

Study on the in-core-instrumentation tube ejection failure at APR1400 lower reactor vessel

2015. 2. 17

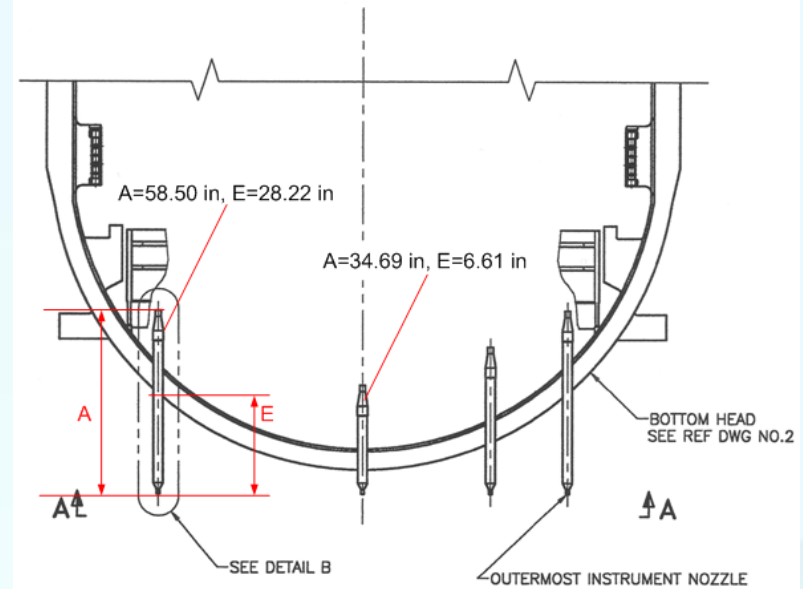
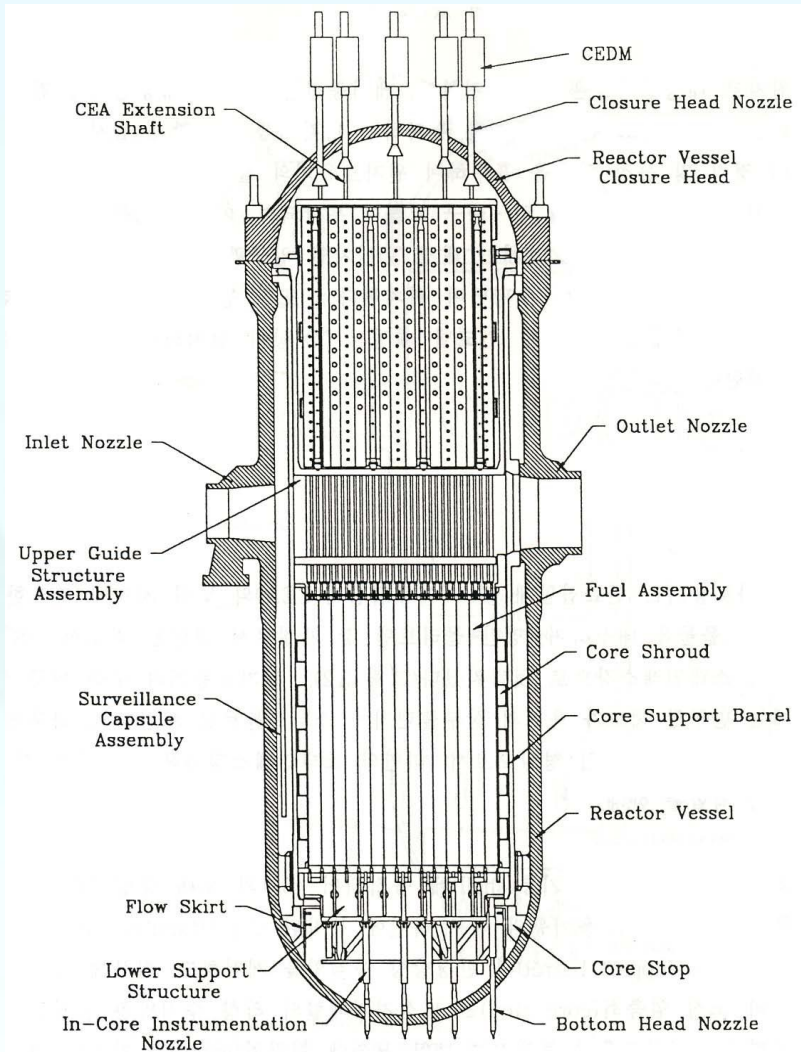
Hwan Yeol Kim

Severe Accident & PHWR Safety Research Division

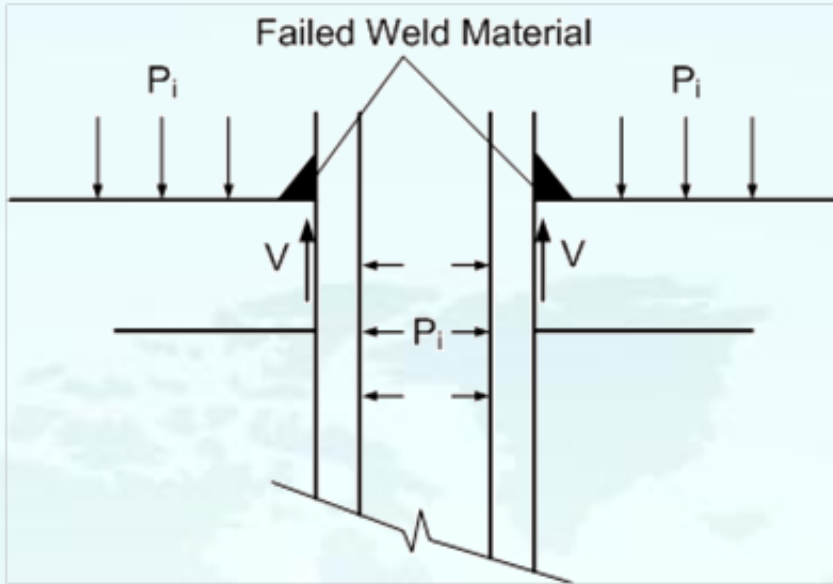


한국원자력연구원
Korea Atomic Energy Research Institute

ICI Penetration for APR1400

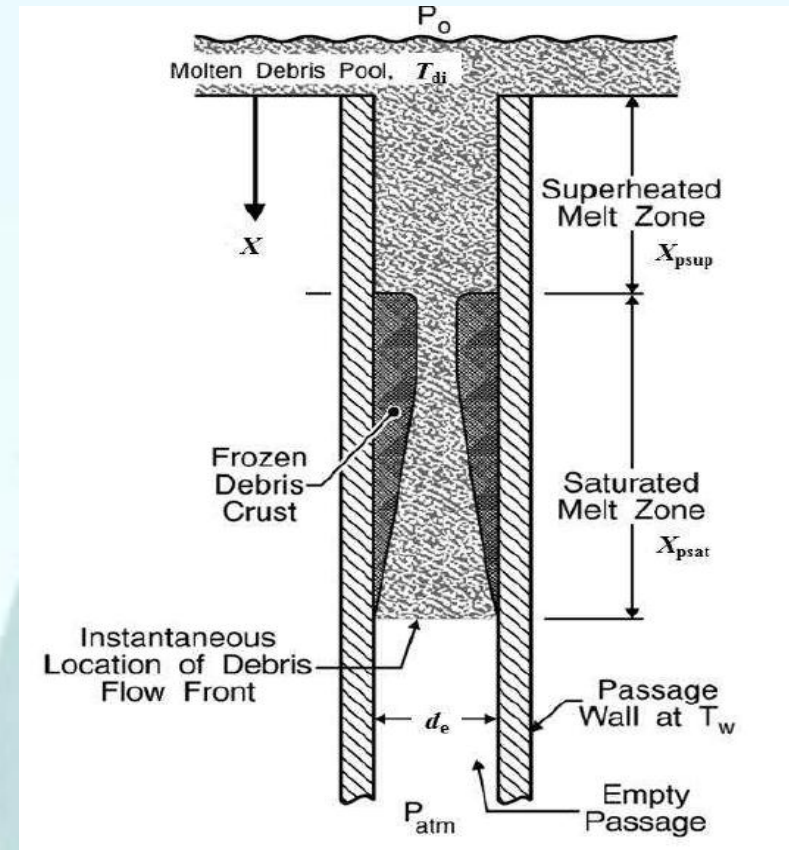


ICI Penetration Failure



Penetration tube ejection & rupture

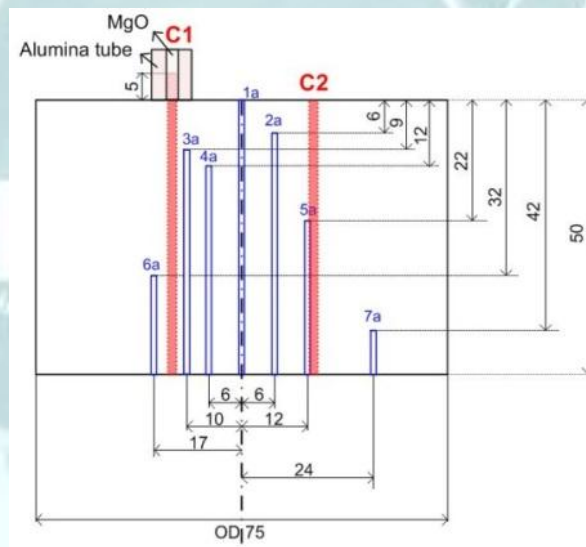
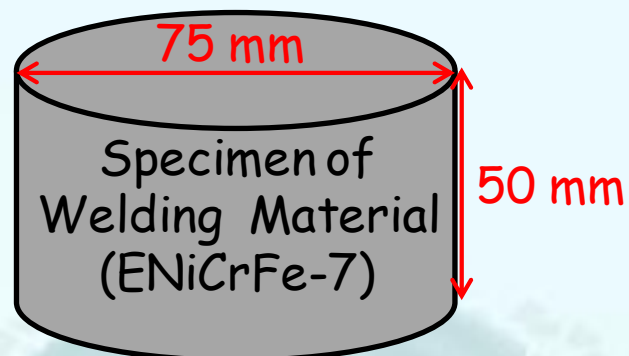
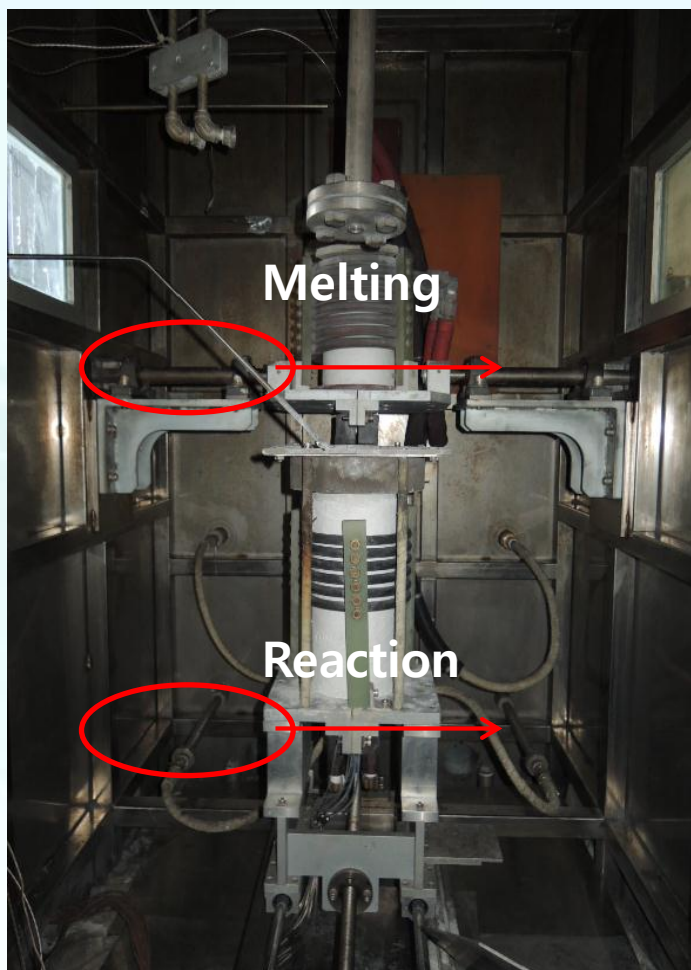
Compare P_i and V



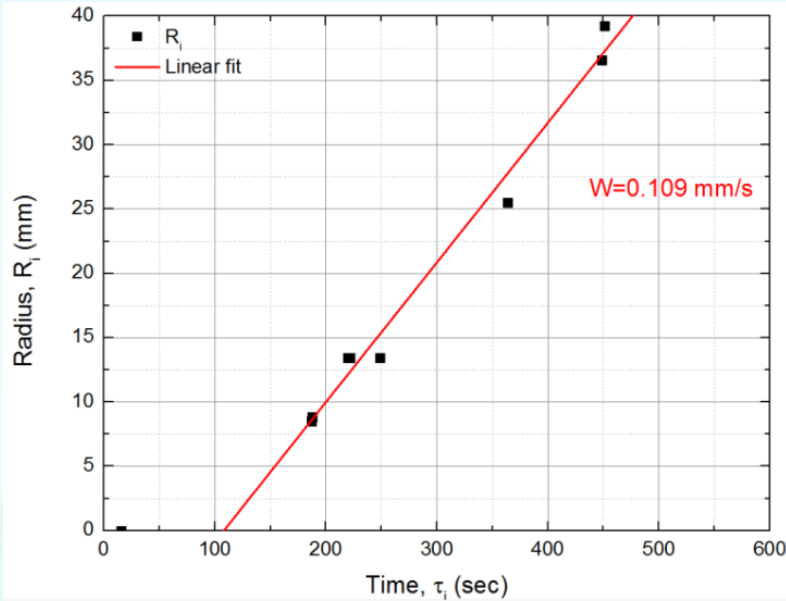
Penetration tube heat-up & rupture

Welding Erosion Test (1)

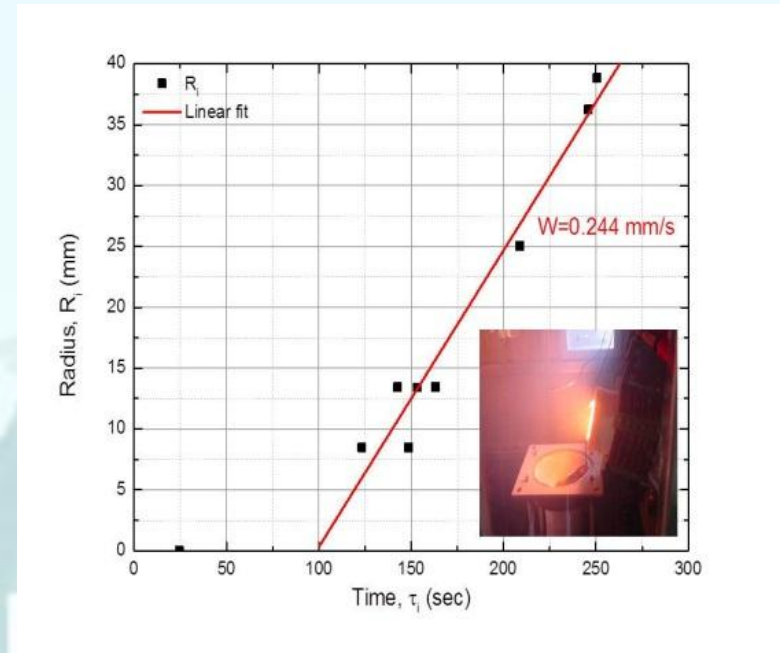
VESTA-S Test Facility



Welding Erosion Test (2)



Composition:
Fe 46%, U 31%, Zr 16%, Cr 7%)
Mass:
3.129 kg



Composition:
SUS304 (Cr 19%, Ni 11%, Fe 70%)
Mass: 2.2155 kg

ICI Penetration Failure Test (1)

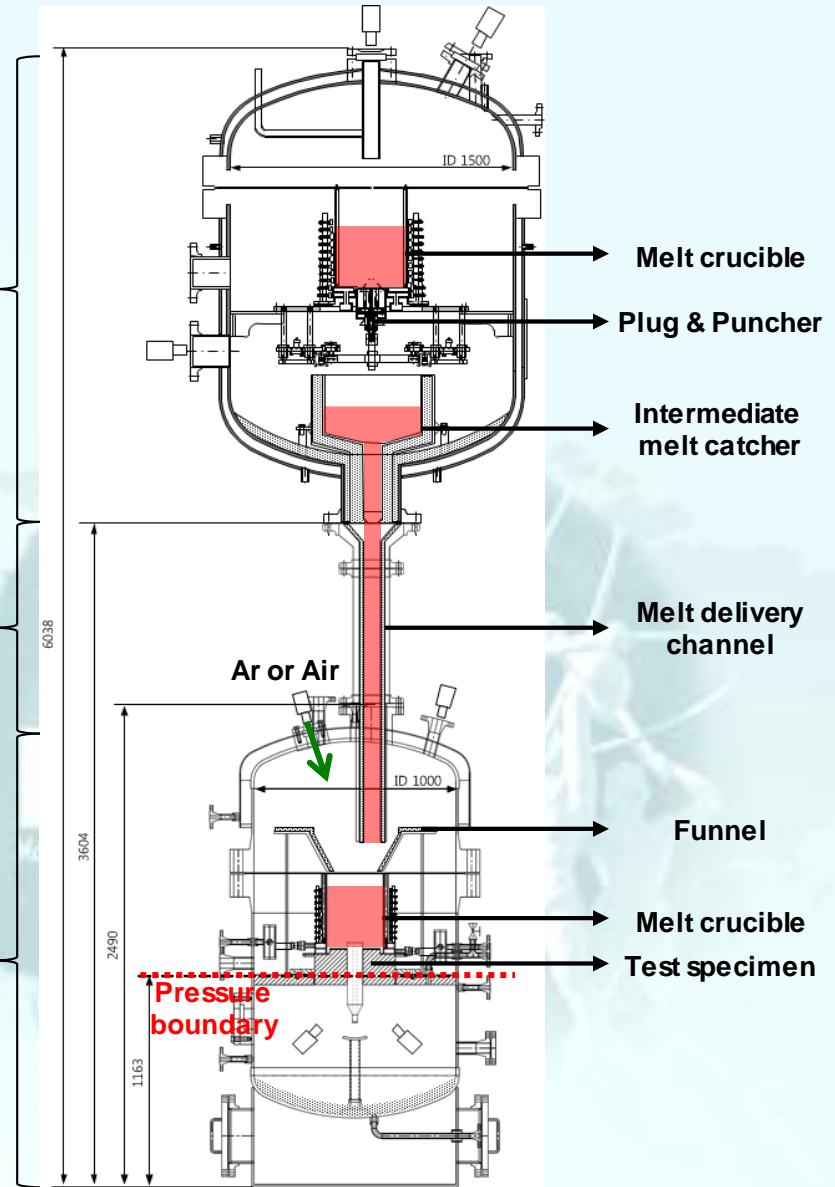


Furnace vessel (VESTA)



Melt delivery channel

Interaction vessel



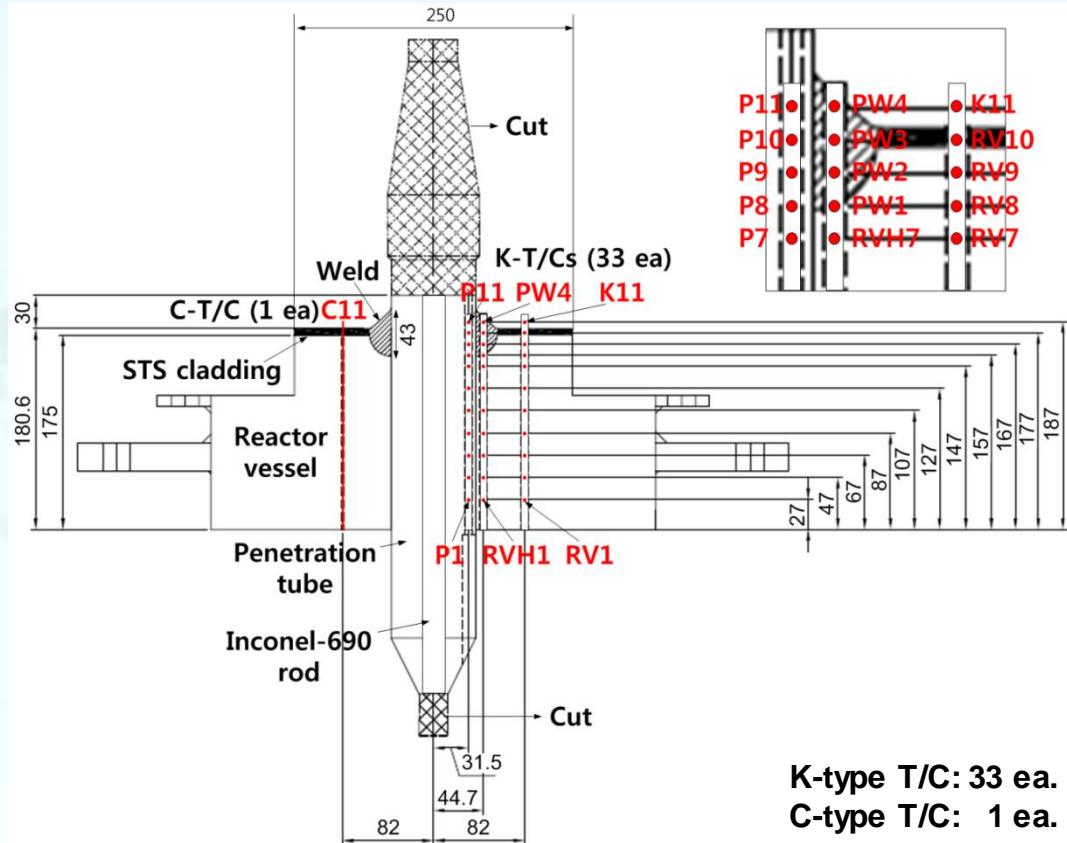
ICI Penetration Failure Test (2)

□ Penetration test specimen



Penetration test specimen

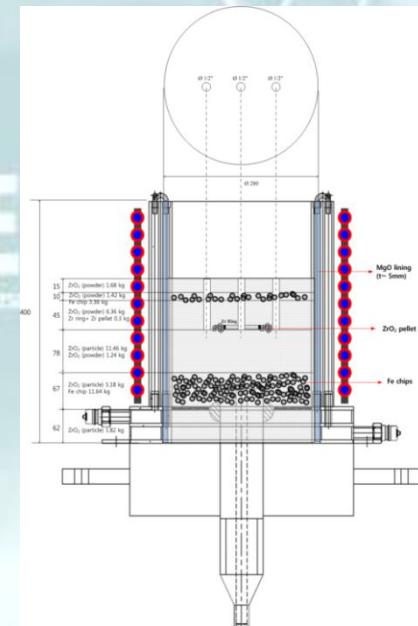
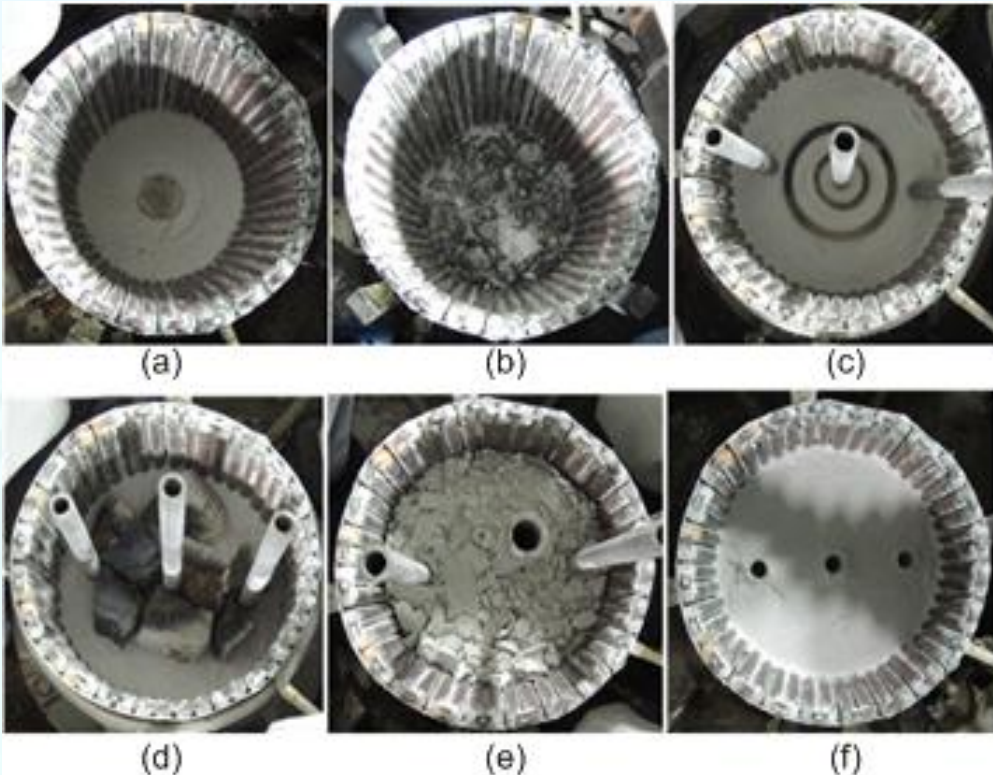
(DOOSAN Heavy Industries and Construction. Co., Ltd.)



- C11, K11 : Melt temperature
- P1-P11 : Penetration tube temperature
- PW1-PW4 : Penetration weld temperature
- RVH1-RVH7 : Reactor vessel hole temperature
- RV1-RV10 : Reactor vessel temperature

ICI Penetration Failure Test (3)

❑ Melt Material Charging



○ ZrO₂ : Fe = 66 : 34 (wt%)

○ Charging mass: 44.16 kg

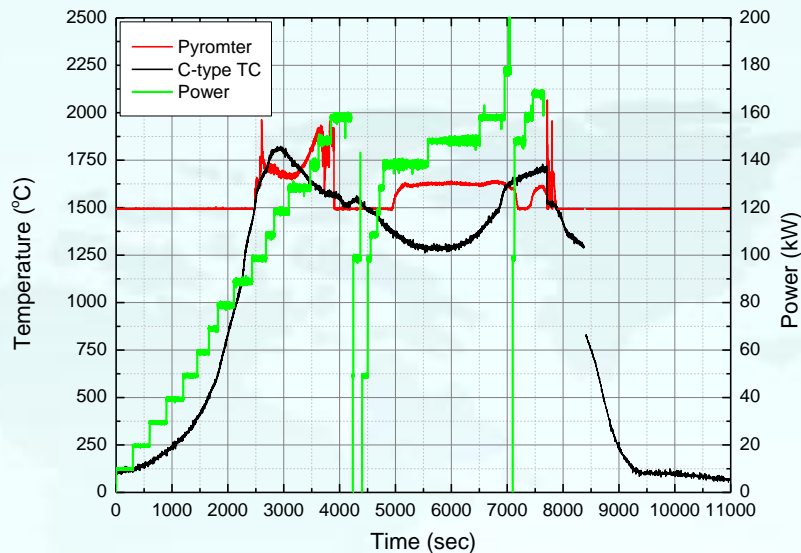
‣ ZrO₂ powder: 29.16 kg

‣ Fe: 15.00 kg

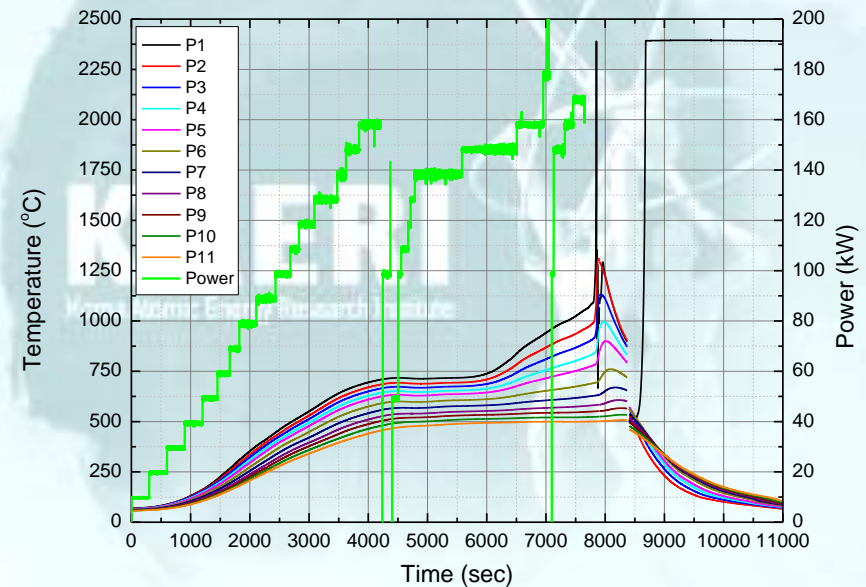
‣ Zr ring: small

ICI Penetration Failure Test (4)

Melt Temp.

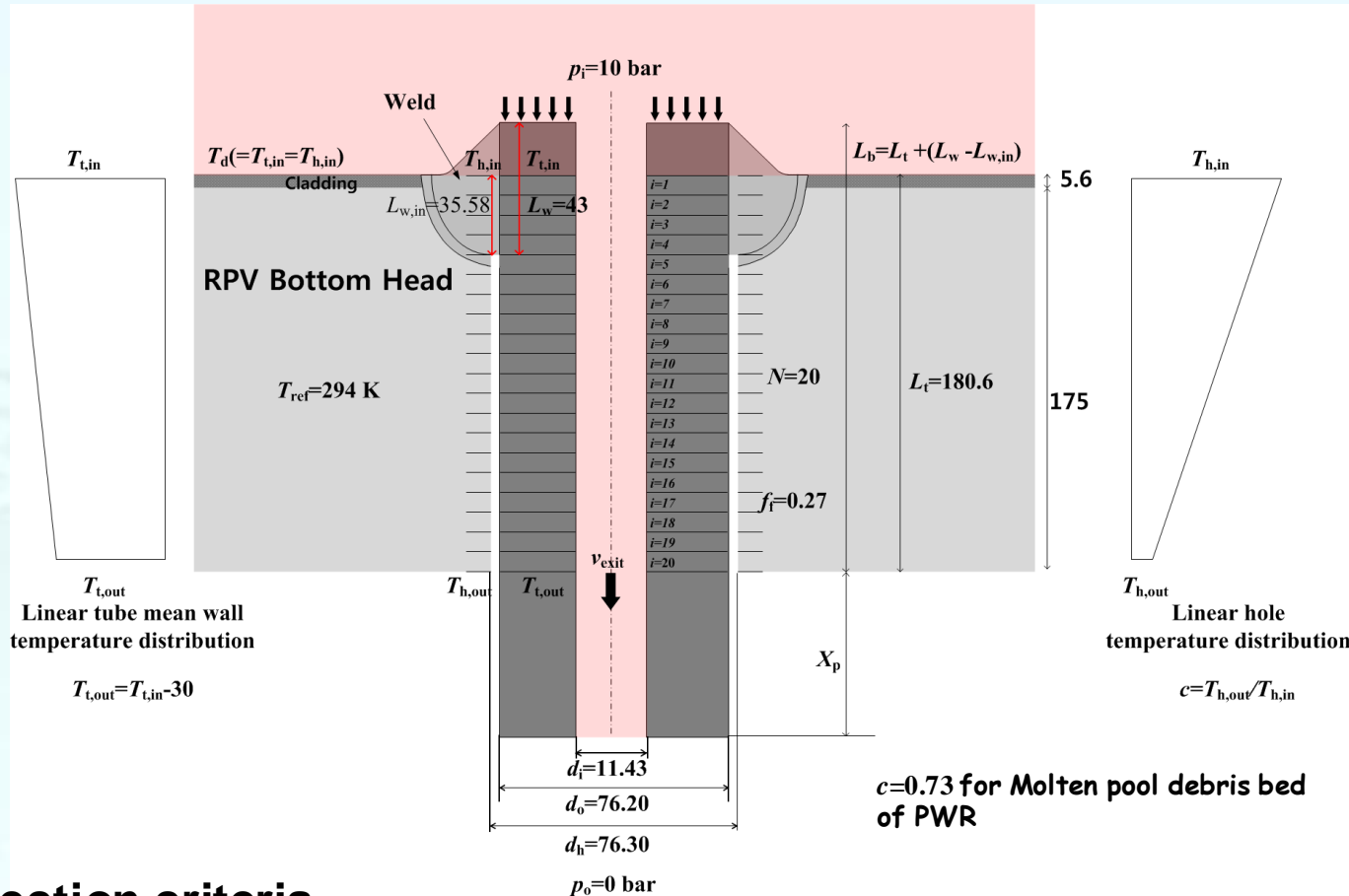


Penetration tube Temp.



Failure Models & Calculations (1)

□ Tube Ejection (Weld failure)



■ Ejection criteria

$$F_p > V_T$$

where, V_T : Total thermal binding shear force
 F_p : Ejecting pressure force

Failure Models & Calculations (2)

□ Tube Ejection

1. Free thermal expansion of tube and hole

$$\text{Tube: } \Delta r_o^T = r_o \alpha_t (T_t - T_{\text{ref}}), \quad T_{\text{ref}} = 294 \text{ K}$$

$$\text{Hole: } \Delta r_h^T = r_h \alpha_h (T_h - T_{\text{ref}}), \quad T_{\text{ref}} = 294 \text{ K}$$

2. Pressure expansion of tube

$$\text{Tube: } \Delta r_o^P = \frac{p_i}{E} \cdot \frac{r_o r_i (2 - \nu_t)}{(r_o^2 - r_i^2)}$$

$$\text{Hole: } \Delta r_h^P = 0$$

- The pressure expansion of hole is negligibly small.

3. Total expansion of tube

$$\text{Tube: } \Delta r_o = \Delta r_o^T + \Delta r_o^P$$

4. Tube-hole radial gap at temperature and pressure

$$\delta_i = (r_h + \Delta r_h) - (r_o + \Delta r_o)$$

+ → *gap*

- → *interface*

5. Tube-hole interface pressure

$$\delta_i < 0: P_{\text{th}} = \text{lesser of } \left\{ \begin{array}{l} \frac{\delta_i \cdot E (r_o^2 - r_i^2)}{r_o [r_o^2 (1 - 2\nu_t) + r_i^2 (1 + \nu_t)]} \\ \frac{2}{\sqrt{3}} \sigma_u \ln \left(\frac{r_o}{r_i} \right) \end{array} \right\}$$

Required interfacial pressure to force the outer diameter of the tube to conform to the diameter of the hole after free expansion

Required pressure to cause compression failure of the tube material

6. Total thermal binding shear

$$V_T = \sum_{n=1}^n f \cdot P_{\text{th}} 2\pi r_o \Delta l_t$$

f : not a f (temp.), but a f (roughness)

- 0.27 for high-temperature, oxidized conditions

7. Ejecting pressure force

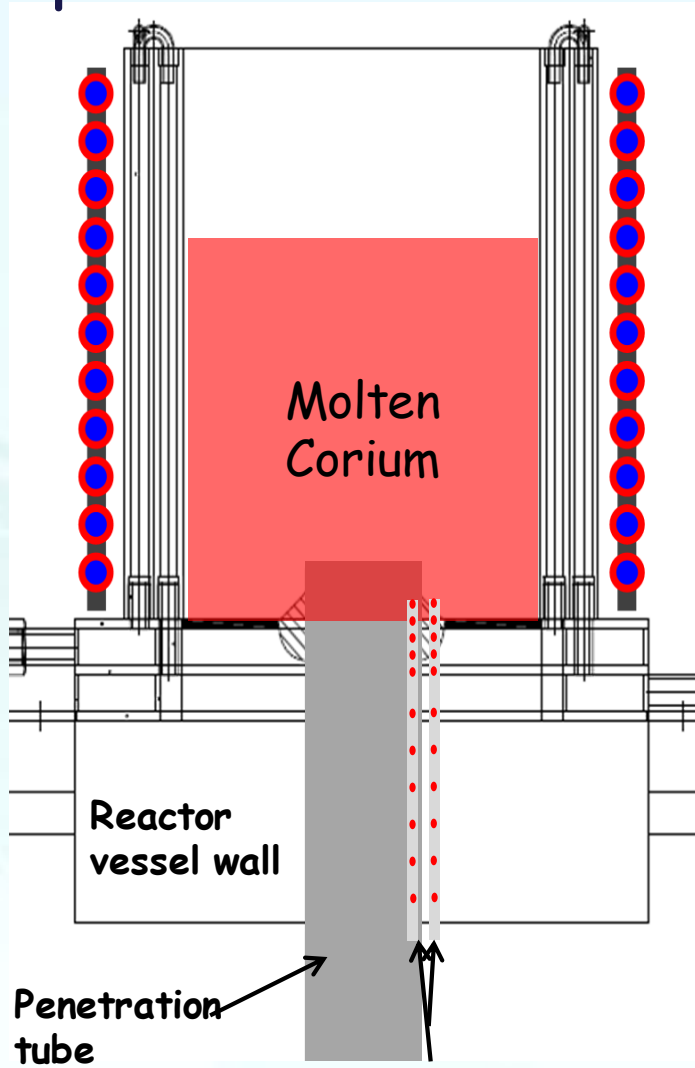
$$F_p = p_i \pi r_o^2$$

8. Ejection criteria

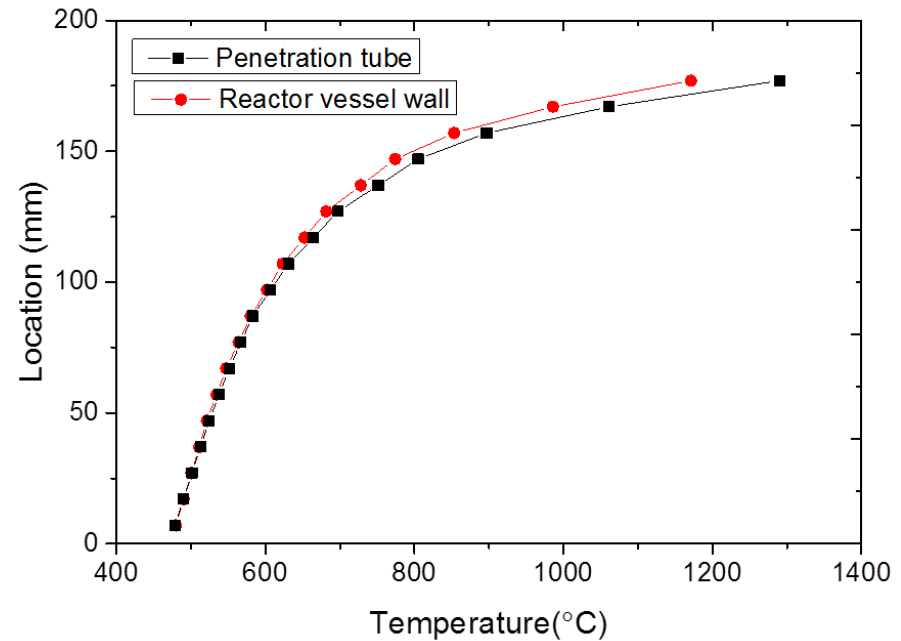
$$F_p > V_T$$

Failure Models & Calculations (3)

○ Experimental results

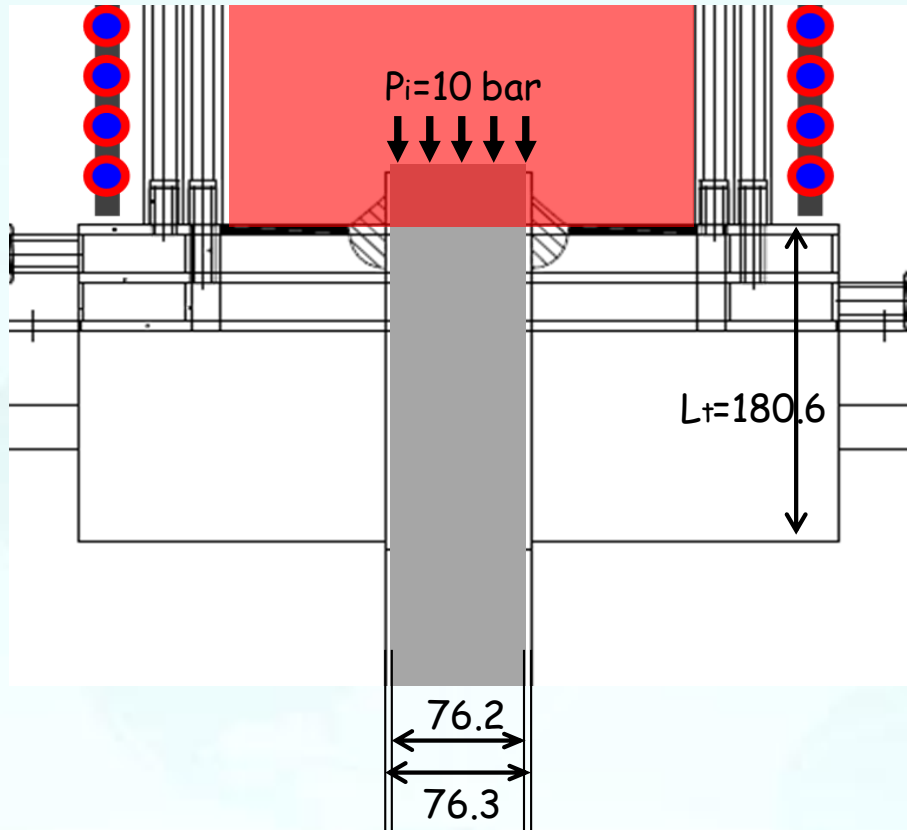


✓ Temperature distribution



Failure Models & Calculations (4)

□ Tube Ejection



○ Input data

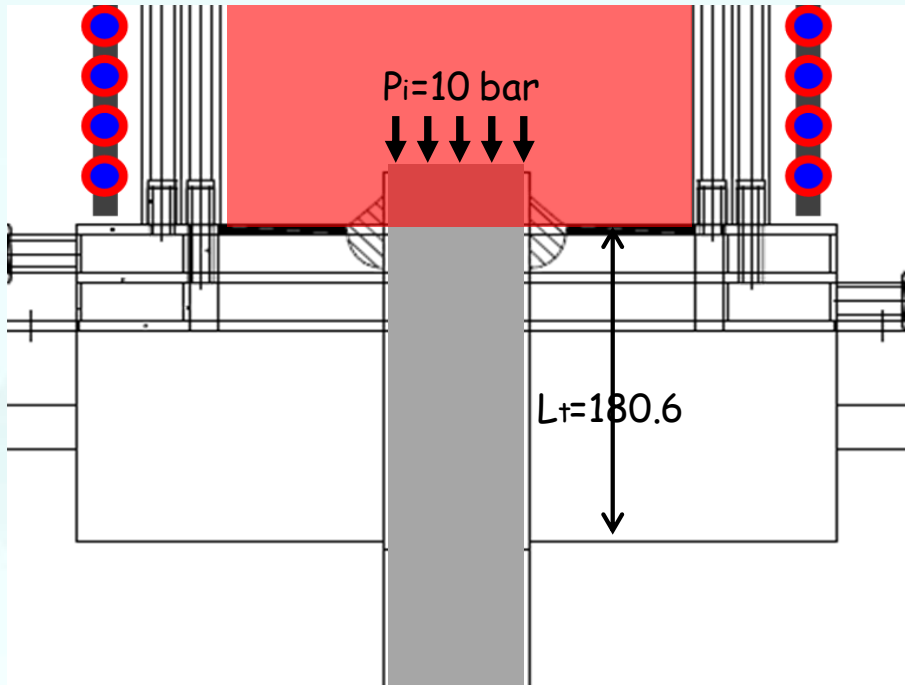
- ✓ Obtained temperature profile

○ Assumption

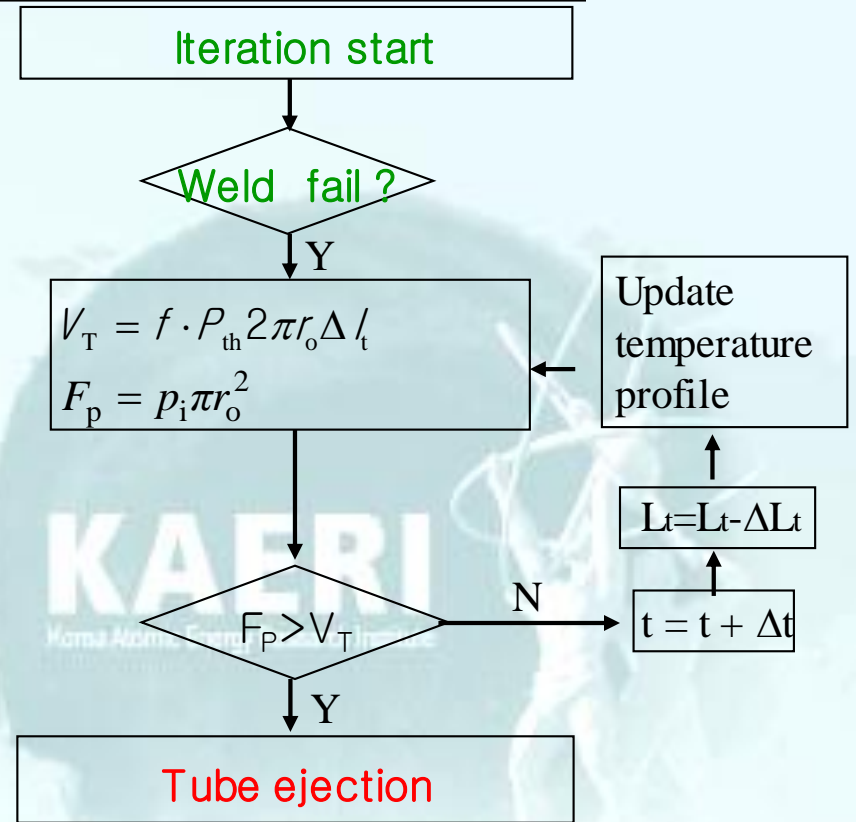
- ✓ $P_i = 10 \text{ bar}$
- ✓ Clearance gap size: same as normal operating condition
- ✓ Top surface temp. up to $2600 \text{ }^\circ\text{C}$ while maintaining similar temp. profile

Failure Models & Calculations (5)

□ Tube Ejection (Weld failure)



Simplified Flow Diagram



▪ Ejection criteria

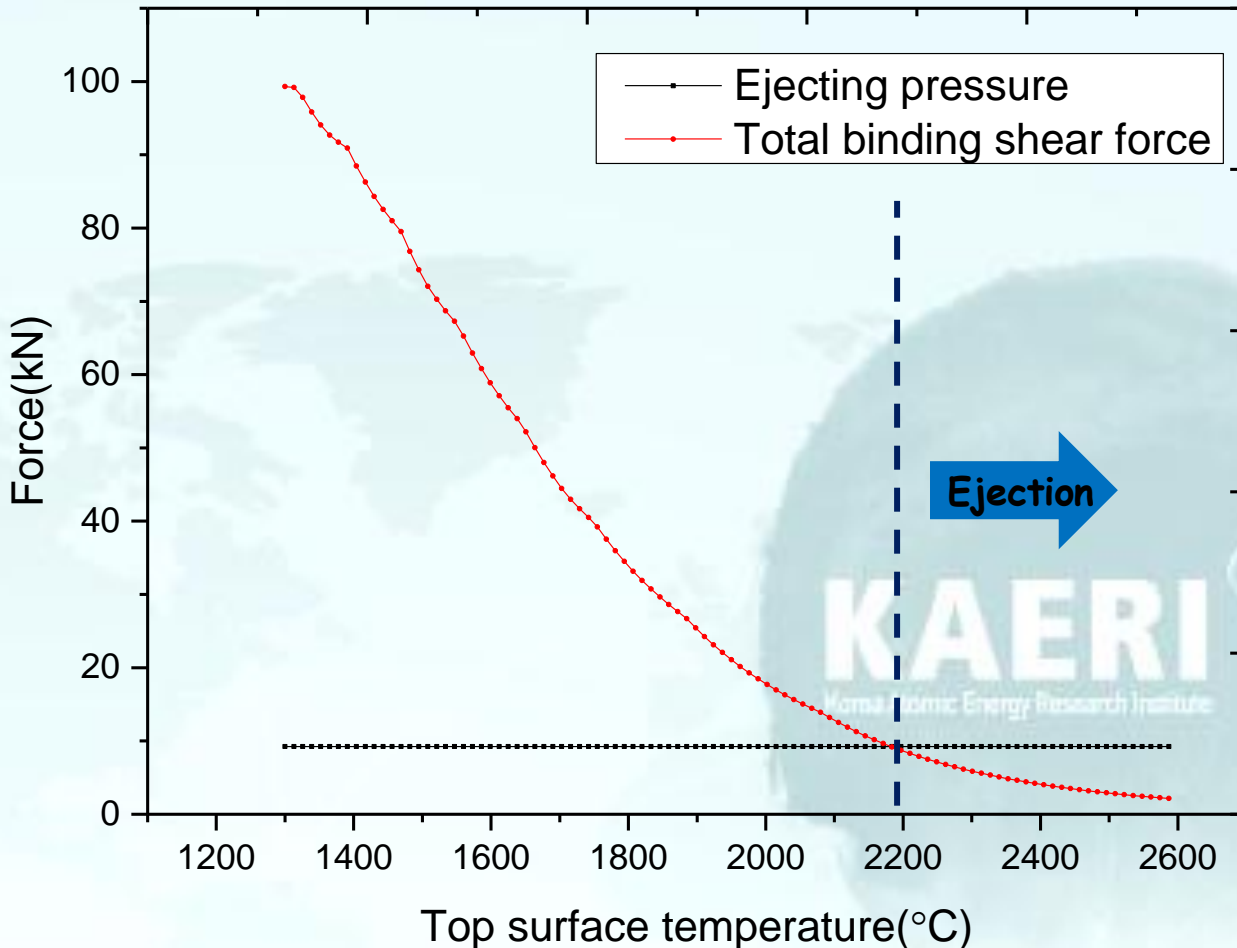
$$F_p > V_T$$

where,

V_T : Total thermal binding shear force, $f \cdot P_{th} 2\pi r_o \Delta l_t$
 F_p : Ejecting pressure force, $p_i \pi r_o^2$

Failure Models & Calculations (6)

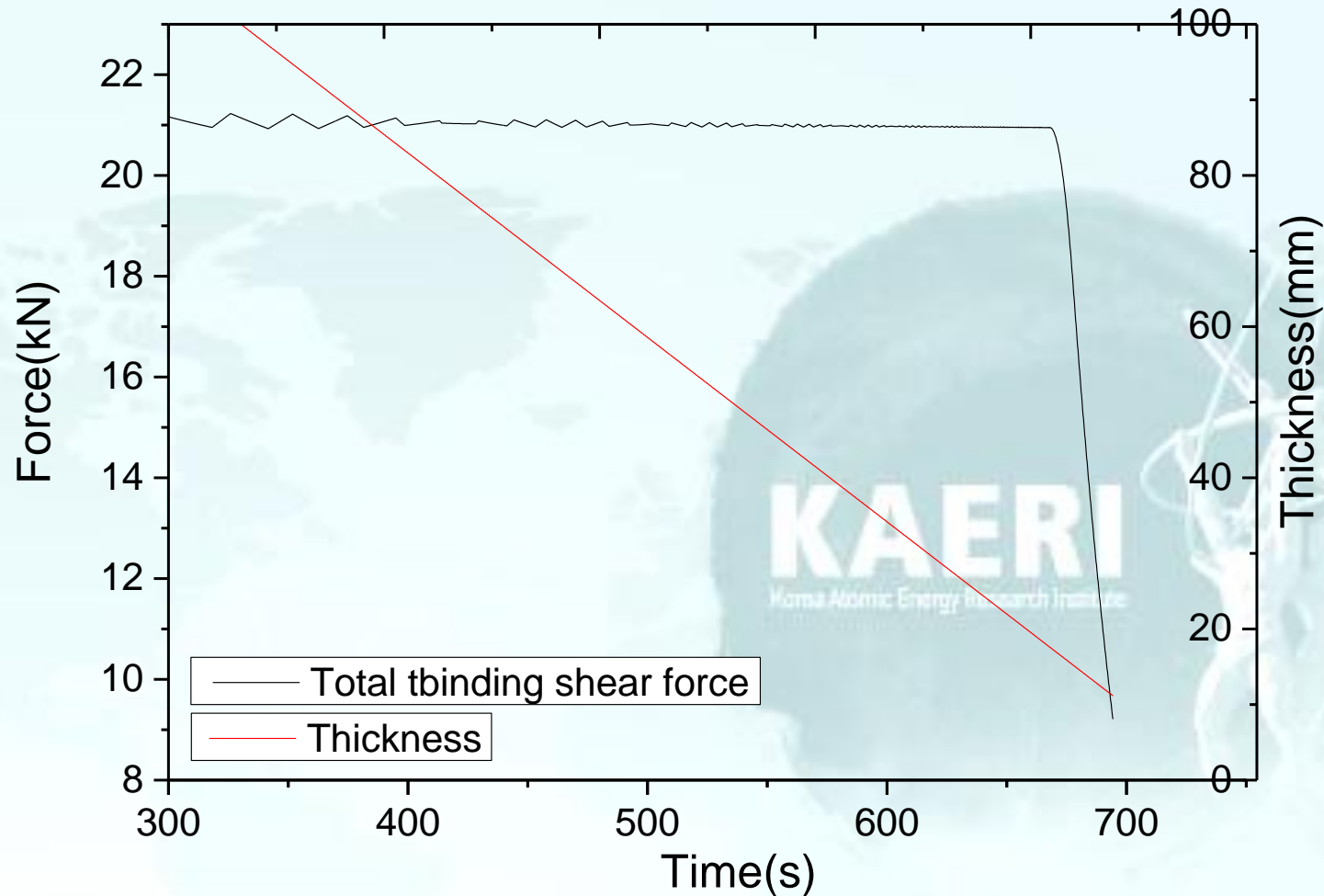
□ Tube Ejection



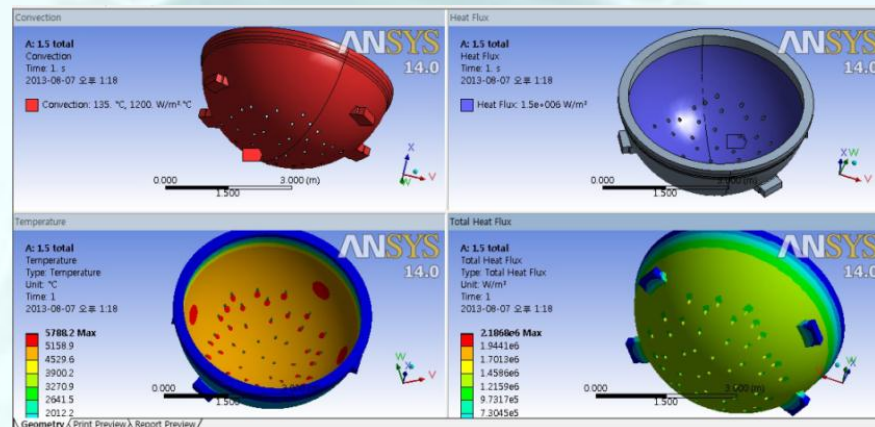
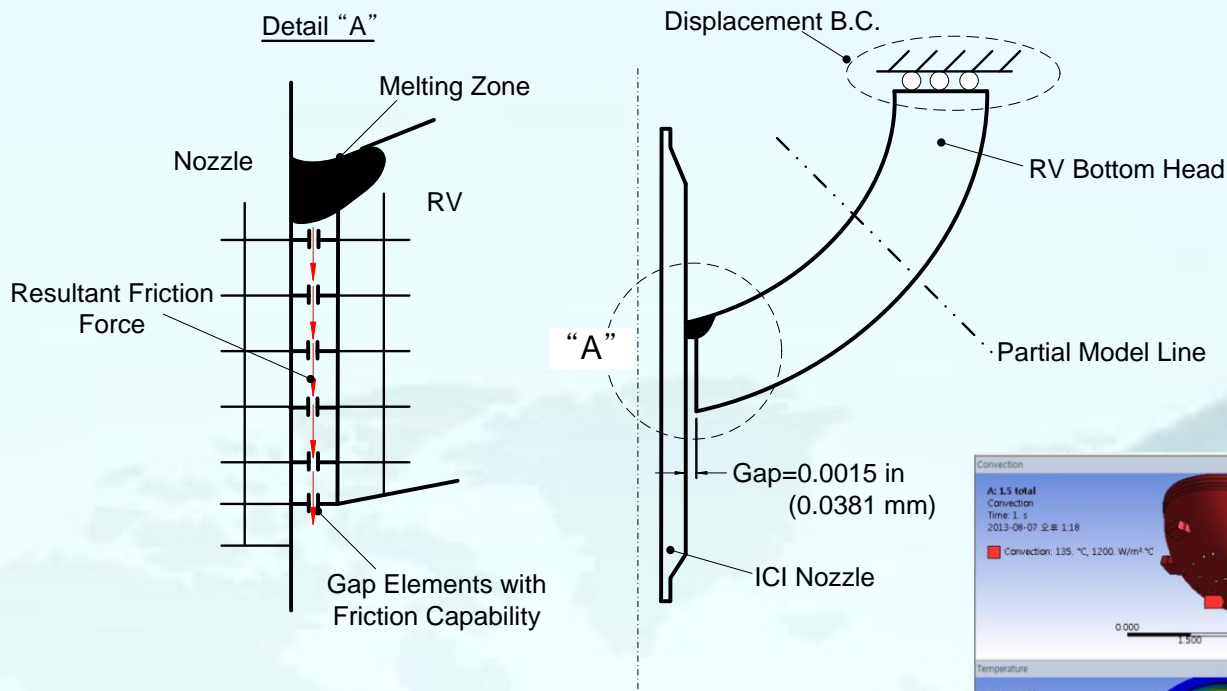
Failure Models & Calculations (7)

□ Tube Ejection

✓ Top surface temperature = 1950°C



ANSYS Analysis



Deformation of reactor vessel affects the gap.
Clamping or non-clamping ICI nozzle depends on the location.
Clearance gap size may change.

Concluding Remarks

- APR1400 ICI penetration tube failure study
 - Welding material erosion test at VESTA-S facility
 - ICI penetration tube failure test at VESTA facility
 - ICI penetration tube failure calculation with suggested model

- Future work
 - Test with high heat flux and elevated pressure
 - Test under the external reactor vessel cooling condition
 - Analysis in case of clearance gap change