

Elemental researches on the critical issue of laser fusion reactor KOYO-F

- Formation of aerosols, protection of beam port and flow stability -

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Abstract. Critical issues on laser fusion reactor with a liquid wall are discussed. Formation of aerosols after laser shot was studied experimentally and theoretically. Our simulation results for formation of aerosols agreed with experimental results obtained with electric discharge through a thin lead membrane. Formation of micro particles is discussed basing on experimental results obtained by backside irradiation of a lead membrane. Protection of beam ports of the laser fusion reactor with a liquid first wall is described. A magnetic field generated with a pulse current successfully shielded the tip of beam ports from alpha particles. A continuous protective liquid LiPb flow controlled with cascade scheme was formed as the protective first wall of KOYO-F.

1. Introduction

Many concepts for inertial fusion reactor were reported during 1975 through 1980. HYLIFE II for heavy ion beam was continuously studied[1]. The ARIES-IFE team reported many modern, useful papers, which can be seen on a web site[2]. ILE Osaka and the IFE Forum organized a laser fusion reactor design committee to conceptually design the laser fusion power plant KOYO-F based on fast ignition scheme and the result was reported at IAEA-FEC 2006[3]. KOYO-F has a liquid LiPb flow as the first protective wall[4]. After the activity of the committee, we concentrated elemental researches on the issues to increase the reliability of the concept under co-lateral collaborations with other universities. Formation of aerosols and micro particles was studied at ILE Osaka University and ILT Osaka. The researches include two types of experiments on formation of aerosols and micro-particles produced by hydrodynamic instabilities during the ablation process. In the case of KOYO-F, the alpha load on the first wall is about 0.35 MJ/m^2 in $0.1 \mu\text{sec}$. As the result,

10 kg of LiPb evaporates after fusion burn. Major part of ablated material condenses on the surface of opposite wall. Some part of evaporated vapor stagnates at the center of the target chamber and, in the worst case, the stagnated vapor makes lot of liquid droplets at the center, which would disables a high repetition rate. Protection of beam ports is another important issue. Use of a thin liquid LiPb membrane fed through a porous wall would be the solution[5] but some protective mechanism is desired to increase the reliability. We propose use of a magnetic field to reduce the thermal load on the tip of the beam port. The scheme was numerically studied at the Kyushu University and the Kyoto University. Stability of liquid LiPb flow is experimentally and numerically investigated at Kyoto University. When the surface flow is a simple laminar flow, the surface temperature becomes too high to evacuate the chamber by cryogenic effect in designated time of 0.25 sec. The surface flow must be mixed with the inner cold flow to keep the temperature low. A cascade flow was proposed but the stability of flow as the protective first wall was not clear at the time.

2. Aerosols and Micro Particles

2.1 Discharge method

It is quite difficult to experimentally simulate the ablation process and formation of aerosols by alpha particles in the wet wall reactor. Up to date, numerical simulation is a good tool to understand the processes. We employed discharge method to check the simulation code.

A 5-mm-wide, 10-mm-long, 10- μm -thick, Pb ribbon target was heated to 3000 – 4000 K in 100 μs by an electric discharge from a 150 μF , 2kV capacitor. [6] The target was 10 μm thick Pb membrane coated on a glass plate by physical vapor deposition. The glass plate was regarded as cold LiPb beyond the Bragg's peak. Evaporated materials were deposited on glass witness plates located 10 – 20 mm apart from the source. The spatial distribution of temperature was monitored by using a charge-coupled device (CCD) camera equipped with band-pass filters that were inserted in front of the pinholes to disperse the plasma emission at 460 nm and 660 nm in order to determine the color temperature. Morphology of deposited materials was observed with a SEM and the average thickness was measured from the intensity of fluorescent x-ray stimulated with a collimated Cu-K x-ray beam from a tube.

Figure 1 shows the time-integrated, temperature distribution observed from the front (a) and the side (b) of the Pb membrane. In the front view we can say the temperature distribution is quite uniform and there is no narrow current path. In the side view, we found quite high temperature zone existed 2 mm apart from the initial Pb membrane. We think that the second current path moved

to the low density region where the mobility of electrons was high. Because of damping oscillation of discharge current, the electric power consumed at the Pb membrane had two peaks at 20 μ s and 80 μ s. We think influence of the change of the discharge path on the formation of aerosols was small because the growth rate of aerosols in hot, low density plasma is slow.

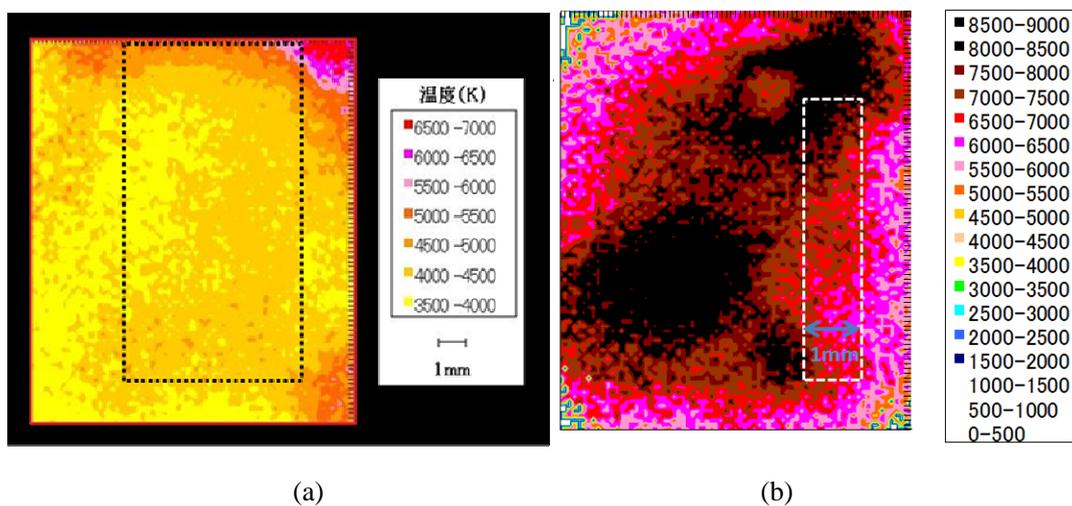


Fig. 1 Temperature distribution of discharge plasma. Front view (a), and side view (b)

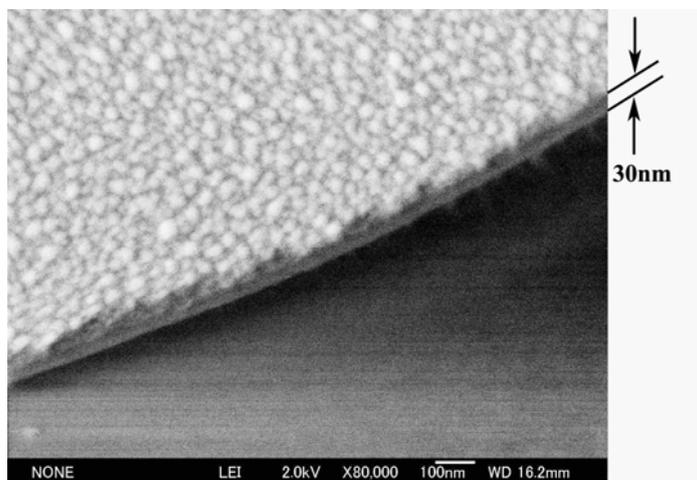


Fig. 2 Surface and cross section of deposited materials on a glass plate. There is continuous membrane under micro particles.

Lot of 30-nm-diameter particles were observed on a witness plate as shown in Fig. 2. Small particles whose diameter ranged 30 to 40 nm were found on a 30 nm thick, continuous membrane. This experimental result was compared with the simulation code DECORE (DEsign COde for REactor) [7].

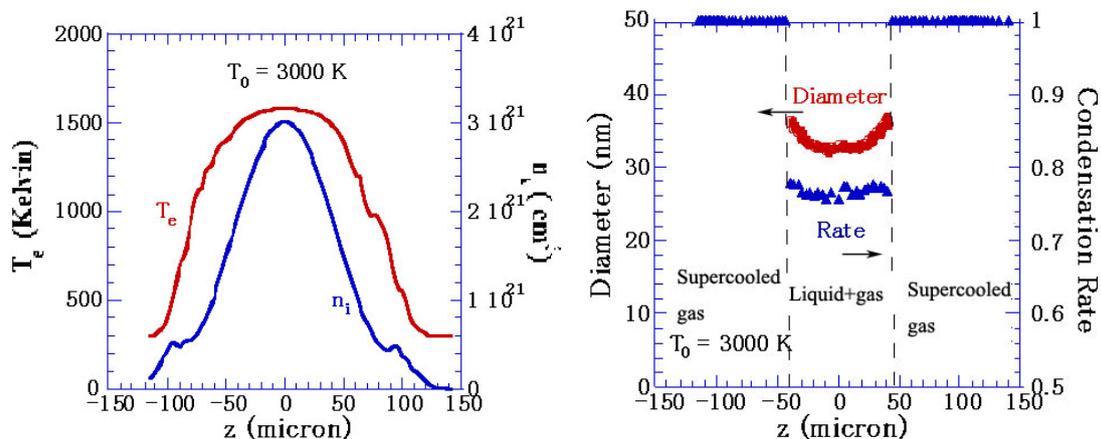


Fig. 3 Simulation on expansion of plasma from a 10 μm thick, 3000K, free standing Pb membrane. The temperature and the density profile (a) and the diameter of aerosols (b) at 40 ns after the start of expansion..

Figure 3 shows spatial profiles of the temperature, the density, the condensation rate and the diameter of aerosols at 40 ns after the discharge. Initially 10 μm thick, 3000K Pb begins to expand to both directions. Lot of 30 nm diameter aerosols are formed in the middle of expanding gas. The vapor pressure of gases of leading portion ($|z| > 50 \mu\text{m}$) is much less than its vapor pressure at the temperature. The gas is in super-cooled condition. In DECORE, estimation of formation of aerosol at the region of super-cooled gas is omitted. The diameter of aerosols are calculated only $-50 < z < 50 \mu\text{m}$. Outside of this region, the diameter will rapidly decrease because of decreases in the density and the temperature. When this leading portion collides with the witness plate, vapor condenses on the witness plate as a continuous layer as shown in Fig. 2. Then, the trailing portion that contains lot of aerosols deposits on the continuous layer. As we mentioned in a previous section, this leading portion would be heated with the second pulse, which helped to form a continuous membrane on the witness plate.

Average diameter of particles on the witness plate was very close to that numerically calculated with DECORE. Two layer structure of the deposited Pb could be explained with above mentioned model but we need additional experiment to say we successfully captured aerosols. .

2.1 Laser back lighting

Another interest is hydrodynamic instabilities due to the spatial distribution of deposited energy by alpha particles. Alpha particles release their energy at the Bragg's peak. Figure 4 shows thermal load by particles on the first wall (a) and time integrated energy deposition in liquid Pb (b). Since

energy of alpha particles decreases with time due to collisions with compressed core plasma, the position of Bragg peak approaches to the surface.. As the result, the liquid metal surface is ablated as if an 3 – 10 μm thick membrane is lift off.

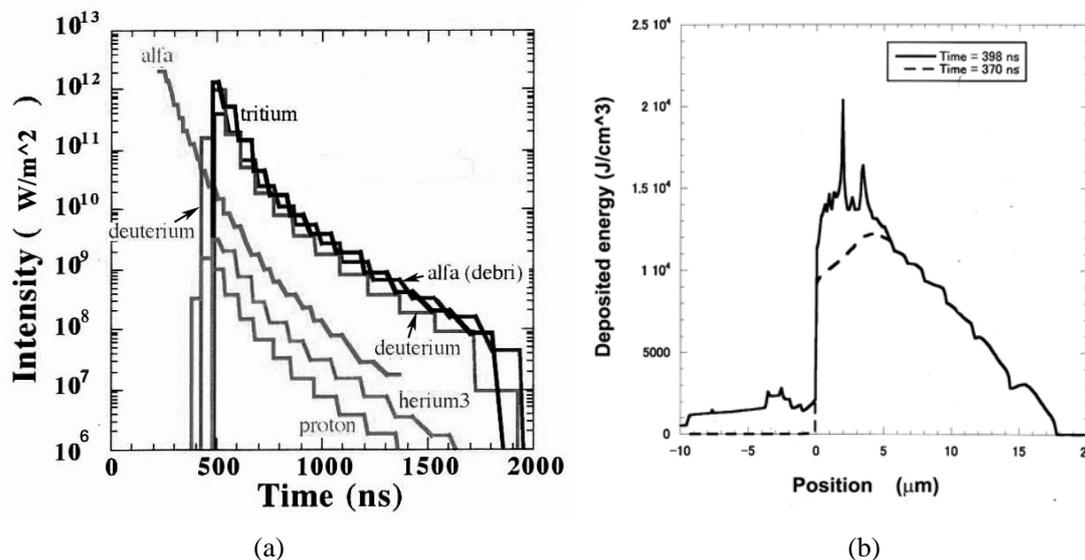


Fig. 4 Thermal loads by particles on the first wall of KOYO-F(a) and the energy deposition in Pb (b)

To experimentally simulate this phenomenon, we fired a 10- μm-thick Sn layer on a transparent glass plate from the glass plate side with a 0.08J/pulse, 15 ns, Nd:YAG laser. The laser energy deposits between the Sn membrane and the glass plate, which accelerates the Sn membrane. The glass plate was regarded as a residual LiPb flow. The absorbed laser energy density was estimated to 0.15 MJ/m² in 15 ns while heat load of alpha particles is 0.35 MJ/m² in 100ns. A plume from the laser spot was back lighted with different timings

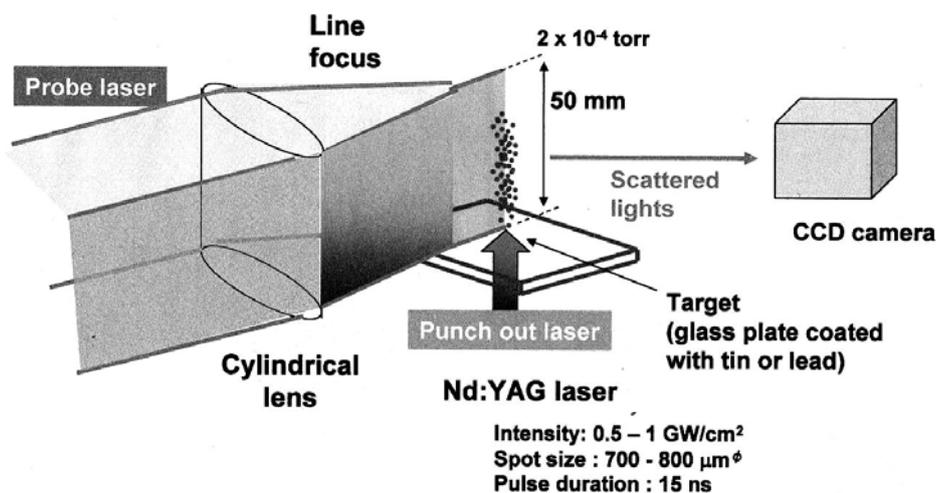


Fig. 5 Experimental setup to simulate ablation by particles that have Bragg peaks.

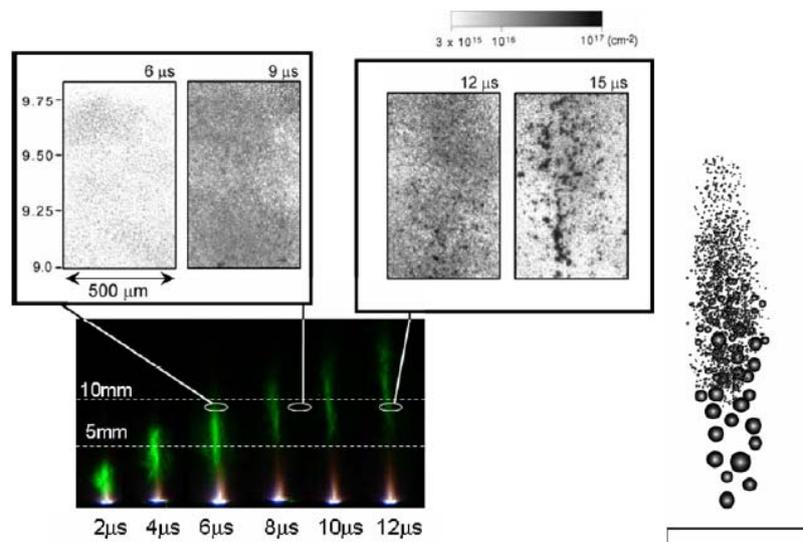


Fig. 6 Time elapsed images of plumes

Figure 6 shows back lighted images of plume at different timing. Since the spatial resolution of the image was about $10\ \mu\text{m}$, dots in images did not correspond to actual size of particles but we could see illustrated structure of the plume. Low density gas or aerosols lead heavy, large particles. We attributed formation of these large droplets to the hydrodynamic instabilities in the membrane. It is known that the growth rate of hydrodynamic instabilities in an accelerated membrane takes its maximum when the spatial wavelength of perturbation is close to the thickness of the membrane. That means largest diameter of the droplet in this experiment is about $10\ \mu\text{m}$.

When we apply this experiment result to the KOYO-F case, we had to consider followings; 1) the heating process in the KOYO-F case is volumetric heating, 2) the peak location is $2 - 3\ \mu\text{m}$ deep while laser experiment was surface heating at $10\ \mu\text{m}$ deep, and 3) the temperature of ablated vapor is still higher than its boiling point at 1932ns as shown in Fig 7. Our preliminary estimation says that the largest diameter of micro particles formed by this instability will be about $1 - 2\ \mu\text{m}$ that is 10 times larger than that of aerosols.

We also found that the plume was strongly oriented to the perpendicular to the surface. The speed of the mass center was $1 - 1.5\ \text{km/s}$. This result seems encouraging to reduce the stagnation of ablated materials by tilting the front panels. In the case of KOYO-F, temperature of ablated vapor is 2000K and the leading portion is heated to 3500K due to slow component from plasma as shown in Fig. 7. Expansion parallel to the surface with thermal velocity must be added to the perpendicular velocity to discuss the stagnation of ablated materials at the chamber center.

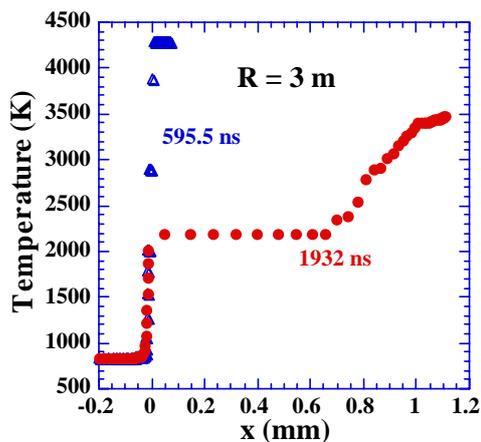


Fig. 7 temperature of ablated Pb in KOYO-F chamber

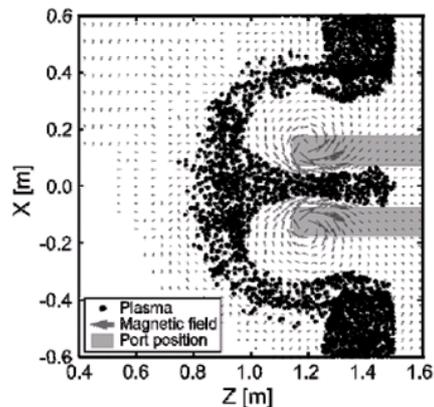


Fig. 8 Motion of alpha particles in a magnetic field for a port protection.

3. Protection of beam ports

In the KOYO-F chamber, beam ports project over the protective liquid wall and directly exposed by alpha particles from fusion burn. Some protection scheme is needed to survive the maintenance period of 2 years. We are going to use a magnetic field as the protective shield. A solenoid was housed at the tip of the beam port concentrically with the laser beam and operated synchronously with the fusion burn.

Figure 8 shows motion of alpha particles encountered with a magnetic field whose intensity was 1 T at the center. Positions of representative alpha particles are shown with x. In this calculation, electrons were treated as a fluid and alpha particles were treated as particles. Electrons were trapped with the magnetic field and alpha particles were controlled by electric field induced by charge separation. We found a 0.9 T magnetic field is sufficient to reduce the thermal load of alpha particles to less than 1/10 of the incident energy. At this energy density, no ablation takes place. This scheme requires that the tip of beam port must be fabricated with insulator such as SiC since the magnetic field will be produced by a pulse current.

On the other hand, this scheme indicates new issue. If the surface of the beam port is covered with a thin membrane of LiPb that is formed with condensation of ablated LiPb by the previous laser shot, an eddy current will be induced in the membrane due to the rapid change in the magnetic field. As the result, the membrane is blow off and the beam port becomes naked before bombing of alpha particles. Protection with rectangular coils would be the solution.[8] In this coil geometry, magnetic field is parallel to the surface and no magnetic force appears on the membrane.

4. Stability of cascade flow.

We proposed a cascade flow of liquid LiPb (Fig 9) to protect the first structural wall of the reactor from the alpha particles. To know the minimum flow rate at which a continuous layer of liquid LiPb is formed on the first wall, we made a three-step mockup using acrylic resin and water. The mockup was designed so that the Weber number of the flow was the same as the actual liquid LiPb flow from the view point of flow stability.

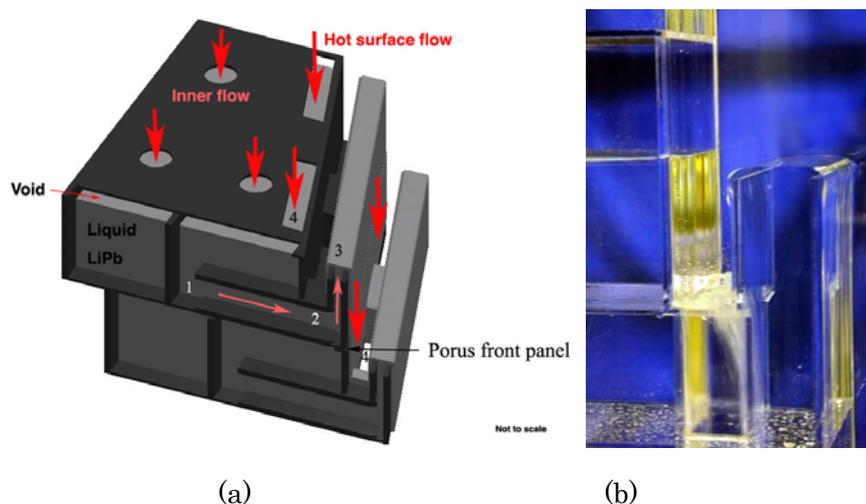


Fig. 9 Cascade scheme of KOYO-F (a) and mock-up experiment with water (b).

A 5-mm-thick stable flow was formed on a 30-cm-high, 15-cm-wide, acrylic panel. The minimum flow rate to obtain the continuous flow was confirmed experimentally and numerically [9]. Mixing of surface flow. With the inner flow was experimentally confirmed by injecting hot water into the top cascade.

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