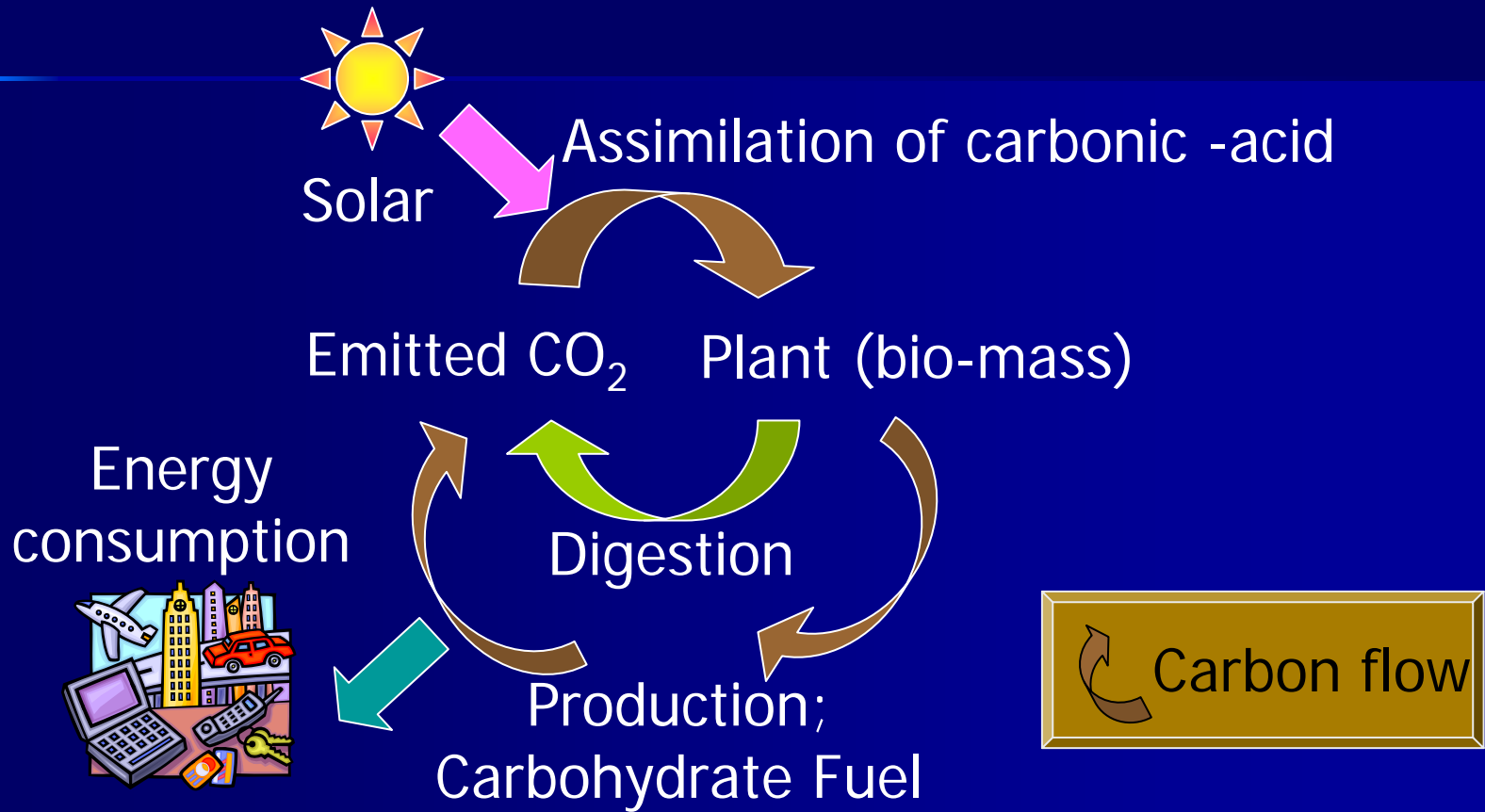
(CO<sub>2</sub> absorption reforming, self-heating)



# **Synergy of bio-mass and nuclear for H<sub>2</sub> supply**

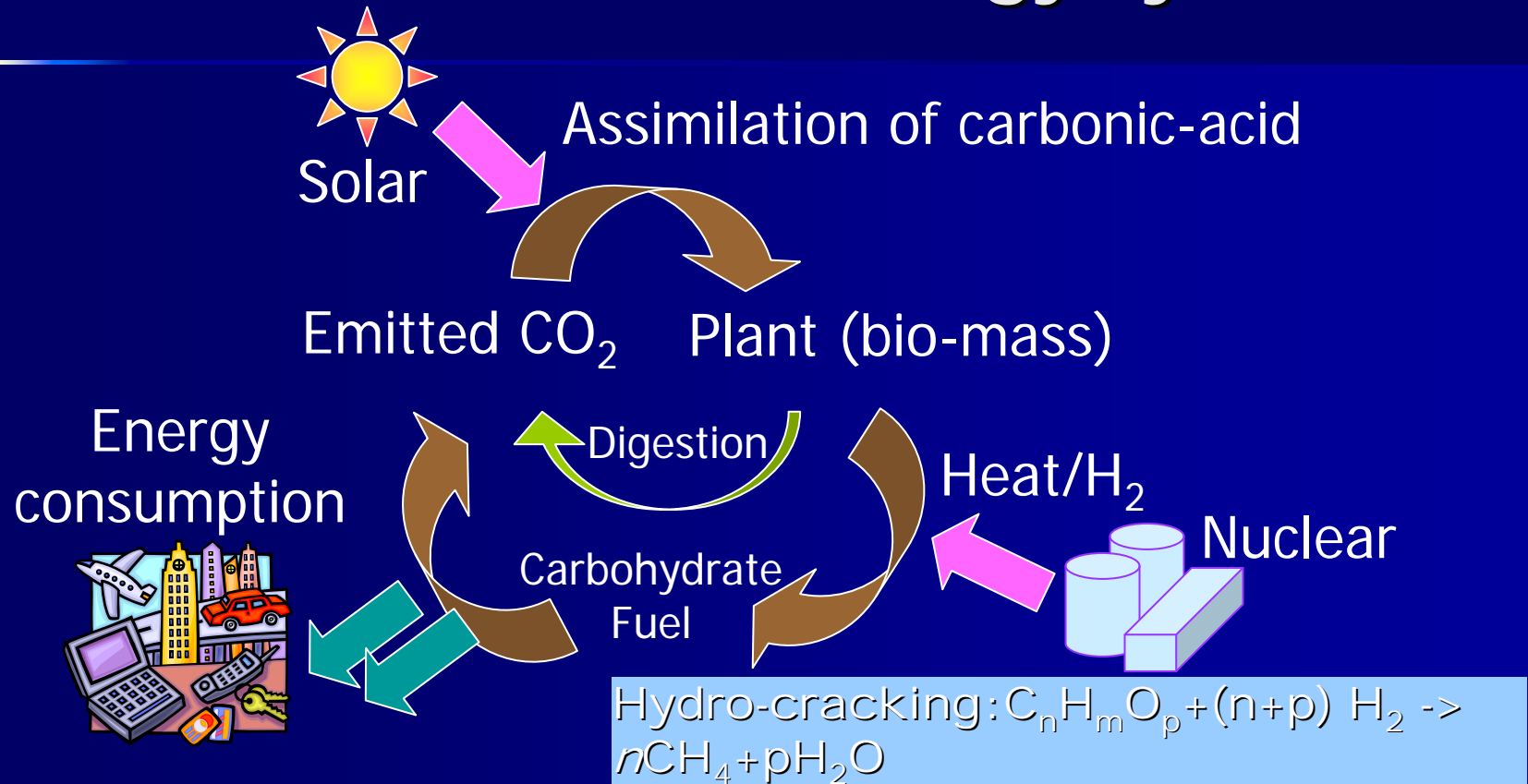


# Carbon neutral energy system



Forests and farms maintain air-borne CO<sub>2</sub> at constant by recycling in the carbon neutral cycle, while converting solar power to energy

# Synergistic system by carbon neutral and nuclear energy systems



- Increasing carbohydrate fuels by synergistic combination of carbon neutral and nuclear H<sub>2</sub> systems
- CO<sub>2</sub> and H<sub>2</sub> are recycled in the synergistic neutral system



# Conclusions

- Carbon recycle type H<sub>2</sub> carrier system has possibility to realize efficient H<sub>2</sub> transportation by reduction of storage compression work, storage volume and fuel explosion risk.
- Total energy consumption is similar with conventional H<sub>2</sub>O electrolysis system.
- The carrier system have good compatibility with HTGR, and can utilize the top temperature part in the primary loop of HTGR
- Synergistic systems of carbon neutral and nuclear energy systems
- Choice of hydrogen source is limited by numbers of FC vehicles
  - First generation: Synergy of biomass and nuclear for hydrogen economy
  - Next generation: Carbon recycle H<sub>2</sub> carrier system using nuclear power

# Thanks!

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# CO<sub>2</sub> absorption reforming

- During the initial 60 min, hydrogen production was higher than the equilibrium concentration of conventional reforming.
- Charged CaO absorbed well CO<sub>2</sub> by carbonation. CO<sub>2</sub> <1%
- CO was removed, <1%
- Low-temperature reforming (conventional reform. temp. > 700°C)

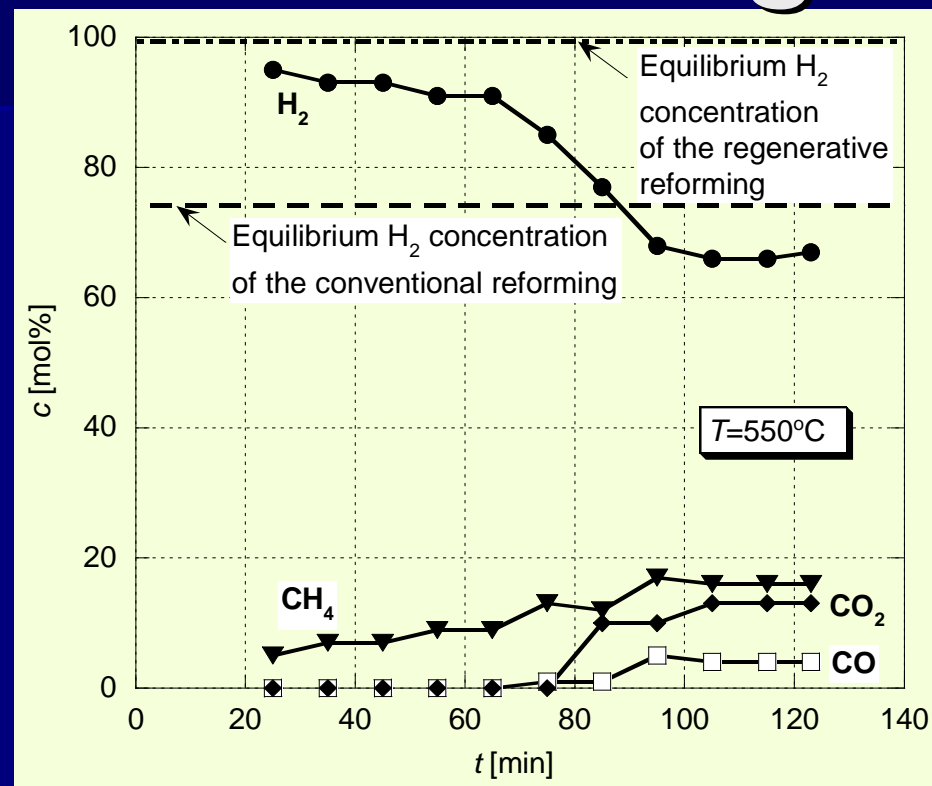


Fig. Temporal change of effluent composition of the regenerative reformer at 550°C

