

Simulations of Turbulent Diffusion in Wire-Wrapped Sodium Fast Reactor Fuel Assemblies

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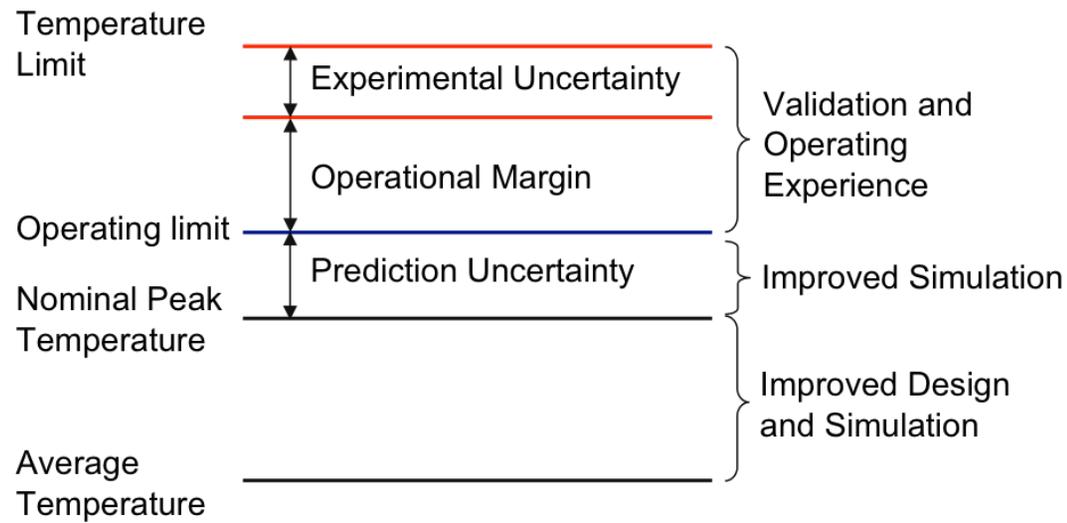
Overview

- Background and Motivation
- Multi-scale approach to design and safety analysis
- Review of initial results
- Recent Results
- Full-size assembly simulation benchmarking
- Conclusions and Future Work



Path Forward to Future Commercial ABR's

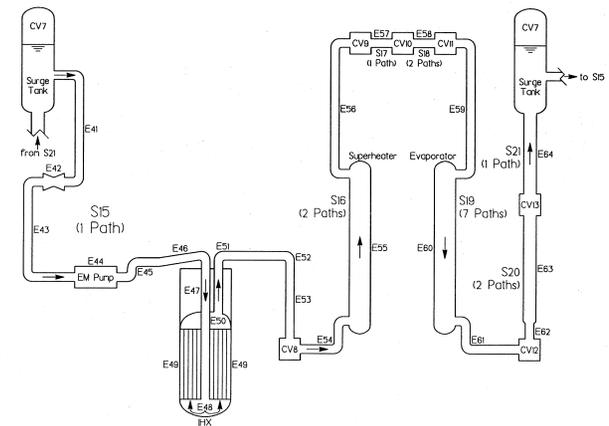
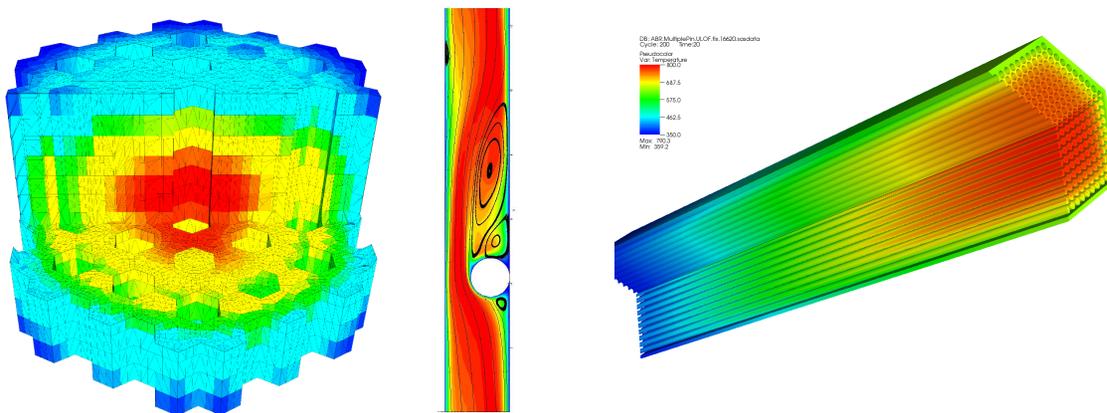
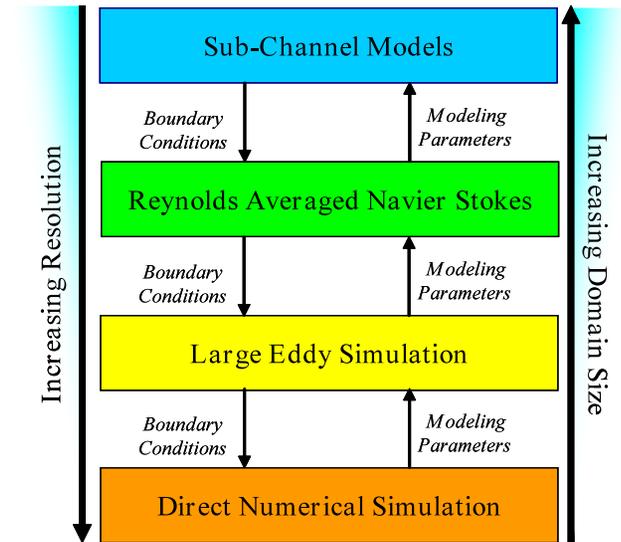
- Path Forward
 - Design simplifications (reduce mass of steel)
 - Compact reactor vessel
 - Compact intermediate components
 - Advanced compact fuel handling systems
 - New technologies that allow for reduced structural materials inventory and compact piping systems
 - Improved management of design and safety margins



Role of Advanced Simulations

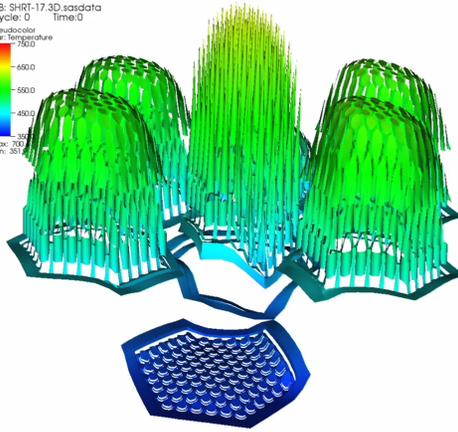
- Need to develop multi-resolution modeling approach capable of quantifying the complex interactions from fuel centerline to the ultimate heat sink.
 - This presents a challenge because of the large domains in time (10^{-7} seconds to years) and space (10^{-6} meters to 10s of meters).
 - In the absence of experiments, higher-fidelity models need to provide accurate, geometry-dependent parameters to lower-fidelity models that can capture much larger domains in both space and time.

T/H Modeling Domains

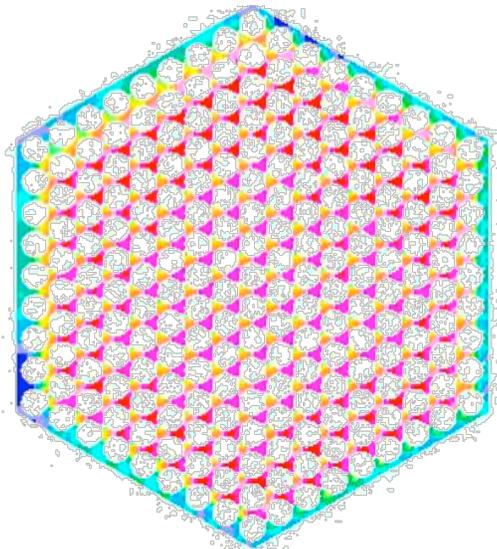


Thermofluid Code Development

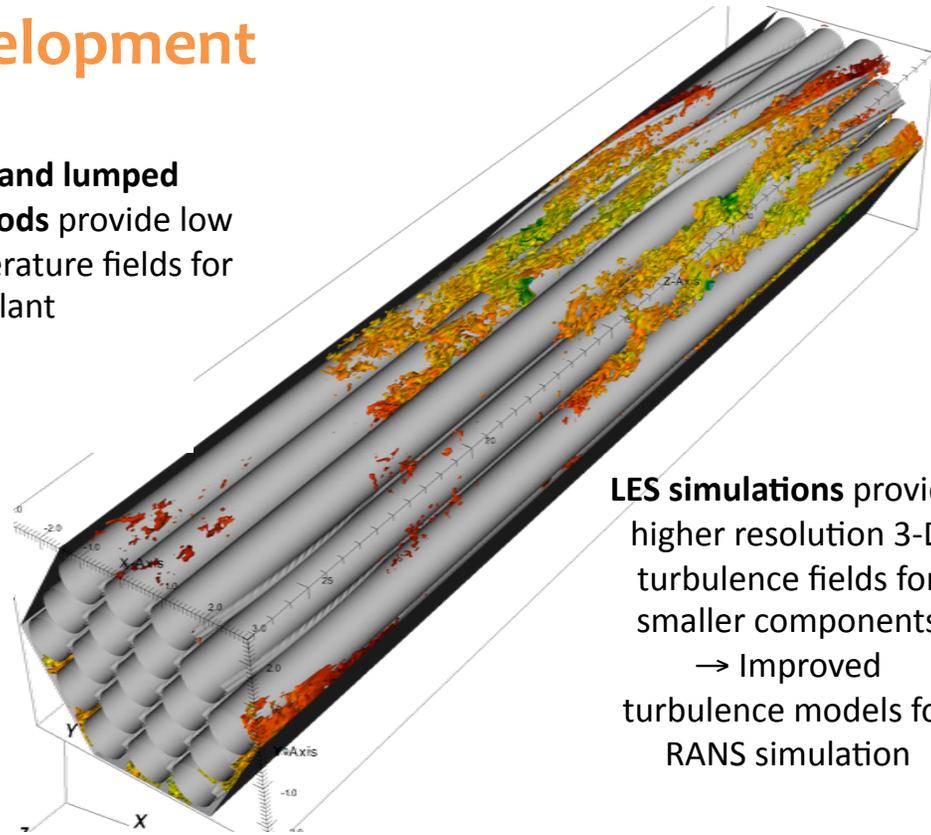
DB: SHRT-17_3D_sasdata
Cycle: 0 Time: 0
Pseudocolor
Var: Temperature
7000
6500
6000
5500
5000
4500
4000
3500
3000
Max: 7000
Min: 3000



Sub-channel and lumped parameter methods provide low resolution temperature fields for full plant

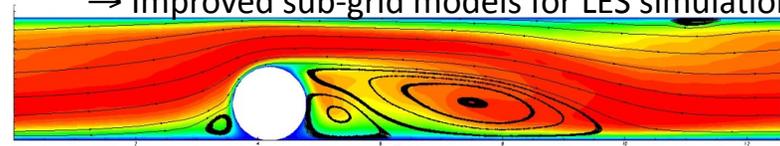


RANS simulations provide high resolution 3-D temperature fields for large components
→ Improved models for lower fidelity simulations



LES simulations provide higher resolution 3-D turbulence fields for smaller components
→ Improved turbulence models for RANS simulation

DNS simulations provide first principles turbulence fields for small characteristic geometries
→ Improved sub-grid models for LES simulations



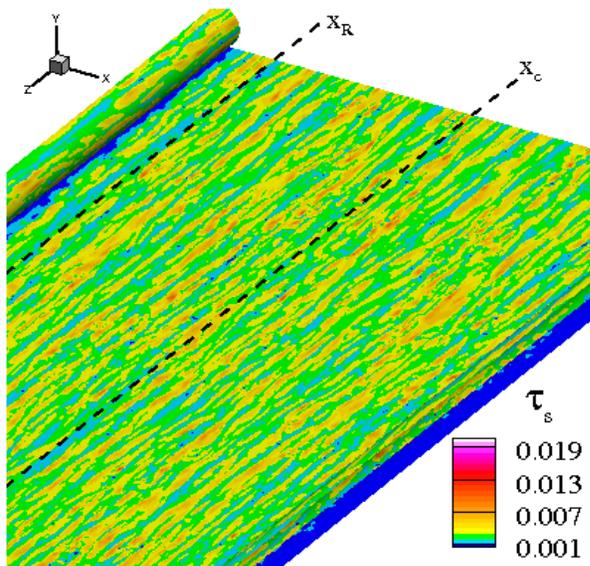
Key Findings 06-08: Direct Numerical Simulation of Turbulence

Plane Channel + Wire in Cross Flow

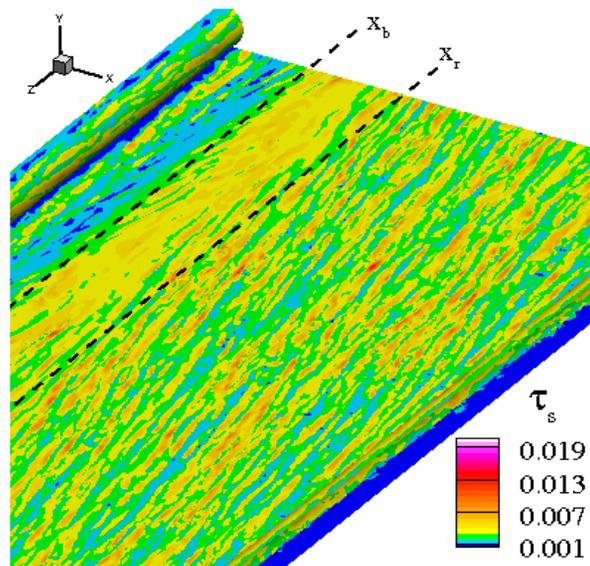
R. Ranjan & C. Pantano, UIUC

- Single wire in a channel with cross flow simulated at $Re_b = 6000$ using a spectral code: **gold standard turbulence benchmark**
- 3 million node hours through INCITE award.

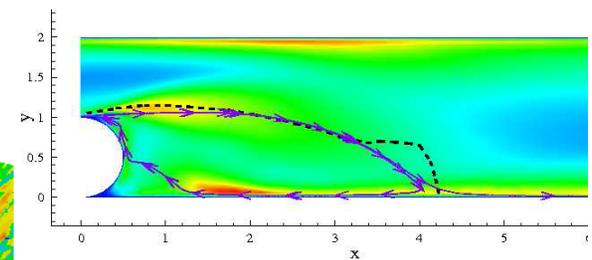
Wall Shear: No Cross-Flow



16% Cross-Flow



TKE, 16% CF



Separation in wire wake leads to increased variance in wall shear. Anticipate similar effects for heat transfer.

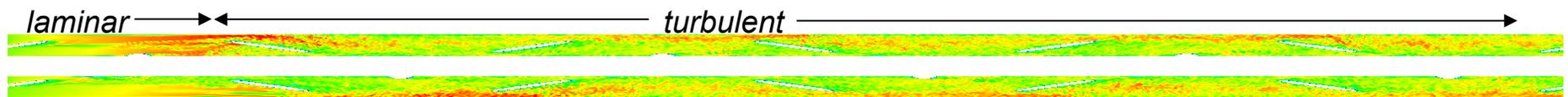
Ranjan, Pantano, & Fischer, *DNS of swept flow over a wire in a channel*, *J. Fluid Mech.*, 2009 (in review).

Key Findings 06-08: LES of SFR Subassemblies

7 pin wire-wrapped assemblies

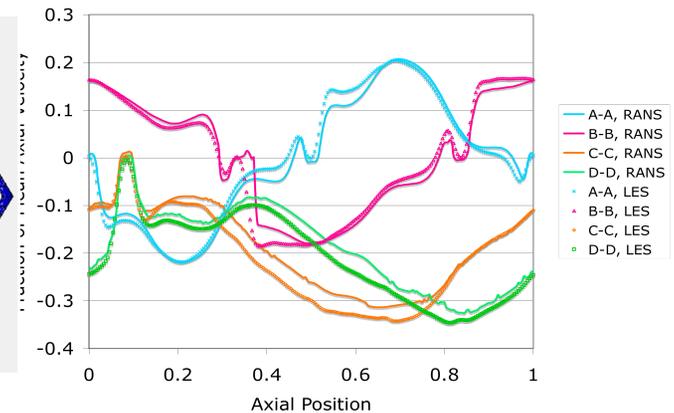
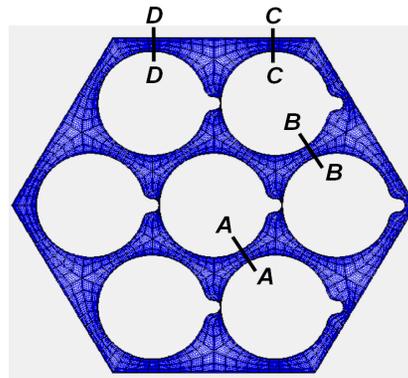
P. Fischer, A. Obabko and J. Lottes, Argonne

- Transition to turbulence with inflow/outflow boundary conditions occurs at $z \sim 30 D_h$
 - Verified in: single-pin x periodic array and 7-pin x 3H subassembly
 - Therefore: axial periodicity is warranted \rightarrow significant savings (10 x)



Transition in a 7-pin subassembly with laminar inflow conditions

- LES and RANS simulations give comparable results for cross-flow distributions in 7-pin case:
 - We have a mechanism for validating RANS, which gives considerable savings.
 - Data provides direct input to core-scale simulations



Velocity for RANS vs LES

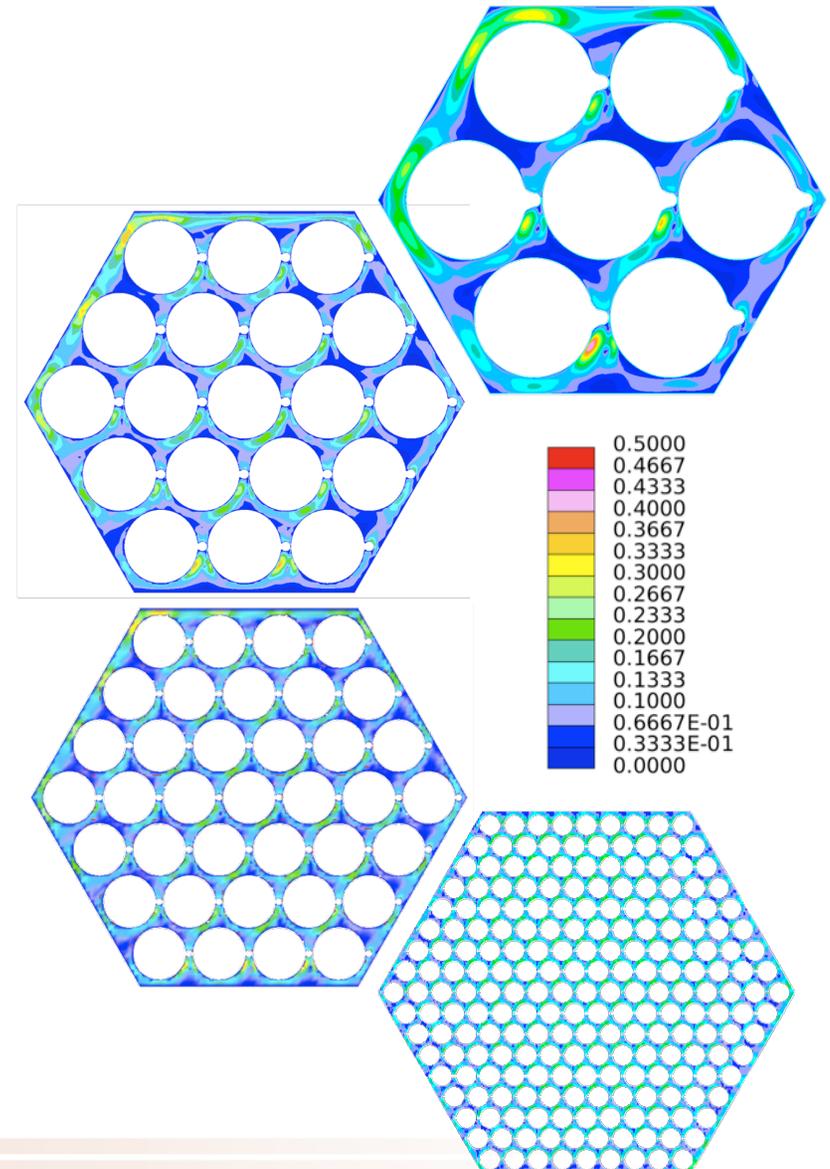


Key Findings 06-08: RANS Simulations of SFR Assemblies

7-37pin wire-wrapped assemblies

D. Pointer, Argonne and J. Smith, UIdaho

- Demonstrated evolution of flow field from 7 to 217 pin assemblies
 - Reduced importance of bulk swirling and increased complexity of flow field with increasing pin count
 - Fundamental change in flow behavior between 19- and 37-pin assemblies
 - Consistent with evidence in pressure drop data sets

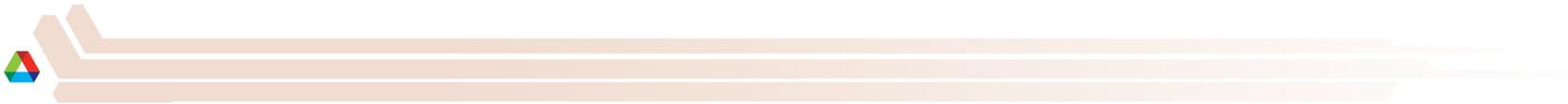


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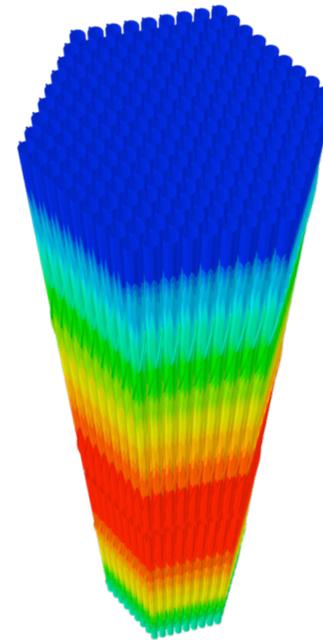


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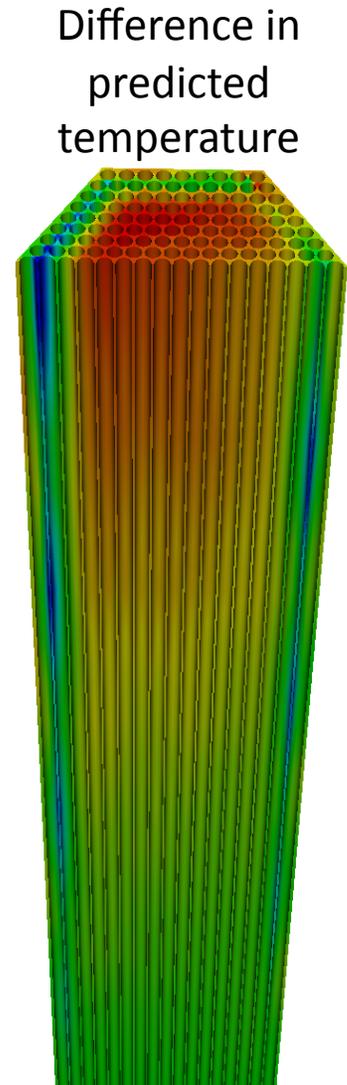
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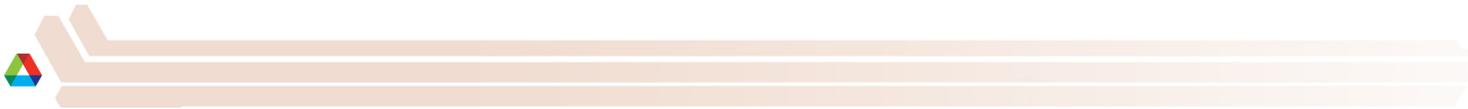
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Power
Distribution



Difference in
predicted
temperature



Predicted Dimensionless Pressure Loss Coefficient from RANS Simulations vs. Correlations

- The dimensionless pressure loss coefficient is the pressure drop normalized by the dynamic head, so that $C_p = f (L/D)$.
- The Cheng & Todreas correlation assumes that there are three fundamental sub-channel types: interior, edge, and corner. Each of the three types of sub-channel frictional losses is calculated separately. The bundle friction factor is then averaged.
- The Rehme correlation is a simpler single equation formulation based on representative geometric parameters.

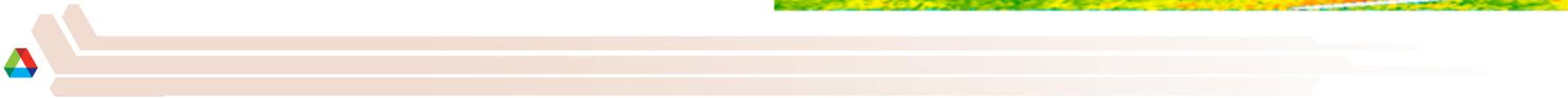
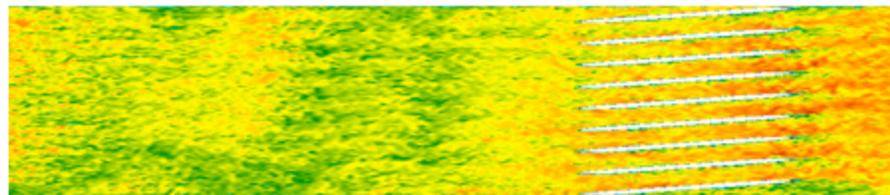
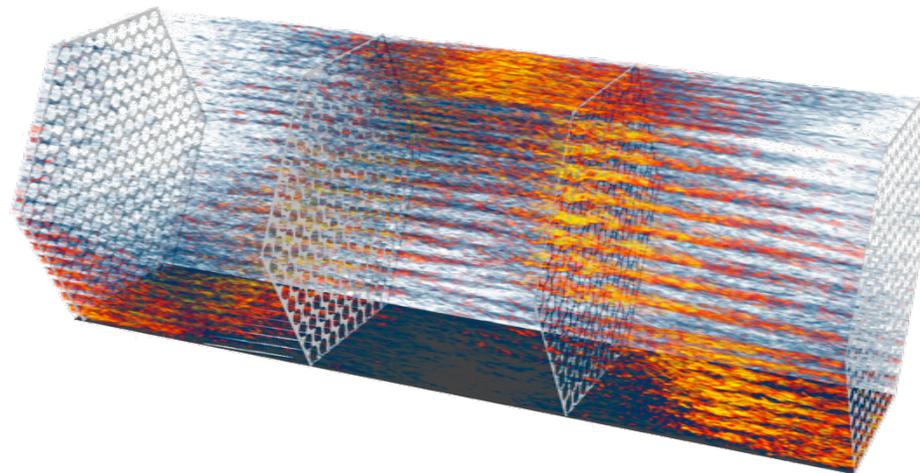
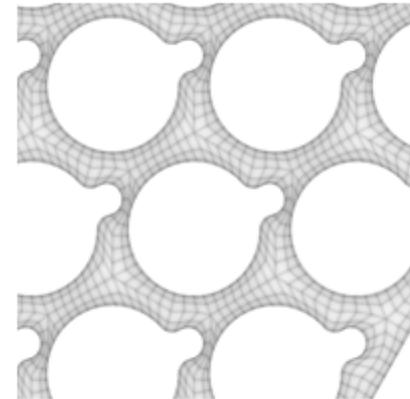
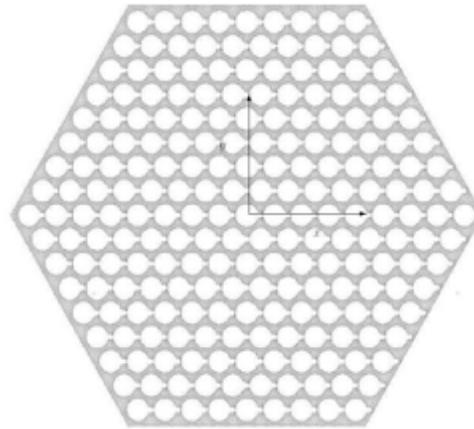
Number of Pins	Cheng & Todreas Correlation	Rehme Correlation	RANS Simulation Prediction
7*	1.116 ± 14%	1.179 ± 5%	2.282
19	1.088 ± 14%	1.041 ± 5%	1.199
37	1.075 ± 14%	0.943 ± 5%	1.059

* Small 7-pin assemblies are not within the range of applicability of the correlations



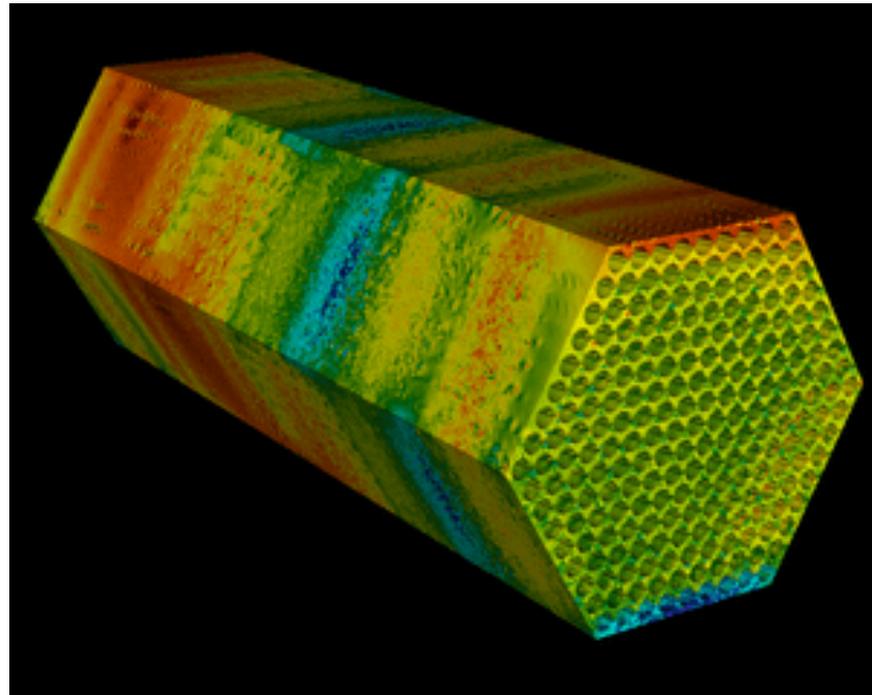
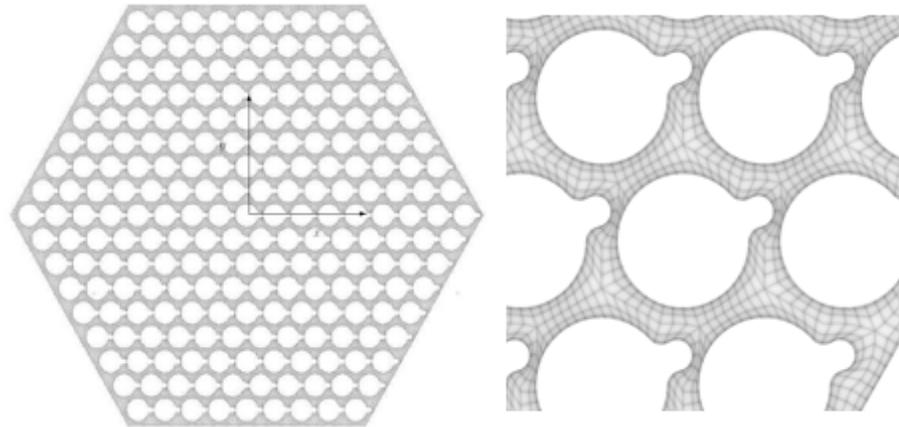
LES Simulations of 217 pin assemblies

- Using spectral element code Nek5000
 - Single wire pitch H with periodicity in the axial direction
 - Reynolds number reduced to $Re_D=15000$ to reduce computational burden
 - Based on prior experience with smaller assemblies
 - Confirm scaling with RANS simulations
 - 2.95 million spectral elements of order $N=7$ ($n=1.01$ billion)
 - Have also run $N=9$ ($n=2.1$ billion)
 - Under-resolved – particularly axially
 - 4x larger than any previous Nek5000 run



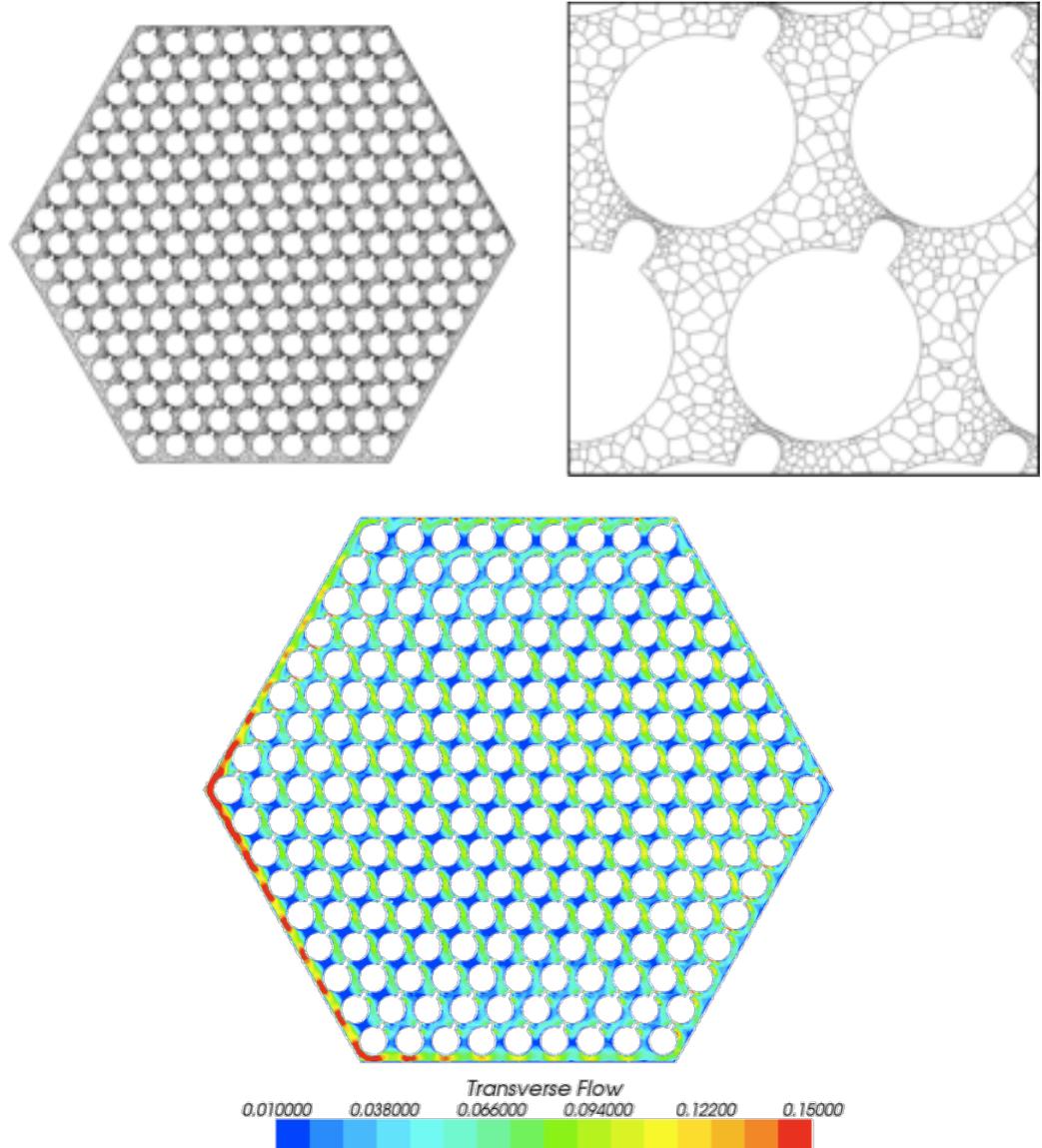
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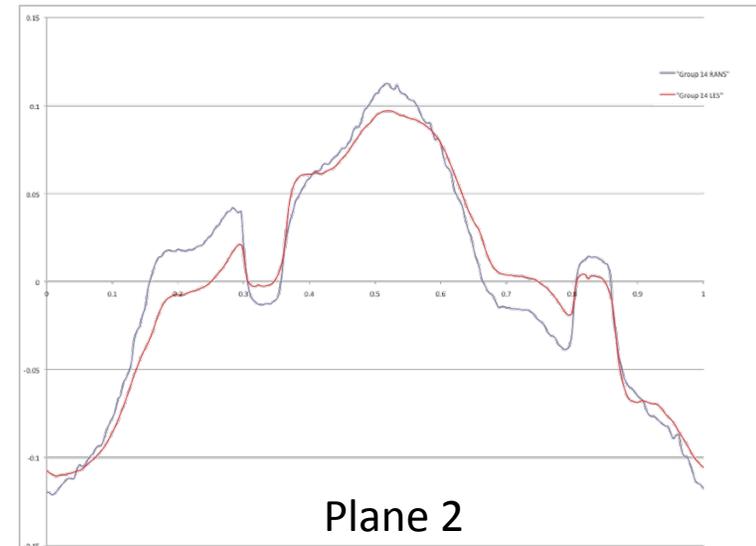
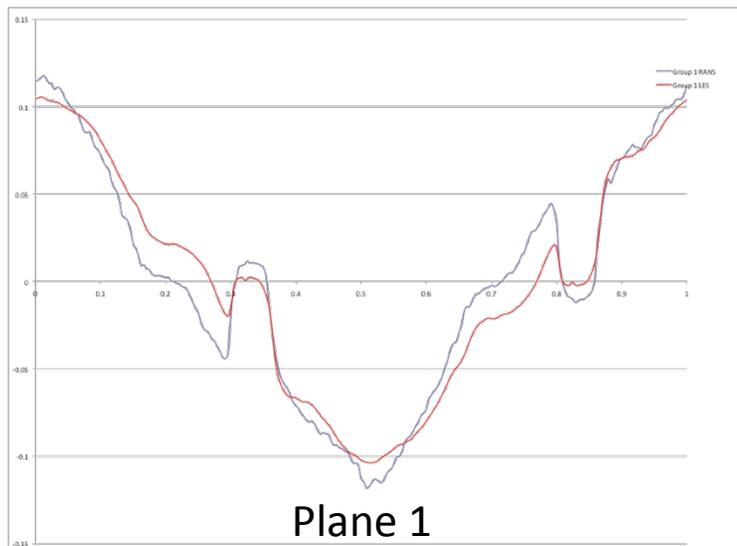
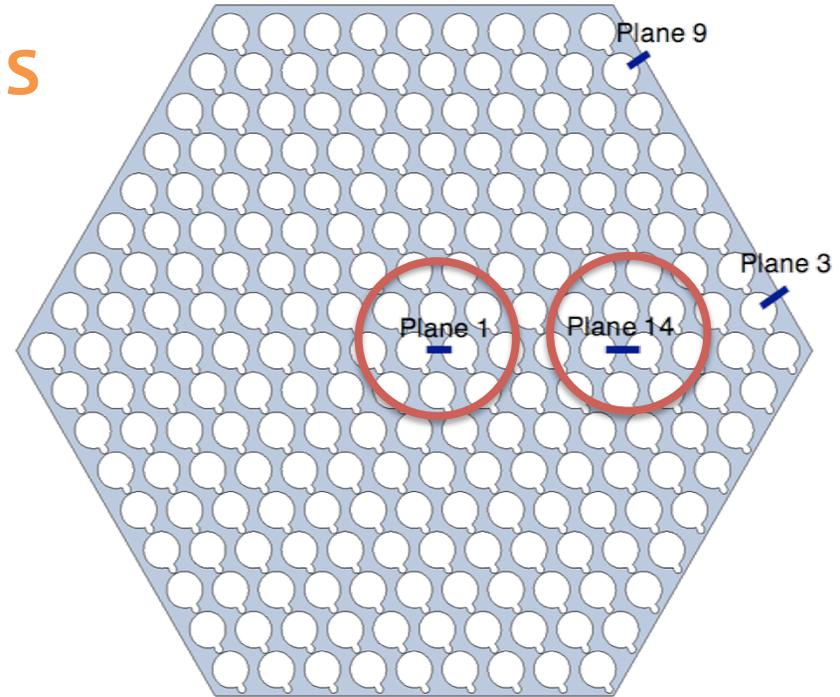
RANS Simulations of 217 pin assemblies

- Using commercial code STAR-CCM+
 - 5 wire pitches, 5H, with inflow/outflow boundary conditions
 - Reynolds number reduced to $Re_D=15000$ to match LES conditions
 - 22 million cells
 - Have also run $n=44$ million
 - Under-resolved – particularly axially



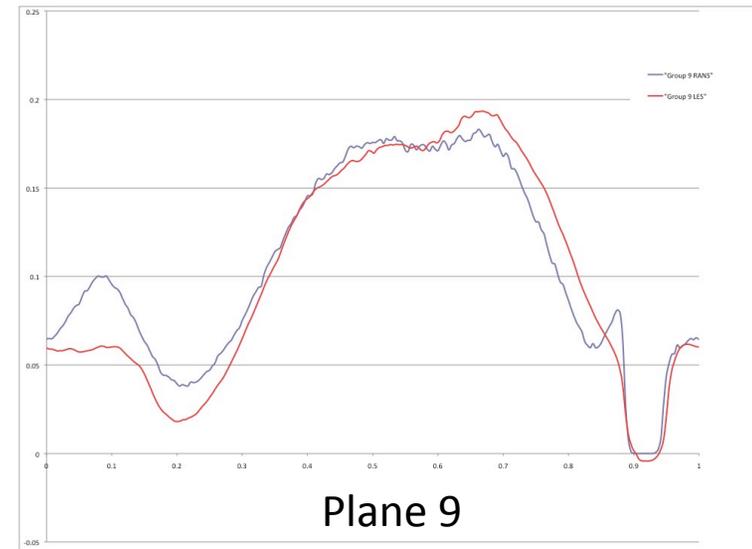
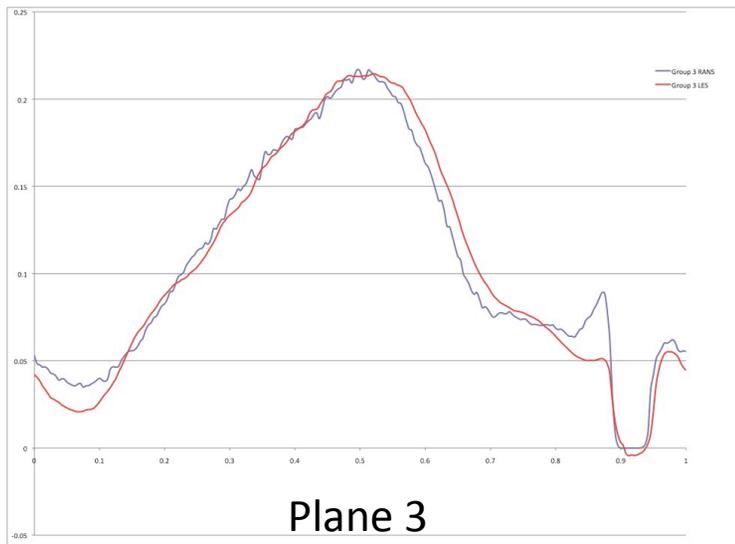
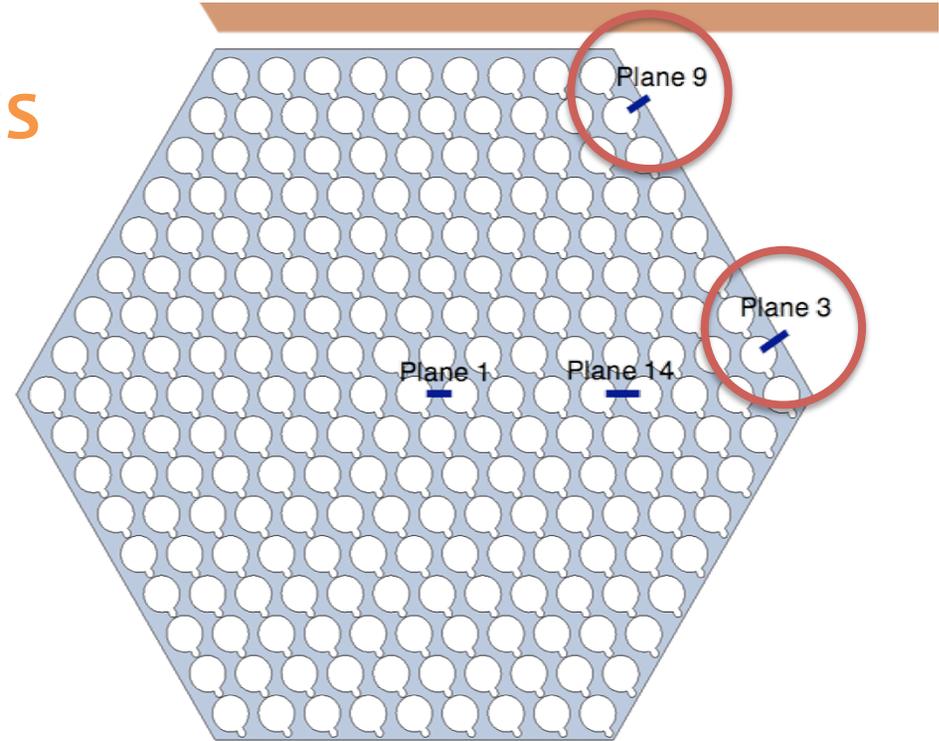
Benchmarking of LES vs RANS

- Extract field data along selected planes.
- Calculate velocity component normal to plane
- Average data across plane to collapsed data to an axial profile of average normal velocity



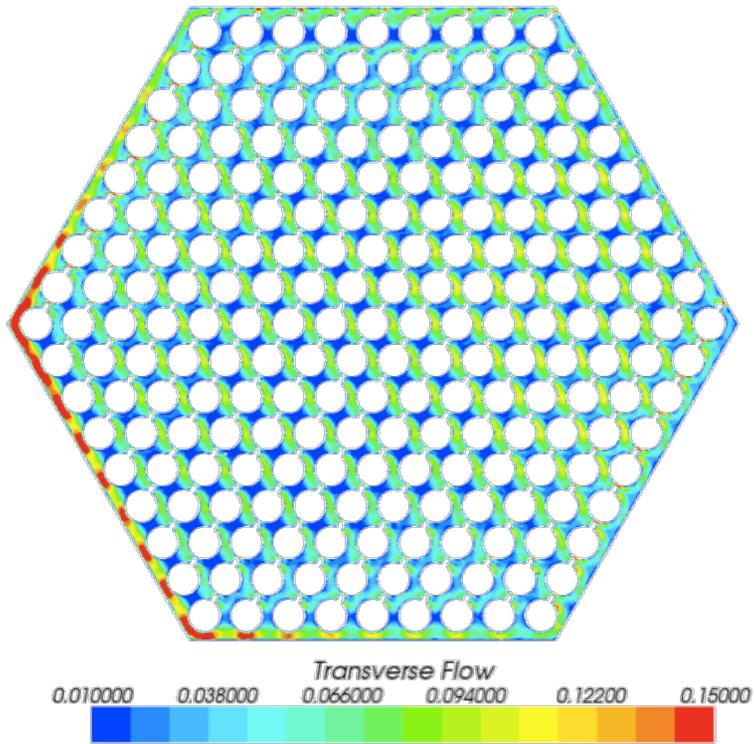
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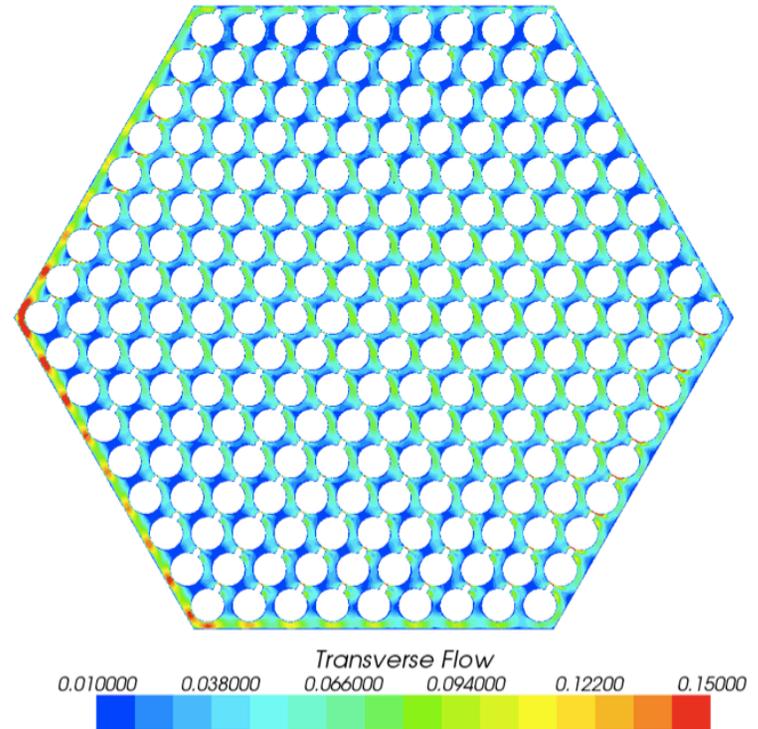


RANS Simulations

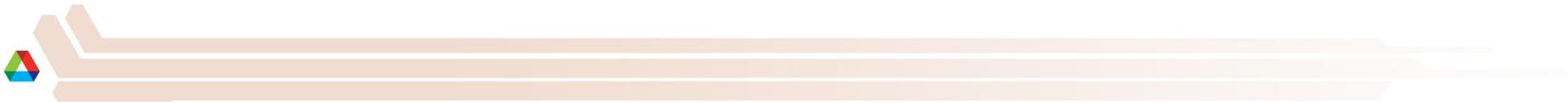
$Re_h=15000$ vs $Re_h=108,000$



Re = 15,000

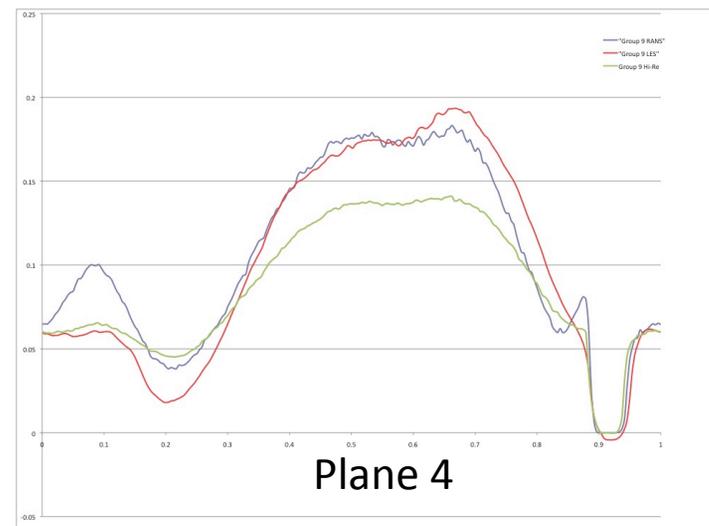
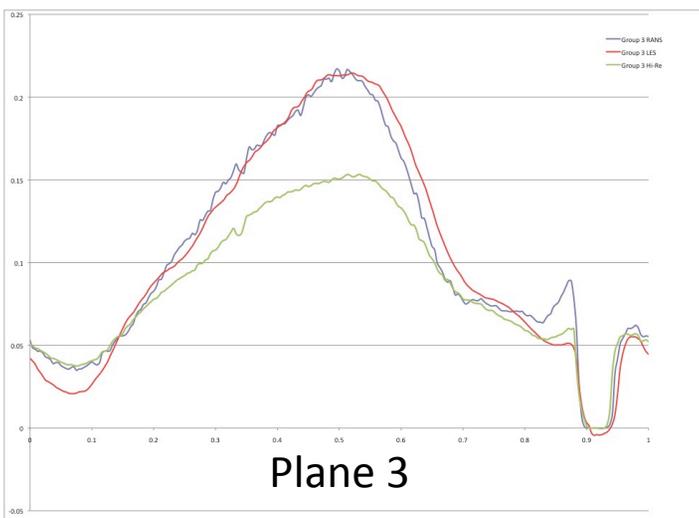
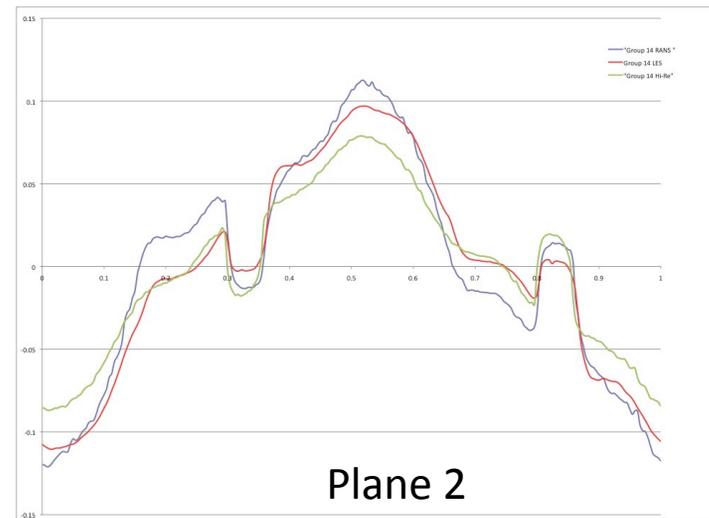
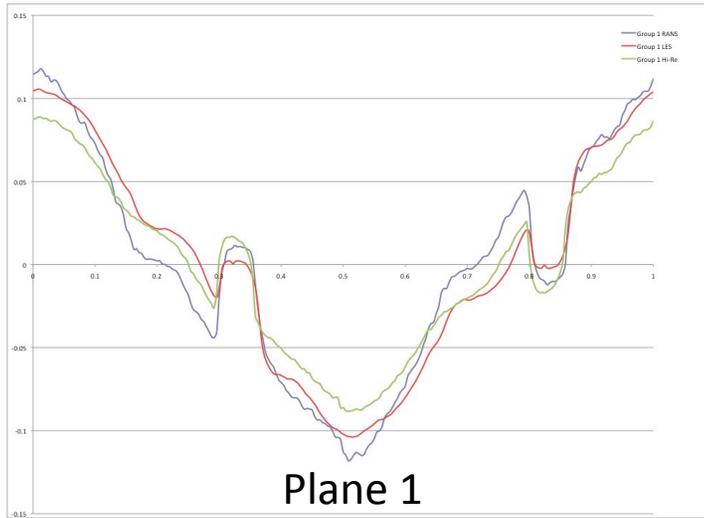


Re = 108,000



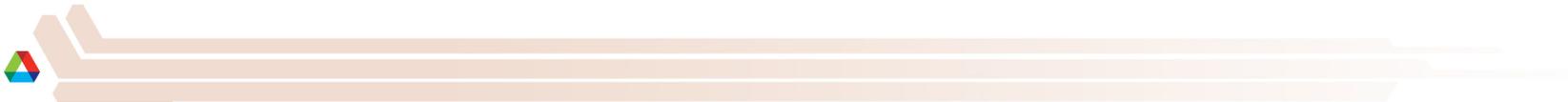
RANS Simulations

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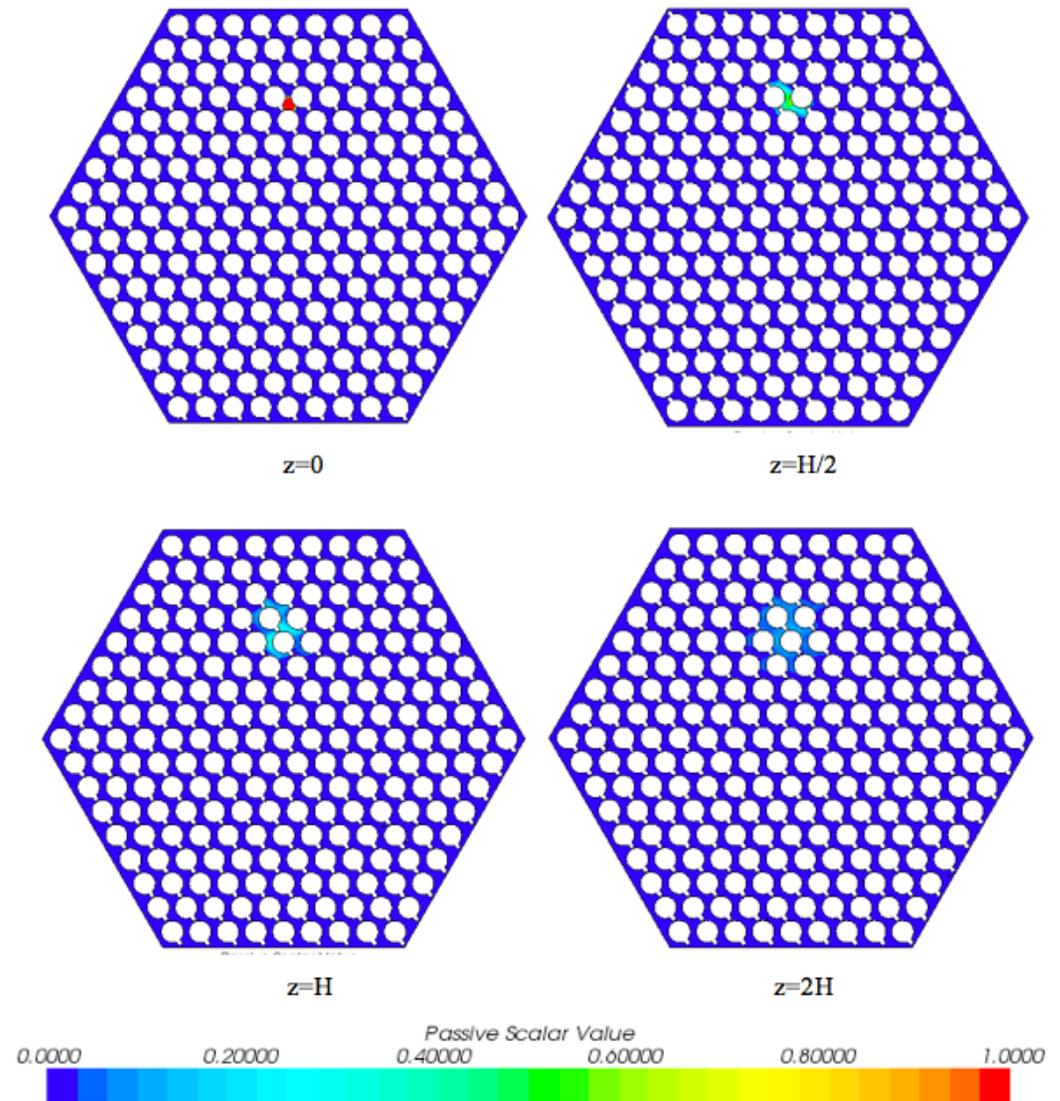
Conclusions

- A series of LES and RANS based CFD simulations of a 217-pin wire-wrapped sodium-cooled fast reactor fuel assembly have been completed
 - initial benchmark of RANS models against high fidelity LES simulations in large wire wrapped pin bundles.
- Initial comparisons show that RANS and LES predict similar transverse flow fields within the assembly – a well mixed flow through the central channels and a swirling flow through the edge channels along the assembly boundary.
 - Much different than the flow field in 7- and 19-pin assemblies where swirling flow dominates
- Comparisons of RANS to 1-D subchannel simulations reveal bias in temperature distribution as a consequence of azimuthal starting position of the wire relative to can wall.
- Comparisons of detailed inter-channel exchange velocity profiles show that the two methods generally agree.
 - RANS simulations tend to predict more inter-channel mixing
 - Less turbulence generation on the windward side of the wire wrap spacer



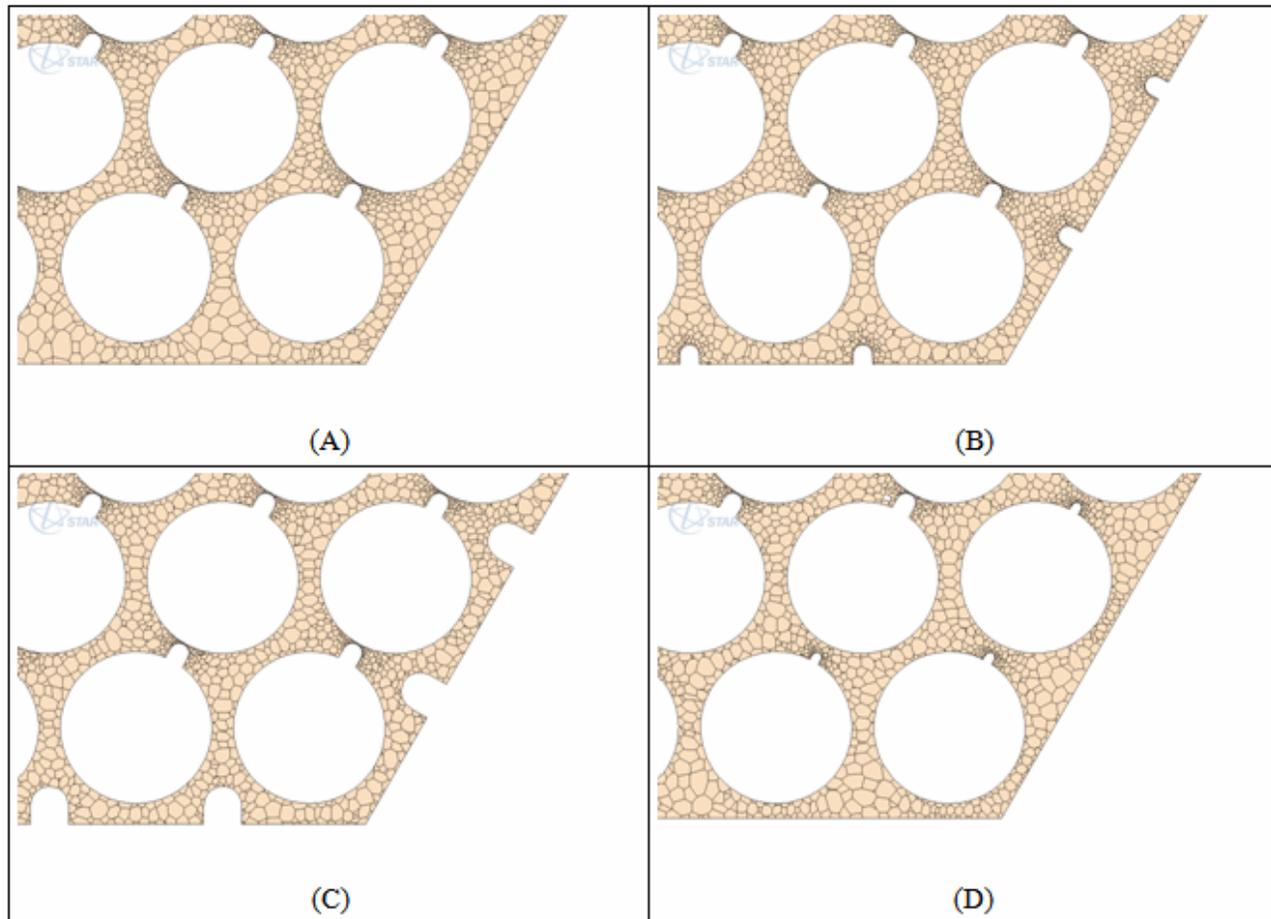
Current Efforts: Turbulent Diffusion

- Benchmarking of turbulent diffusion based on legacy experiments
- Water experiments using conduction probes to track plume diffusion
 - Use single injection port in variety of sub-channel locations
- For the interior channels, one observes that fluid is swept into the channel from which the wire is exiting.
- Discharge into the other subchannels is not evenly split between the neighboring subchannels – there is a significant bias for the flow to follow the wire
- By $z=H$, the peak concentration has typically moved two or three channels.



Current Efforts: Design Studies

- Alternative edge channel geometries
- Wire wrap vs. Spacer Grid



Questions?

