Review of Beam Aided Diagnostics for ITER

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Abstract A reassessment of the proposed package of beam aided diagnostic systems for ITER has led to a number of new developments. As a result of a joint development effort and comprehensive optimisation studies it was decided to use two separate diagnostic observation periscope assemblies both dedicated to CXRS (Charge Exchange Recombination Spectroscopy) and BES (Beam Emission Spectroscopy), which will exploit a Diagnostic Neutral Beam injected radially into the plasma:

A 'Core CXRS' system (EU) which covers dominantly the inner half of the confined plasma, and an 'Edge CXRS' system (RF) which ensures a high radial resolution in the outer half of the plasma. The Core system utilises an upper port periscope (U-port-3), and two periscopes located in an equatorial port (E-port-3) are envisaged for the Edge CX system. The equatorial port is shared with a dedicated MSE (Motional Stark Effect) system for the measurement of magnetic field pitch angles making use of the Heating Neutral Beams. A complementary MSE approach is proposed for the exploitation of intensity line ratios as measured by the BES data from upper and equatorial ports. More recently, at the 10th ITPA meeting on ITER diagnostics at Moscow in April 2006, it was proposed to share the use of Core and Edge periscopes with the new ITER partner India, and introduce a package of Beam related diagnostics in order to optimise instrumentation for CXRS and BES.

The optical layouts of the two periscope systems have been recently reviewed and alignment and instrumentation schemes were developed.

A comprehensive multi-parameter spectral modelling effort based on an ITER reference scenario ($n_e(0)=10^{20}m^{-3}$, $T_e(0)=T_i(0)=20$ keV, B=5.2T, $Z_{eff}=1.6$) the actual observation geometry, and modelling of atomic processes, has enabled an update of expected performances in terms of measurement accuracies, time and spatial resolution.

Summarising the results of the performance study we can conclude that the measurement of radially resolved profiles of ion temperature, plasma rotation and ion densities, including that of the helium ash, are a realistic feasibility and expected parameter errors are compatible with the specifications laid down in the ITER "Measurement requirement table". Moreover, spectral Signal-To-Noise numbers well above 10 are expected for the main part of the confined plasma, that is for 0.2 < r/a < 1 for the Upper port and 0.4 < r/a < 1 for the E-port.

1. Introduction

The main progress and development steps compared to earlier feasibility studies [1-6] can be summarised by the following features:

- 1) Relaxed operational constraints in terms of beam attenuation due to a reduced size of the ITER minor radius.
- 2) Significant signal boost thanks to the development of high-resolution and high optical throughput spectral instruments [6] and back illuminated high QE cameras linked to the decision to dedicate one spectral instrument for each radial channel.
- 3) Development of in-situ calibration procedures making use of beam-emission spectroscopy (BES), charge exchange spectroscopy (CXRS) and the simultaneous measurement of continuum radiation.
- 4) Development of suitable first-mirror schemes based on substantial progress in the understanding of erosion and depositions physics [7]. A re-allocation of the first mirror further inside the blanket structure (c.f. Figs.1 and 2) and a support structure

linked to a heat exchange system kept at 400C is believed to minimise erosion and deposition.

The need for a dual observation of the DNB path from upper and equatorial ports implying an overlap of observed DNB regions has been accepted as a key ingredient in the overall diagnostic performance analysis.

The main reasons for this proposed spatial extension of the viewing region of Core and Edge periscopes are an enhanced measurement capability for plasma rotation and the investigation of anisotropic features, e.g. alpha particle slowing-down features, or anisotropic ion temperatures in transient heating phases.

The issue of plasma rotation measurements which applies for both, "Core CXRS" and "Edge CXRS" periscopes is a challenging task. In the case of the Core CXRS periscope the measured Doppler shift represents both the velocity components of the dominant toroidal plasma rotation and that of the considerably smaller poloidal rotation. Although the main region for a significant poloidal rotation is expected close to the plasma boundary, or more generally, in the region of strong pressure gradients, independent poloidal rotation profiles as measured by the two equatorial edge CXRS periscopes (c.f. ref.1) are needed for a correction of the core profile. On the other hand, any poloidal rotation measurement will be flawed by gyro-orbit effects (ref.[8]), which potentially lead to systematic errors.



The gyro-orbit effect depends strongly on the observation geometry, and the combined evaluation of both upper and equatorial observation at the same radial points will improve the

reliability of deduced velocity data. For this reason, the goal of aiming for a maximal overlap of the two observation periscope systems appeared to be highly desirable.

2.1 Radial Resolution issues

The effective radial resolution resulting from an oblique intersection of line of sight with a finite beam width can be expressed analytically in the case of a Gaussian-like beam shape with width w. Results for U- and E-ports are shown in Fig.3. A further reduction of the spatial spread imposed by blanket aperture which limits the effective DNB width inside the plasma region has not been taken into account.

$$\sigma_{R}^{2} = \int_{-\infty}^{+\infty} ds (R - R_{0})^{2} \frac{1}{\sqrt{\pi w}} \exp\left[-\left(\frac{x(s)}{w}\right)^{2}\right]$$
$$\sigma_{R}^{'} = w \cdot abs\left(\frac{\cot \alpha}{\sqrt{2 \cdot \sin \alpha}}\right) + d_{fib} \cdot m \cdot abs\left(\frac{1}{2\sin \alpha}\right)$$

Here the radius w denotes the 1/e radius of the DNB, d_{fib} , the fibre diameter, α the angle between line of sight and DNB and m the magnification factor of the optical system.



2.2 Modelling of Spectra and Performance analysis

The parametric simulation model allows the investigation of critical parameter dependencies encompassing beam parameters (beam energy, neutral current, species mix, beam divergence, viewing geometry (solid angles, line of sight directions, path length through plasma), spectral instrumentation (optical throughput, spectral resolution, quantum efficiency, integration time), plasma data (n_e , n_i , n_z , T_e , T_i , v_{rot} , B_t) and modelled edge features (edge temperatures).

A similar exercise as for the thermal CX feature representing the dominant low-Z impurity ions has been performed for beam emission spectroscopy, with regard to local beam densities, pitch angles and Lorentz splitting as a measure of the total local field. The potential measurement of local fuel mixtures is investigated by a simulation of thermal CX spectra for deuterons and tritons.

Details of the Spectral modelling concept are described in ref. [9]. The main issue is that both **active** (beam induced) and **passive** features (continuum radiation, plasma edge line emission as well as passive charge exchange line emission) have to be quantitatively assessed. In theory, any passive background feature can be suppressed by beam-modulation. This recipe fails, however, in the case, when during the beam-on phase the neutral density background has changed compared to the beam-off phase. An alternative, or complementary, scheme is to implement an additional set of "passive" lines-of-sight which are directed to the immediate background close to the beam area (c.f. Fig.4) thus monitoring wall areas close to the active line of sight set, but avoiding direct light collection from the beam itself.

The figure of merit which represents the measurability of a CX spectrum in the presence of a dominant background of continuum radiation is given by the following expression for the SNR (c.f. ref [1]) ratio which takes into account a Gaussian-like intensity profile of the DNB, part of which is imaged onto the entrance slit of a spectrometer (Fig.5). The measured signal is the result of a 3-dim integration (see also Fig.4) along the line of sight and also across within the boundaries of the viewing cone. In the case of a limiting blanket aperture both integrations will be truncated within the blanket aperture boundaries.

$$I(\lambda = \lambda_{1/2}) = \frac{1}{2} \cdot \frac{1}{\sqrt{\pi} \cdot \lambda_d} \cdot \frac{1}{4\pi} \cdot n_z \cdot Q_z \cdot \int_{-r}^{r} dx \cdot \int_{\Delta z} dz \int_{l.o.s} ds \cdot n_b(x, y, z) \cdot \Delta \lambda$$

The Spectral-Signal to Noise (cf. ref.1) revised by the truncation of finite slit image and blanket aperture is defined by the ratio of spectral amplitude at half intensity divided by the underlying continuum noise level:

$$\frac{S}{N}(\lambda_{1/2}) = \frac{I_n c_\alpha \sigma_{CX} \exp\{-\int dr n_e \sum_z c_z \sigma_{z,stop}\}}{8\pi^2 \cdot \sin \alpha \cdot e \sqrt{Z_{eff}} g_{ff} L_p B}} \cdot erf(\Delta r / w_{perp}) \cdot erf(\Delta Bl / wperp) \cdot \sqrt{\Delta \tau \frac{\Delta \lambda \cdot \lambda_{de}}{\lambda_\alpha^2} \Delta \Omega_{obs} \cdot \Delta z \cdot \eta \cdot T / 2\Delta r}}$$

$$\begin{split} I_n &= e \cdot n_{beam} \cdot v_{beam} \cdot A_{beam} = e \cdot n_{beam} \cdot v_{beam} \cdot \pi \cdot w_{\perp}^2 \text{ neutral beam current (30A),} \\ c_{\alpha} &= n_{\alpha}/n_e\text{: alpha particle concentration (0.04),} \\ \Delta \tau \text{ (sec): integration time (0.1s),} \\ \Delta \lambda(\text{Å})\text{: instrument interval (2.5Å),} \end{split}$$

 Δz : size of imaged slit along NB direction (20 mm) Δr : half size of imaged slit across NB direction (120 mm) ΔBl : half size of blanket aperture width (150 mm)

$$\lambda_{\alpha}(\text{\AA}) = \lambda_{0} \sqrt{\frac{2T_{i}}{m_{\alpha}c^{2}}} = 3.42 \cdot T_{i}^{1/2} (\text{keV}) : \text{Doppler width of the alpha particle spectrum,}$$

$$\lambda_{de}(\text{\AA}) = \lambda_{0} \sqrt{\frac{2T_{e}}{m_{e}c^{2}}} = 293 \cdot T_{e}^{1/2} (\text{keV}) : \text{Doppler width corresponding to electron temperature,}$$

L_p : path length of line of sight through plasma

- n: quantum efficiency, n=0.8,
- t: optical transmission, t=0.05,



ε: spectrometer étendue $\varepsilon = \Delta \Omega_{sp} \cdot A_{sp} = 1.05 \cdot 10^{-6} \text{ m}^2 \text{ sr.}$

Two separate criteria must be satisfied, in order to demonstrate the projected measuring capabilities. The first is **spectral measuring capability** that is the unambiguous extraction of a CX spectrum, e.g. a HeII spectrum, in the presence of a huge background of continuum radiation and a multiplicity of plasma edge emission lines. The second criterion, which is listed in the ITER measurement requirement table is the expected **data accuracy** (c.f. Figs.5 and 7), i.e. experimental errors for ion temperature, plasma rotation and ion density. The first criterion is determined solely by the ratio of expected spectral CX signal, i.e. the amplitude at half maximum, and the fluctuation of underlying continuum radiation. The second criterion reflects the errors in the least-square fit of modelled spectral shapes to noisy experimental spectra. Ultimately, the quoted errors for the extracted physics parameter depend on the complexity of the spectral model, i.e. its degrees of freedom as well as the signal noise of the measured spectrum

The scenario for the performance study is summarised in the following:

Plasma data: $n_e(0) = 10^{20} \text{m}^{-3}$, $T_e(0)=T_i(0)=15$ keV, $v_{rot}=200$ km/s, $B_{tor}=5.2$ T

 $R_0=6.2m$, a=2m, elongation=1.6 c(He⁺²)=4%, c(C⁺⁶)= 1%, c(Be⁺⁴)=2% (with respect to electrons) **DNB¹ data**: $P_{\text{NBI}}=6MW$, E= 100 keV/amu, $I_{\text{neutral}}=30A$, used current for given optical configuration (and limitation by blanket cut) 62%

Optical link: 1200 PCS fibres of 1mm diameter, length 120m, overall transmission including spectrometer grating : $T_{total}=0.05$.

The transmission estimate T is based on the periscope losses (first mirror: 0.5, followed by 4 dielectric mirrors: 0.95^4 , double window: 0.92^2 , 120m fibre link: 0.02db/m @ 500nm: 0.7, fibre F-number change:0.5, input optics : 0.92, grating efficiency: 0.6)

Instrumentation:

High-through-put, high-resolution spectrometers: Echelle Littrow configuration, F/3, f=600mm, slit-width = 1mm, slit-height = 12mm, dispersion = 2.6 A/mm. The enhanced slit height of 12mm is adapted to the 10mrad DNB diameter of 240mm.



¹ The update of DNB specification represents the status following discussion with members of the Indian Institute for Plasma Research, Bhat, Gandhinagar, who as new ITER partners have taken on the task for DNB development in 2006. The main changes compared to earlier specifications are a higher total neutral current (30A compared to 22A), and at the same time a lower current density (higher beam divergence (10mrad compared to 5mrad). The size of blanket-cut aperture for the DNB inlet is presently under discussion, also a possible toroidal tilt of the DNB by a few degrees to avoid stagnating fast ions as expected in the case of a purely radial injection.



3. Future CXRS and BES work

Supporting pilot experiments and activities are currently discussed or are already implemented. Specific goals are: optimisation of spectral instrumentation, feasibility of a Motional Stark Effect evaluation based on line ratios, 'first-mirror' test-bed experiments at the tokamak TEXTOR. The detection boost factor moving, for example, from the present JET CXRS system (several radial channels measured by one common spectrometer and CCD camera) to the envisaged ITER system (one spectrometer per radial channel) is about two orders of magnitude. For this reason it appeared sensible to explore in a pilot experiment in a look-alike viewing configuration and instrumentation the noise and detection performance. The following table shows the expected detection sensitivity (CCD photo-electrons per emitted photon flux) for the JET, ITER and the presently implemented pilot experiment on TEXTOR.

	JET	ITER(predicted)	TEXTOR-
			Pilot
Quantum	50	80	80
efficiency (%)			
Slit width (mm)	0.8	1.0	0.6
Slit height(mm)	1.0	12.0	6.3
F-number	10	3	3
Etendue (sr \cdot m ²)	5.2·10 ⁻⁹	$1.05 \cdot 10^{-6}$	$3.3 \cdot 10^{-7}$
transmission	0.05	0.05	0.07
Responsivity R	$1.3 \cdot 10^{-10}$	$4.2 \cdot 10^{-8}$	1.8· 10 ⁻⁸
$(pe/(ph \cdot m^{-2} \cdot sr^{-1}))$			

Conclusions

Significant progress has been made in terms of conceptual layout of the observation periscopes optical design and instrumentation for CXRS and BES. Advanced modelling in

context with existing CXRS diagnostic systems at JET, TEXTOR, ASDEX-UG and Tore Supra has enabled more precise predictions for active and passive spectral features. A performance analysis based on synthetic spectra has demonstrated the feasibility of the ITER CXRS and BES diagnostic with accuracies, radial and temporal resolution in line of the specification of the ITER measurement requirement table.

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