

## Peaked Density Profiles in Low Collisionality H-modes in JET, ASDEX Upgrade and TCV

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**Abstract.** Results from an extensive database analysis of JET and AUG density profiles in H-mode, show that the density peaking factor  $n_{e0}/\langle n_e \rangle$  increases to above 1.5 as the effective collisionality drops to values close to those expected for ITER. On any single device density peaking is also strongly correlated with the Greenwald number  $N_G$  and the particle outward flux  $\Gamma$  from the neutral beam source, when applicable. Fully RF-heated H-modes in JET and TCV show that neutral beam fuelling is not the dominant contributor to density peaking. Multiple regression analyses are performed which show that in the combined database, collisionality is the most relevant parameter. Scalings for density peaking are proposed and implications for ITER performance are discussed.

### 1. Introduction

Peaked electron and fuel density profiles in reactor plasmas provide the advantage of higher reactivity, higher bootstrap fraction and stronger electron-ion coupling in the core, than obtained with flat density profiles at the same average density and stored energy. Several recent papers have established that the existence of peaked density profiles in tokamak discharges is not in general due to the Ware pinch, nor to the particle source (be it by edge or neutral beam fuelling), although both of these processes may contribute, depending on circumstances [1-8]. The main cause for density peaking hence appears to be an anomalous pinch. While some of the observations are in qualitative agreement with some of the theoretical predictions [2,9-11], it is fair to say that agreement of state-of-the-art gyrokinetic theory with observation has not yet been demonstrated [12,13]. In these conditions, as for many other aspects in fusion research, the authors have resorted to an empirical approach, by combining evidence from different devices in order to obtain a scaling of the peaking factor and normalised density gradients that is suitable for extrapolation towards reactor conditions. Following separate investigations on AUG [11] and JET [5-7] the data were combined into a single database, with the advantage of reduced colinearities in the regression variables

### 2. Combined JET-AUG Database

The dimensionless physics parameters  $v_{\text{eff}}$ ,  $\beta$  and  $\rho^*$ , are used here with the following definitions:

$$\rho^* = 0.3225(m_{\text{eff}} \langle T_e \rangle)^{1/2} / (aB_T) ; v_{\text{eff}} = 2 \times 10^{-14} \langle n_e \rangle R_0 / \langle T_e \rangle^2 ; \beta = 4.02 \times 10^{-3} \langle p \rangle / B_T^2 .$$

The above definition of  $v_{\text{eff}}$  omits the factor  $Z_{\text{eff}}$ , in effect assumed to be equal to 2. Geometrical plasma parameters like  $q_{95}$  and the edge triangularity  $\delta$  are also considered. The geometrical

major radius  $R_0$ , despite being dimensional, is also included in part of the analysis as a device label, in order to check its significance in the regressions.

Detailed edge source calculations [4] have shown that the edge source cannot account for the observed level of peaking. These findings were confirmed in experiments in He plasmas, which have the same peaking as deuterium with otherwise similar operational parameters, despite quenching of charge exchange chains due to the low cross sections for double charge exchange [4]. Consequently, only fuelling by beams is considered here. The beam heating and particle source profiles have been computed for all the observations by the PENCIL code for JET and the FAFNER code for AUG data. By casting the general diffusive law for the net particle flux  $\Gamma$  in steady state determined by the source in the form  $\frac{R\nabla n}{n} = -\frac{R}{D}\left(\frac{\Gamma}{n} + V\right)$ , the NBI source contribution

to the density peaking can be quantified by a dimensionless source term  $\Gamma^* = \frac{R\Gamma}{nD} \cong 2T \frac{\chi}{D} \frac{\Gamma}{Q_{NBI}} \frac{Q_{NBI}}{Q_{TOT}} \left| \frac{R}{T} \frac{dT}{dr} \right|$ , where  $\chi$  is the effective heat diffusivity and the

approximation corresponds to assuming  $T_i = T_e$ .  $Q_{NBI}$  is the heat flux from neutral beams and  $Q_{TOT}$  is the total heat flux.  $\Gamma/Q_{NBI}$  is determined by the beam energy spectrum.  $\chi/D$  can be treated as a free parameter, whilst all the other terms in  $\Gamma^*$  can be evaluated from parameters in the database.

## 2.2 Definition of the Regression Variables

A meaningful combination of data from different devices requires consistent definitions and measurements of the variables, especially of the regressed variable. Data with systematic errors in opposite direction from different devices are a major concern, because regressions tend to associate these with differences in the dimensionless operating domains of the devices, essentially  $v_{eff}$ ,  $\rho^*$  and  $\Gamma^*$ , thereby leading to erroneous extrapolations.

To overcome this problem, we have devised a method to obtain values of density peaking for JET AUG and JET derived with exactly the same procedure [14]. We have observed that density profile measurements from Thomson scattering and interferometry agree better in JET than in AUG. We therefore computed the line integrals along the chords of the AUG interferometer of all the JET profiles of the database, remapped onto a chosen AUG equilibrium. Using the same equilibrium, we inverted the line integrals of the JET profiles by expressing the profiles as linear combinations of base functions for the profile shape. Finally, by the same method we also inverted all the AUG density profiles. In this way a set of density profiles, for both AUG and JET, reconstructed from the AUG interferometer line integrals by the same inversion method is obtained. Among the various possible definitions of density peaking, the definition of density peaking  $n_e(\rho_{pol} = 0.2)/\langle n_e \rangle_{vol}$  is rather independent of the choice of the basis functions for the inversion, and strongly constrained, once all the line integrals are matched. The RMSE between the original JET density peaking [6], calculated using the SVDI method [15] with basis functions adjusted from shot to shot and the recalculated peaking with fixed basis functions is only 0.018.

## 2.3 Bivariate Correlations

Fig. 1 shows a selection of correlation plots. The related correlation coefficients are quoted in the figure, in black for the combined database, in red for AUG data only and in blue for JET data only. Those in smaller fonts indicate the correlation coefficients for the subset of plasmas heated by NBI only. The combined database is composed of 277 JET observations and 343 AUG observations. Correlations with  $\rho^*$  are strongly reduced by combining the two devices, but the correlation with the Greenwald fraction  $N_{GR}$  remains rather large. Collisionality is the parameter

which has the largest correlation with density peaking in the combined dataset. However both the Greenwald fraction and the beam particle source parameter  $\Gamma^*$  are also highly correlated with density peaking. Finally, a very strong correlation between  $v_{\text{eff}}$  and  $\Gamma^*$  in AUG plasmas heated with NBI only is found. This correlation is reduced by considering data from the two devices and by including data from ICRH-only discharges.

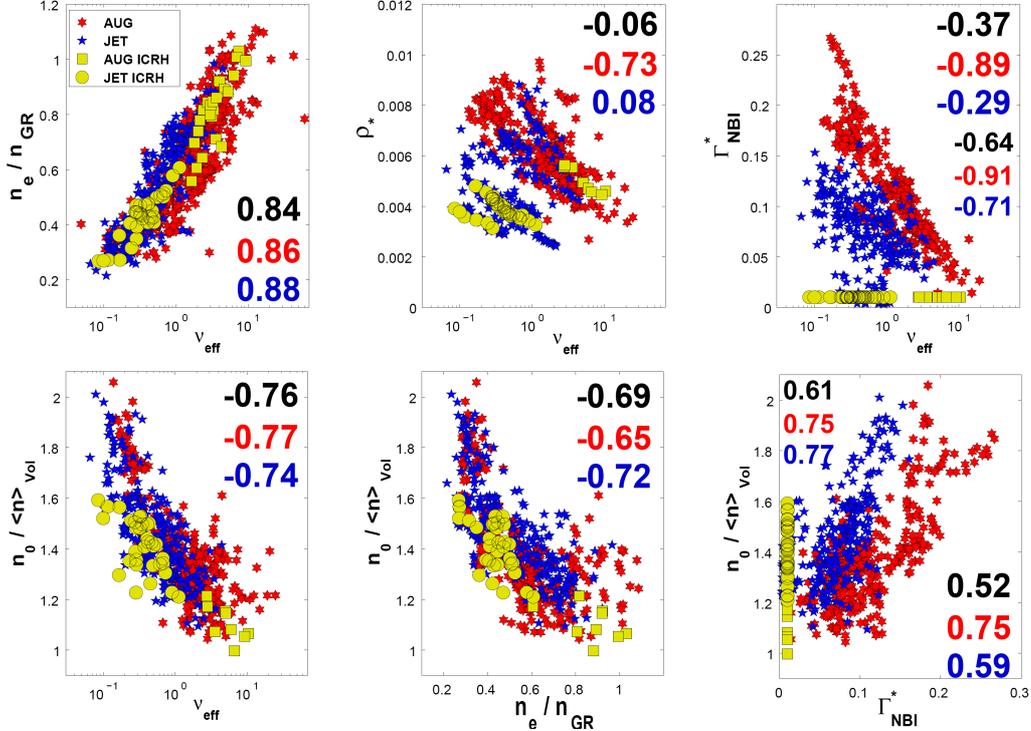


Fig.1 Selection of scatterplots with correlation coefficients (in small for NBI only).

## 2.4 Multivariate Statistical Analysis

Linear and logarithmic multivariable regressions express the regressed variable  $Y$  in the forms  $Y = a_0 + \sum_j a_j X_j$  and  $Y = a_0 \prod_j X_j^{a_j}$ , where  $X_j$  are the regression variables and  $a_j$  the regression coefficients. Linear and logarithmic regressions having provided equivalent results in this study, due to the modest variation of the regressed variable  $n_e(0.2)/\langle n_e \rangle_{\text{vol}}$ , we'll only consider the former here. Following [16], we define the normalised statistical relevance  $\text{StR}_j$  and significance  $\text{StS}_j$  of the regression variable  $X_j$  as:  $\text{StR}_j = a_j \times \text{STD}(X_j) / \text{STD}(Y)$  and  $\text{StS}_j = a_j / \text{STD}(a_j)$ , where  $\text{STD}$  designates the usual standard deviation.

Table 1 shows the normalised statistical relevance obtained for regressions involving different variables. The statistical significance is seen in table 2 for the same set of regressions. For a parameter  $X_j$  to be significant,  $|\text{StS}_j| > 2$  is required. Regressions which include  $v_{\text{eff}}$  and exclude  $N_{GR}$ , which include  $N_{GR}$  and exclude  $v_{\text{eff}}$ , as well as regressions which include both these plasma parameters, are considered. Moreover, for comparison, models which, besides the dimensionless variables, also include a device label (namely  $R_0$ ) are analysed. In all the regression models which include it,  $v_{\text{eff}}$  is found to be the parameter with the largest statistical relevance and has a large statistical significance.

Comparable RMSE is found when the device label is included or excluded. In regression models which include  $v_{\text{eff}}$  and exclude  $R_0$ ,  $\rho^*$  is found to have a negligible statistical significance and relevance. In regression models which include  $N_{GR}$  and exclude  $v_{\text{eff}}$ ,  $R_0$  plays a more important

role, through a larger statistical relevance of  $\rho^*$  and/or  $R_0$ . At the same  $N_{GR}$ , the density peaking is larger in JET than in AUG. In regression models which exclude  $v_{eff}$  and include  $N_{GR}$ ,  $\Gamma^*$  is found to have a larger statistical relevance. Finally, in regression models which include both  $v_{eff}$  and  $N_{GR}$ , density peaking increases with increasing  $N_{GR}$  at fixed  $v_{eff}$ . The significance of  $v_{eff}$  is not only larger than that of all other variables considered separately, but also larger than that of the pair  $(N_{GR}, R_0)$  and comparable to the pair  $(\Gamma^*, N_{GR})$  [14]. The pair  $(v_{eff}, \Gamma^*)$  has the highest significance of all pairs.

TABLE 1: NORMALISED STATISTICAL RELEVANCE OF MAIN VARIABLES AND RMSE FOR DIFFERENT REGRESSION MODELS

Variables excluded	$\Gamma^*$	$\ln v_{eff}$	$N_{GR}$	$\rho^*$	$\beta$	$q_{95}$	$\delta$	$T_{e2}/\langle T_e \rangle$	$R_0$	rmse
$N_{GR}$	0.39	-0.49		0.13	-0.24	-0.07	-0.08	0.03	0.25	0.113
$N_{GR} \& R_0$	0.34	-0.64		-0.02	-0.16	-0.1	-0.014	-0.007		0.114
$\ln v_{eff}$	0.49		-0.30	0.14	-0.17	0.01	-0.08	-0.028	0.47	0.121
$\ln v_{eff} \& R_0$	0.42		-0.61	-0.27	0.09	-0.001	0.114	-0.12		0.126
None	0.39	-0.57	0.13	0.20	-0.31	-0.08	-0.12	0.036	0.29	0.112
$R_0$	0.34	-0.68	0.05	-0.005	-0.18	-0.10	-0.027	-0.008		0.114

TABLE 2: STATISTICAL SIGNIFICANCE OF MAIN VARIABLES FOR ABOVE REGRESSION MODELS

Variables excluded	$\Gamma^*$	$\ln v_{eff}$	$N_{GR}$	$\rho^*$	$\beta$	$q_{95}$	$\delta$	$T_{e2}/\langle T_e \rangle$	$R_0$	rmse
$N_{GR}$	5.2	-5.24		1.0	-2.5	-1.1	-1.2	0.5	2	0.113
$N_{GR} \& R_0$	4.8	-10.2		-0.2	-1.7	-1.5	-0.2	-0.1		0.114
$\ln v_{eff}$	7.3		-3.0	0.9	-1.5	0.2	-1.1	-0.4	4.1	0.121
$\ln v_{eff} \& R_0$	6.2		-8.5	-2.5	0.9	-0.1	1.8	-2		0.126
None	5.2	-4.3	0.9	1.4	-2.6	-1.2	-1.5	0.6	2.2	0.112
$R_0$	4.7	-5.3	0.4	-0.04	-1.7	-1.6	-0.4	-0.1		0.114

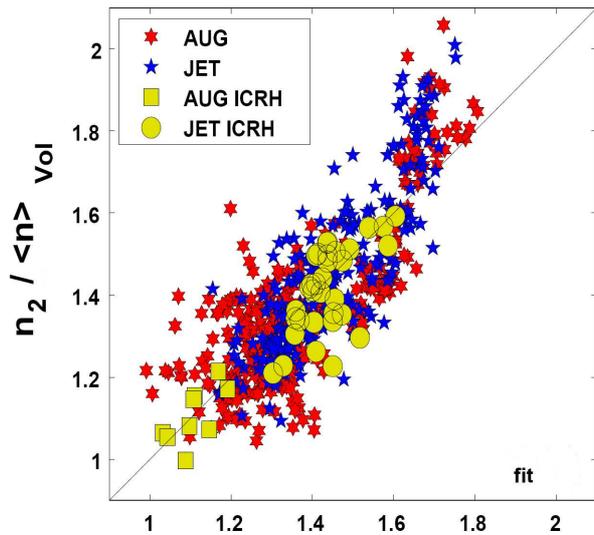


Fig.2 Experimental versus fitted density peaking

An example of a scaling relation (fig.2) without  $N_{GR}$  is given as

$$n_{e2}/\langle n_e \rangle = 1.35 \pm 0.015 - (0.12 \pm 0.01) \ln v_{eff} + (1.17 \pm 0.01) \Gamma^* - (4.3 \pm 0.8) \beta$$

Extrapolation to ITER predicts a density peaking given by  $n_e(0.2)/\langle n_e \rangle \approx 1.45$ . For ITER we assumed  $\langle T_e \rangle = 8$  keV and  $\langle n_e \rangle = 10^{20} \text{m}^{-3}$ ,  $N_{GR} = 0.85$  and  $\Gamma^* = 0$ . All regressions using  $v_{eff}$  as one of the regression variables predict  $n_e(0.2)/\langle n_e \rangle > 1.35$  for ITER, whilst nearly all those excluding  $v_{eff}$  predict  $n_e(0.2)/\langle n_e \rangle < 1.2$ .

### 3. Influence of Specific Parameters and Comparison with theory

The collisionality dependence of the anomalous pinch predicted by gyrofluid turbulence models [11, 17] is qualitatively consistent with the above observations in H-mode. However the collisionality dependence in gyrokinetic models is still an issue under investigation [12,13].

The combined AUG-JET database does not have  $T_i$  and  $q$  profiles. Regressions involving these quantities have been performed on a subset of the JET database [6]. They are consistent with the results from the combined database and confirm a lack of a dependence on local magnetic shear, global shear ( $l_i$ ) and on the normalised temperature gradients. These observations are at odds with theoretical expectations for the curvature pinch and thermodiffusion [18]. However JET data reveal a modest dependence on the theoretically important temperature ratio  $T_i/T_e$ , expressed in the scaling relation obtained from a subset of 114 JET samples:

$$n_{e2}/\langle n_e \rangle = 1.15 \pm 0.07 - 0.12 (\pm 0.02) \ln v_{\text{eff}} + 0.17 (\pm 0.13) D\Gamma^*/\chi + 0.13 (\pm 0.08) T_i/T_e$$

In the above expression  $T_i/T_e$  and  $D\Gamma^*/\chi$  are taken at mid-radius (Calculating  $D\Gamma^*/\chi$  does not require  $D$ , see definition in section 2). An extrapolation to ITER, using this fit and assuming  $T_i/T_e=0.9$ , provides  $n_{e2}/\langle n_e \rangle \approx 1.47$ , consistently with the combined database. A local fit to the normalized density gradients around mid-radius provides

$$R\nabla n_e/n_e = 0.97 \pm 0.34 - (0.65 \pm 0.1) \ln v_{\text{eff}} + (1.46 \pm 0.63) D\Gamma^*/\chi + (0.65 \pm 0.4) T_i/T_e$$

This scaling relation leads to an expectation of  $R\nabla n_e/n_e \approx 2.6$  near mid-radius in ITER. The coefficient ( $1.46 \pm 0.63$ ) of the local fit for  $D\Gamma^*/\chi$  is an estimate for  $\chi/D$  and is consistent with a theoretical expectation ( $\chi/D=1.5$ ) for anomalous transport [18] and with the range of  $\chi/D_T$  observed in trace tritium experiments [19]. The above ratio  $\chi/D$  is however higher and hence the inferred influence of the source on peaking is lower than found or assumed in other investigations of density profiles on JET [7,8]. Importantly for performance extrapolations including the effect of peaked density profiles, we find no significant correlation between  $n_{e2}/\langle n_e \rangle$  and the dimensionless confinement time  $\omega_{ce}\tau_E$ , whether from diamagnetic or kinetic data, whereas  $\omega_{ce}\tau_E$  in the database is clearly correlated with  $\rho^*$ ,  $v_{\text{eff}}$ ,  $\beta_N$  and  $q_{95}$ , as expected.

The observation that density profiles tend to be flatter at low values of  $T_i/T_e$  is in qualitative agreement with theory. A concern for a reactor is that the large core electron heating by slowing-down alpha particles may destabilise TEMs. TEMs drive a thermodiffusive outward particle flux, which may lead to partial or complete flattening of the density profile [12,18]. This cannot be tested at JET yet, because purely ICRH heated H-modes in JET only have  $\beta_N \sim 1$ , due to a lack of available power. However purely electron heated H-modes with  $\beta_N \approx 2$  and  $T_e/T_i \approx 2$ , recently obtained in TCV using ECH, show that flattening is only partial and significantly peaked density profiles ( $n_{e2}/\langle n_e \rangle \sim 1.5$  in TCV ELMy H-modes) persist in electron heated regimes at reactor relevant values of  $\beta_N$ , even when  $T_e$  is significantly above  $T_i$  (fig.3). The weakness of the  $T_e/T_i$  dependence in JET and the observations in TCV suggest that flattening of the density profile in ITER as a result of  $\alpha$ -heating is unlikely.

As for JET, peaking in these TCV plasmas cannot be explained by the Ware pinch, unless very low values of  $D/\chi$  are assumed. To maintain the observed density gradients,  $\nabla n_e/n_e \sim 5\text{m}^{-1}$ , with typical  $V_{\text{ware}} \sim 0.3\text{m/s}$ ,  $D$  would have to be about  $0.06\text{m}^2/\text{s}$  i.e. 50 times smaller than  $\chi$ . The neutral source from the edge, simulated with Kn1D and DOUBLE codes [4] is, as in JET [4], too shallow

to explain the peakedness of the density profiles in a purely diffusive model, unless the ratio  $D/\chi$  is assumed to vary by more than two orders of magnitude within the confinement zone (fig. 4).

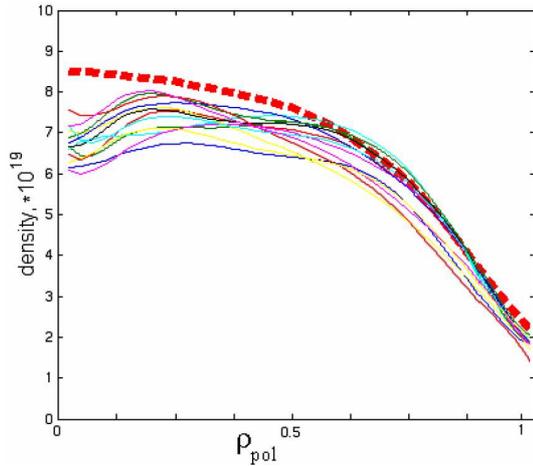


Fig.3 : Multiple TS measurements of density profiles during ECH heating in ELMy H-mode in TCV. Red dashed line – density profile in an Ohmic H-mode plasma.

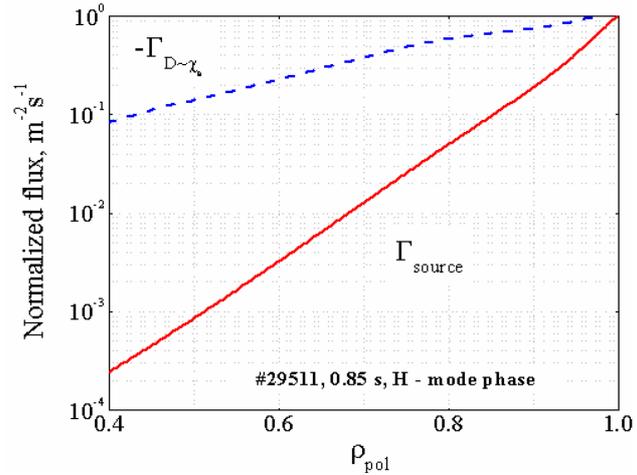


Fig.4: Kn1D simulation of edge neutrals flux and comparison with particle diffusive flux, assuming  $D \propto \chi$ , for ECH heated H-mode plasma on TCV.

#### 4. Impact on Reactor Fusion Performance

We have treated each of the  $n_e$ ,  $T_e$  profile pairs in the JET database as a potential model for ITER by renormalizing the density and the temperature to the ITER parameters for the inductive scenario, i.e.  $\langle n_e \rangle = 1.01 \times 10^{20} \text{m}^{-3}$  and  $\beta_N = 1.8$  and the plasma volume to  $831 \text{m}^3$ , while keeping the normalised profiles unchanged. We assumed  $T_i = T_e$  and the dilution was adjusted such as to obtain a thermonuclear fusion power  $P_{\text{fus}} \equiv 17.6 \times 10^6 [\langle \sigma v \rangle n_{DnT} dV = 400 \text{MW}]$  (corresponding to  $Q=10$ ) for a flat density profile and an ITER-like temperature profile as in [20], with  $T(0.95)/T(0) \approx 0.18$  and  $T(0) \approx 22 \text{keV}$ . Fig.5 shows the resulting fusion power, resolved into classes of relative pedestal temperature,  $T(0.95)/T(0)$ , as they occur in the JET database. In addition to the dependence on density peaking, there also is a strong dependence on  $T(0.95)/T(0)$ , large temperature pedestals being unfavourable for fusion performance when operation is restricted to a fixed value of stored energy, corresponding to the  $\beta$ -restriction of a particular operating scenario (This only reverses for  $T(0) > 40 \text{keV}$ ). Note that, as seen in fig.5 (diamonds, triangles and stars), most temperature profiles in JET are broader than those resulting from the simulations in [20].

For operation at fixed  $\beta$ , the extra  $\alpha$  power must substitute for some of the auxiliary heating power and will hence lead to an increase in  $Q$  from 10 to 30 or more, assuming  $n_{e2}/\langle n_e \rangle = 1.46$  and assuming that peaked density profiles per se have no effect on global confinement, as suggested by the JET results in the previous section. For peaking exceeding the above ITER predictions, the alpha power increase may in principle substitute for all of the auxiliary power (40 MW), allowing ignition. Only a small number of the  $n_e, T_e$  profile pairs in the JET database (those with  $P_{\text{fus}} > 600 \text{MW}$  in fig.5) are however peaked enough and all of those have significant beam fuelling. Beam fuelling will be insignificant in ITER.

The fusion power in these ITER models for fixed  $\beta$  and  $\langle n_e \rangle$  scales very closely to  $\langle p^2 \rangle / \langle p \rangle^2$ , as expected from the nearly quadratic dependence of  $\langle \sigma v \rangle$  on  $T_i$  in the range 7-20keV, which corresponds to most of the plasma volume in the ITER inductive and hybrid scenarios. We may therefore use  $\langle p^2 \rangle / \langle p \rangle^2$  as a figure of merit for the pressure profile. Fig. 6 shows that fusion

performance increases in a very similar fashion as density peaking when the  $v_{\text{eff}}$  decreases.

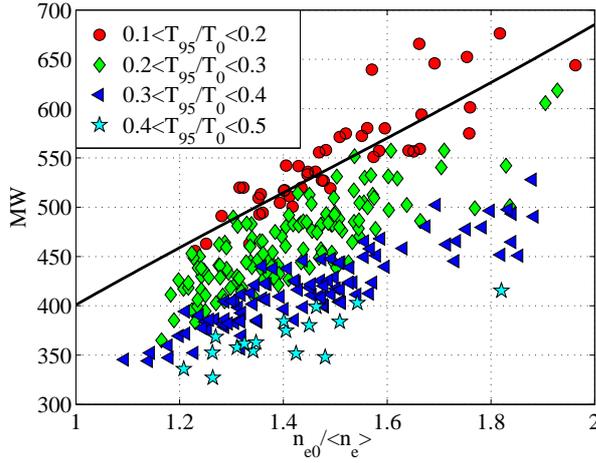


Fig 5: Fusion power versus density peaking, resolved into classes of relative edge temperature, assuming  $\langle n_e \rangle = 1.01 \times 10^{20} \text{ m}^{-3}$ ,  $\beta_N = 1.8$  and  $V = 831 \text{ m}^3$  with density and temperature profile shapes from the JET database. The line is for a temperature profile similar to ITER simulations in ref [20].

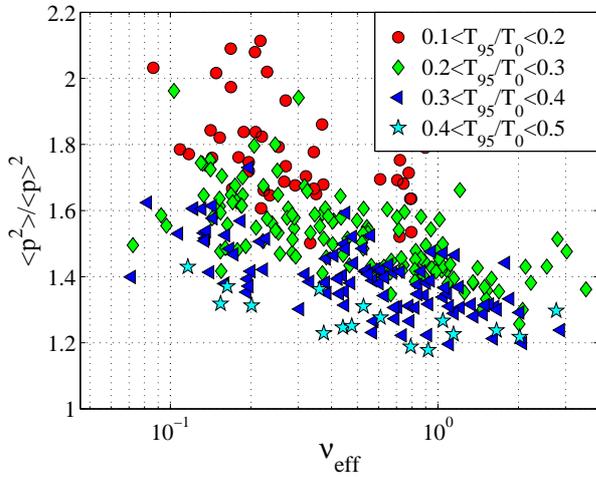


Fig 6. Pressure profile figure of merit versus collisionality in JET. Symbols: classes of relative temperature pedestals.

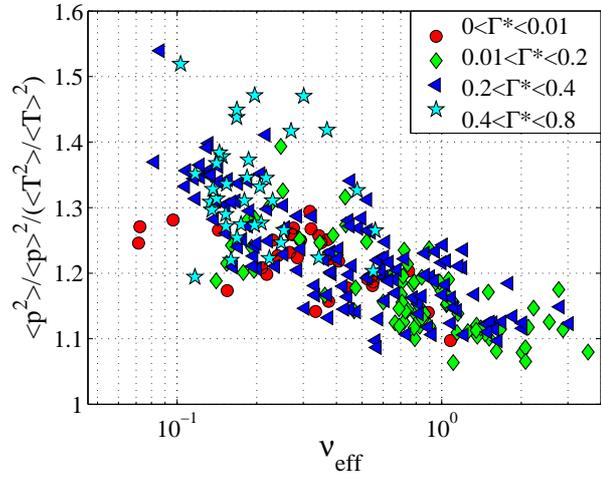


Fig 7. Density contribution to the pressure profile figure of merit. Symbols: classes of dimensionless beam source.

On the other hand  $\langle T^2 \rangle / \langle T \rangle^2$  shows no significant correlation with any of the dimensionless parameters, thereby demonstrating that the beneficial effect of density peaking is not cancelled by temperature profile broadening, as ‘pressure profile consistency’ theories might suggest. For typical JET profiles at low collisionality, the fusion performance improvement attributable to density peaking, quantitatively expressed by the ratio  $\langle p^2 \rangle \langle T \rangle^2 / (\langle p \rangle^2 \langle T^2 \rangle)$ , amounts to some 30%, as seen in fig 7. Instead of regressing the density peaking factor, we may also regress the above profile merit factors. These lead to  $\langle p^2 \rangle / \langle p \rangle^2 \approx 1.55$  and  $\langle p^2 \rangle \langle T \rangle^2 / (\langle p \rangle^2 \langle T^2 \rangle) \approx 1.25$  expected for ITER by regressions including collisionality as a regression variable.

A drawback of density peaking is an increased proneness to heavy impurity accumulation. Carbon density profiles from CXS remain close to flat irrespectively of collisionality in JET H-modes [5]. Core accumulation of laser ablated Ni has been observed in some JET discharges at  $v_{\text{eff}} \sim 0.1$  [21]. Accumulation of tungsten in AUG [22] and Nickel in JET [21] have been shown to be preventable with central electron heating. On the downside we also have to consider that for fixed  $N_G$  and  $\beta$ , density peaking unavoidably leads to a reduction of the pedestal density below the average density, by some 25% for the above ITER projections [6]. This may affect divertor performance by making detachment more difficult. If however the density limit is linked to the

pedestal density, rather than to the line average density, a simple remedy is to raise the edge density to the target value with a corresponding temperature reduction to conserve  $\beta$ . In this case the effect of peaking is still beneficial, although somewhat less than at fixed average density [6]. Density peaking may also provide a natural means to salvage core fusion performance (but not divertor performance) if the edge density limit drops to half of the expected value [23].

## Conclusions

Studies on JET, AUG and TCV have clearly established the anomalous nature of density peaking in H-mode, i.e. this phenomenon cannot be explained by the Ware pinch alone, nor the particle source, although the latter is a contributor in beam heated discharges. The most important parameters for peaking are collisionality, the beam source (where applicable) and the Greenwald fraction. Scaling expressions including collisionality predict fairly peaked density profiles for ITER, providing a fusion power increase of near 30%, while scalings excluding it predict fairly flat profiles for ITER. Although clearly anomalous, many observations of density profile behaviour are still challenges for physics based theoretical modelling. These include the apparent lack of correlation of density peaking with magnetic shear in H-mode (albeit observed in L-mode, [2,3]) and with temperature peaking and the abrupt collisionality dependence of pinches in gyrokinetic models [12,13]. The relatively broad scatter of the regression fits, which exceeds experimental errors, also suggests the existence of factors influencing density peaking, which have yet to be experimentally identified.

**Acknowledgement:** This work was partly supported by the Swiss National Science Foundation.

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