

# Hydride Effect on Cladding Behaviour for Spent Fuel Storage and Transport Conditions

IAEA- International Conference on Management of Spent Fuel  
Vienna, Austria , 15 – 19 June 2015

M. Lloret (ENUSA)

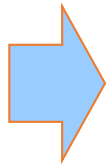
J.M. Rey Gayo (CSN) –F.J. Fernández (ENRESA)



# Spanish Fuel Cycle Strategy - Open Cycle



URANIUM



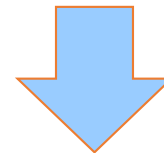
ENUSA FACTORY



REACTOR



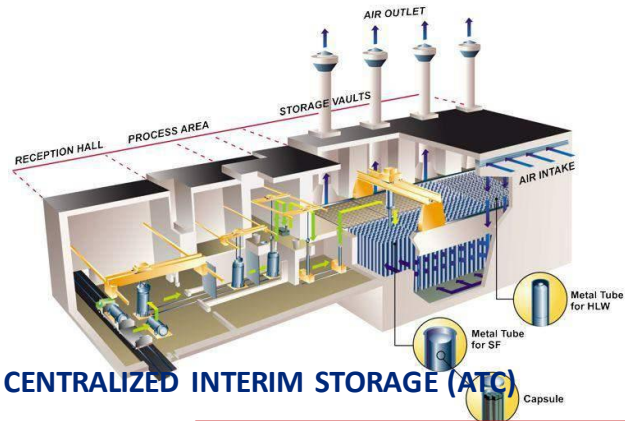
SPENT FUEL POOL (re-racking)



INDEPENDENT SPENT FUEL STORAGE INSTALLATION (ISFSI)



TRANSPORT



CENTRALIZED INTERIM STORAGE (ATC)

Designed in detail  
Being licensed  
Operation in 2018

3 ISFSI in operation



# Dry Spent Fuel Storage and Transport

## SAFETY FUNCTIONS

Subcriticality  
Confinement  
Retrievability  
Heat Removal  
Shielding

Requirements in standards  
10CFR 71 / 10 CFR 72  
No gross cladding rupture  
Geometric form not altered

Key Parameter  
Cladding Integrity

Cladding Failure mechanism

Creep

Hydride embrittlement

...

Good behaviour  
Analyzed in other  
R&D projects <sup>(1)</sup>

Objective of the R&D  
project presented today

(1) M. Quecedo et al. "Results of Thermal Creep Test on Highly Irradiated ZIRLO". WRFPM 2008. Korea  
M. Lloret et al. "Results of thermal creep tests on irradiated Zry-2", TopFuel meeting, Manchester, UK, 2012



# R&D Project

Objective: Effect of hydrides in cladding behaviour during dry storage and transport

Material: Prehydrated/ Non irradiated ZIRLO Cold Work Stress Relieved (CWSR)

Results presented:

- ✓ Cladding Hydration
- ✓ Hydride reorientation
- ✓ Ring Compression Tests
- ✓ Effect of Circumferential vs Radial Hydrides
- ✓ Fractographic analysis
- ✓ Failure criteria

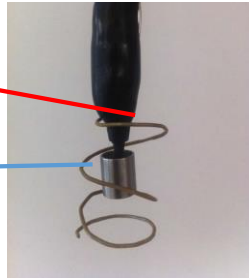
# Cladding hidruration

- Cathodic Charge technique in KOH solution

Pt anode

Zr cathode

Cladding sample



- ✓ Parameters can be adjusted to obtain different H concentrations

- Thermal treatment

- ✓ Homogeneous distribution along hoop direction

450°C

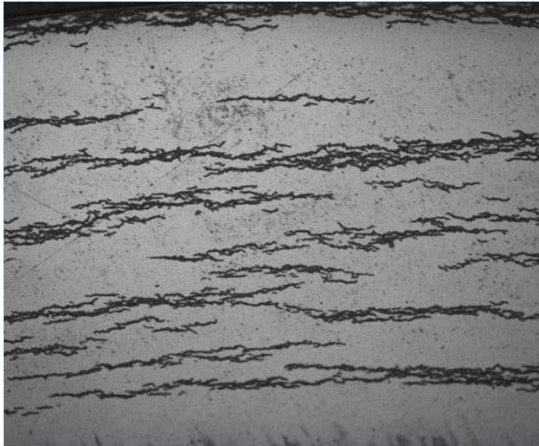
20°C



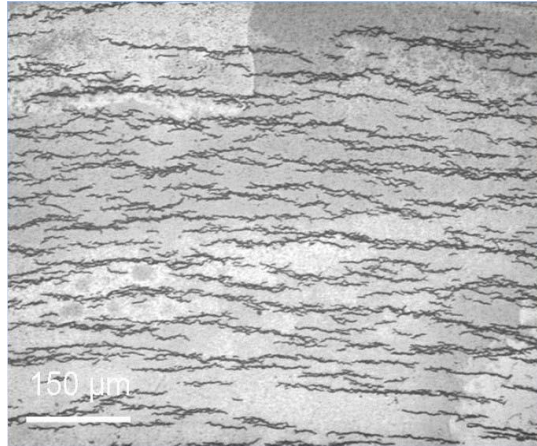


# Cladding hidruration

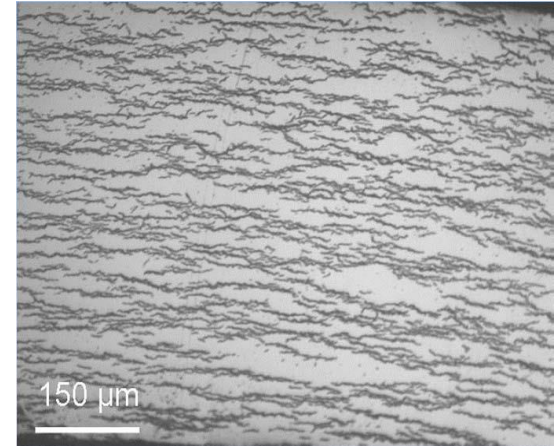
- 150 – 500-1200-2000 ppm hydrogen



150 ppm



500 ppm



1200 ppm

# Hydride reorientation along radial direction



Circumferential stress  
0-60-90-120-140 MPa

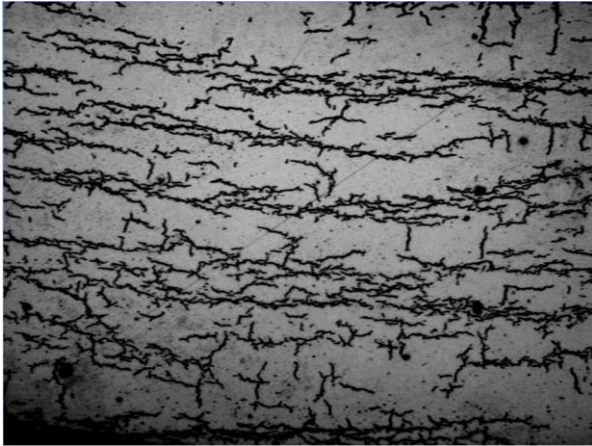
Termomechanical treatment



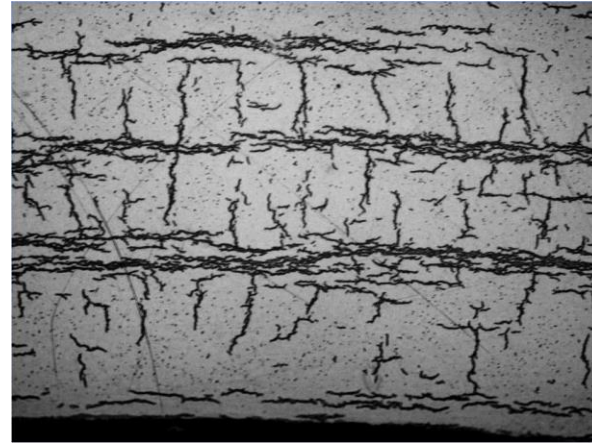
Constant hoop stress during cooling down:  
Thermal dilatation considered and load  
decreases as temperature decreases

# Hydride reorientation along radial direction

## Cladding samples

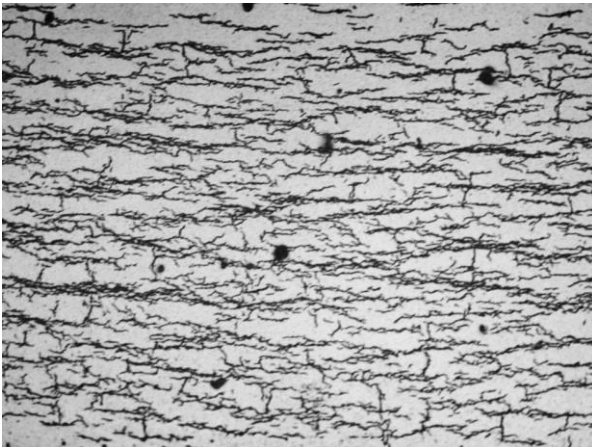


90 MPa



140 MPa

150 ppm

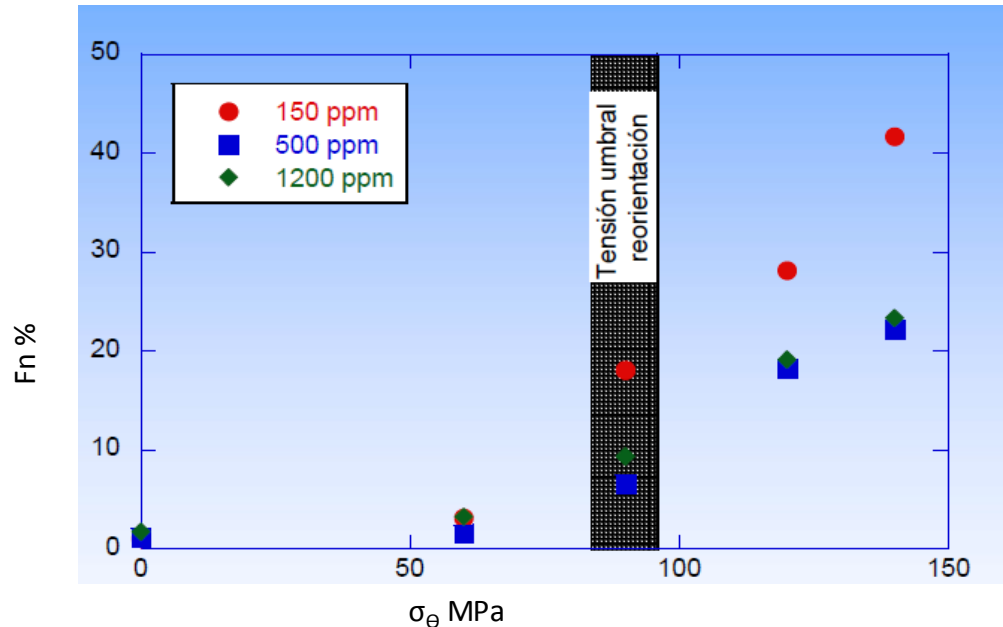


1200 ppm



# Hydride reorientation

- Fn factor (reoriented hydride percentage) has been calculated for de 3 hydrogen concentration
- It has been calculated following ASTM B811

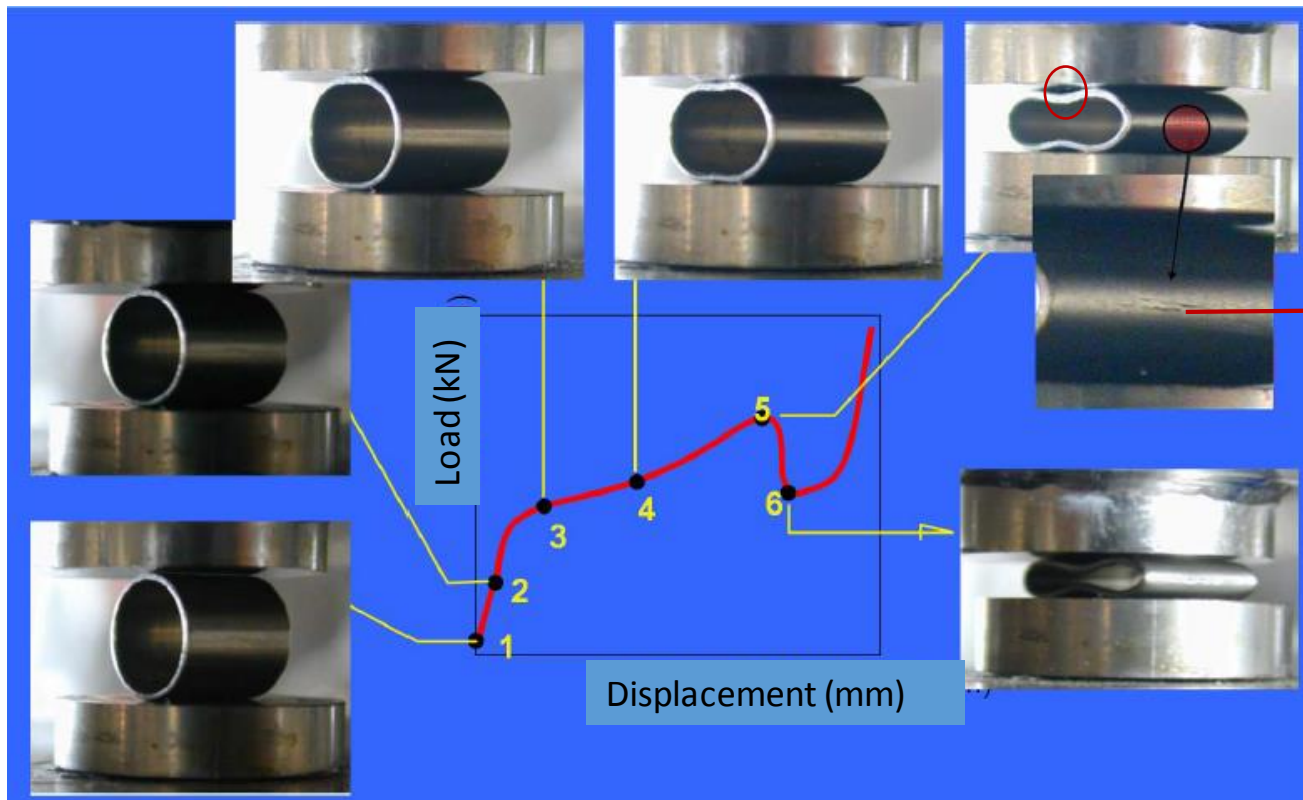


Highest reorientation factor for 150 ppm  
Similar values and evolution for 500 and 1200 ppm

# Ring Compression Tests

Mechanical tests has been performed on different hydrides morphologies samples to evaluate the cladding structural integrity

Representative Load-Displacement curve



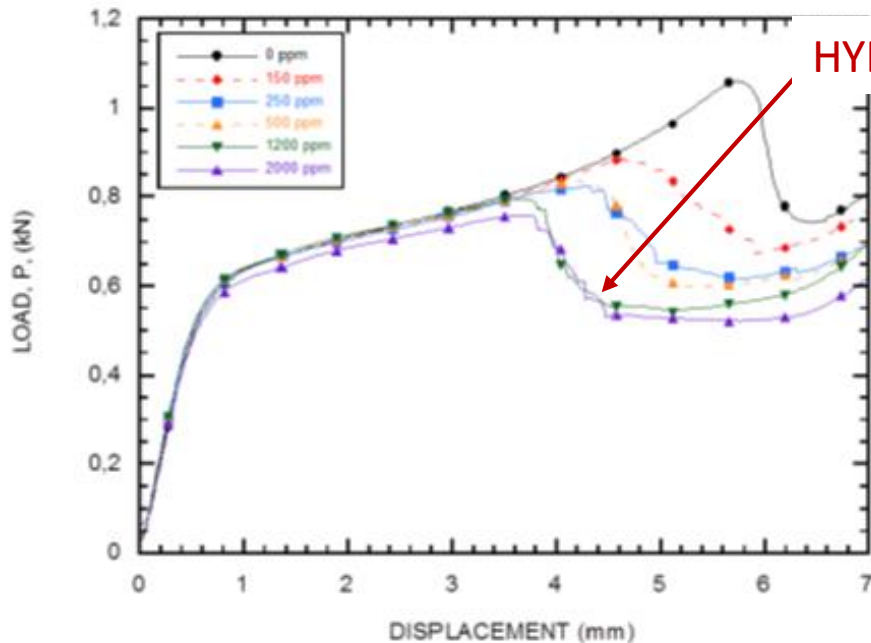
# RCT - Circumferential Hydrides

## Test Conditions

Temperature: 20, 135, 300 °C

Hydrogen content: 150, 250, 500, 1200, 2000 ppm

20 °C



HYDROGEN INCREASE

↑ [ H ]   ↓ displacement for crack initiation

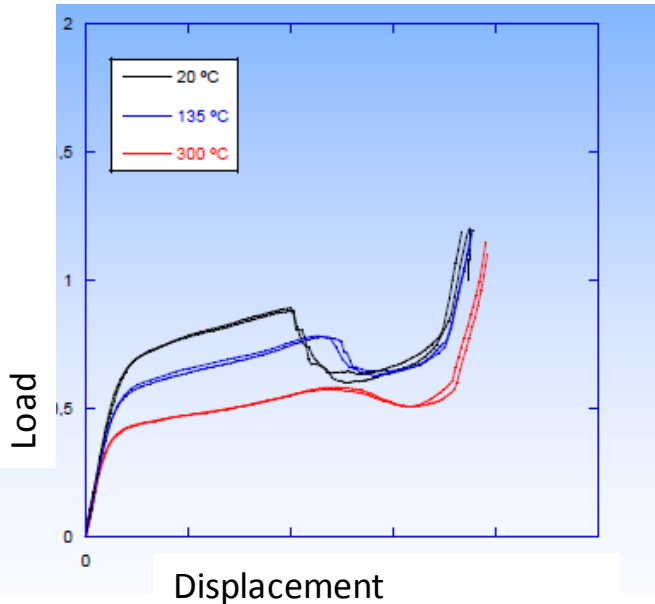
Displacement always higher than 3mm

Yield strength / Young Modulus

No dependence with [H]

# RCT- Circumferential Hydrides

Similar results for 135 and 300 °C



Results for the same hydrogen concentration (1200 ppm) and different temperature

Temperature effect as expected:

Same Young's Modulus

Lower Yield Stress at higher Temperature

Displacement for crack initiation always higher than 3 mm

Ductility is not a problem with circumferential hydrides





# RCT- Radial Hydrides

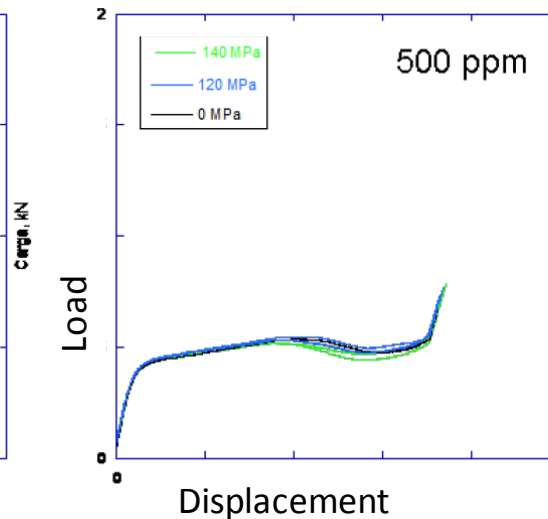
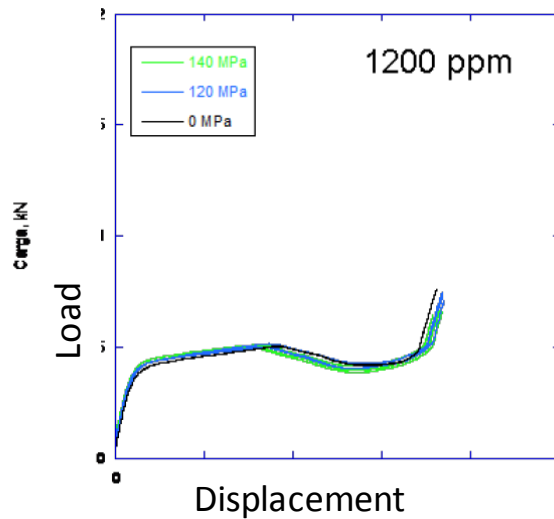
## Test Conditions

Temperature: 20, 135, 300 °C

Hydrogen content: 150, 500, 1200 ppm

Reorientation Hoop Stress: 60, 90, 120, 140 MPa

300 °C



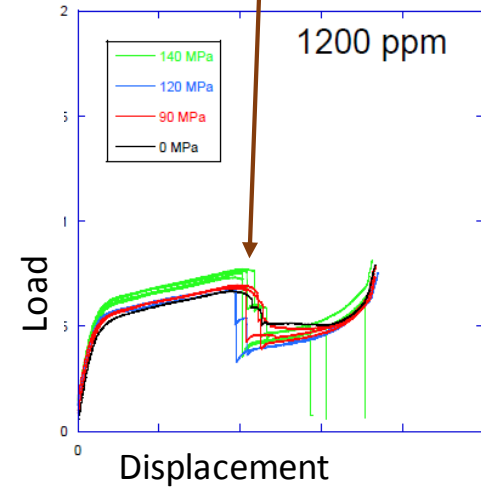
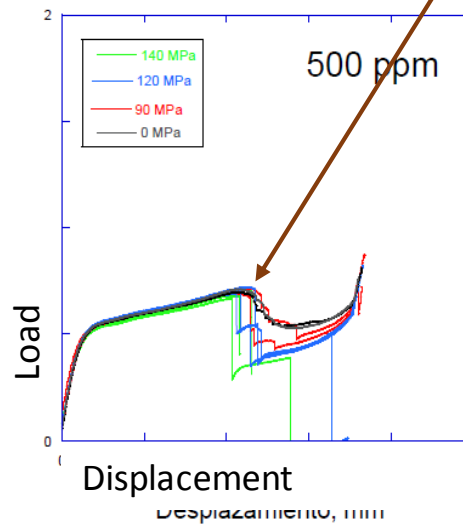
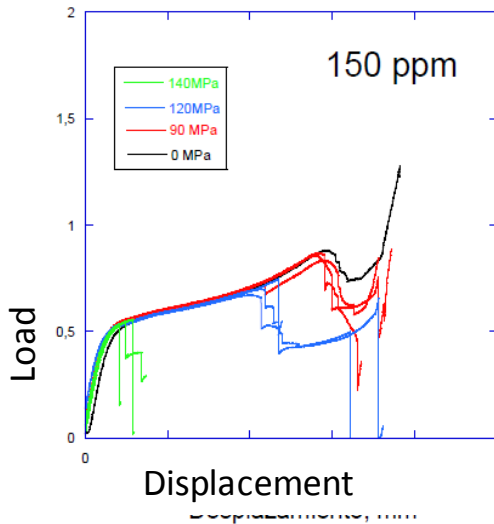
No effect of reoriented  
hydrides  
Enough ductility

300 °C  
DUCTILE BEHAVIOUR

# RCT- Radial Hydrides

135 °C

Enough ductility  
Rupture displacement  
almost independent of  
radial hydrides



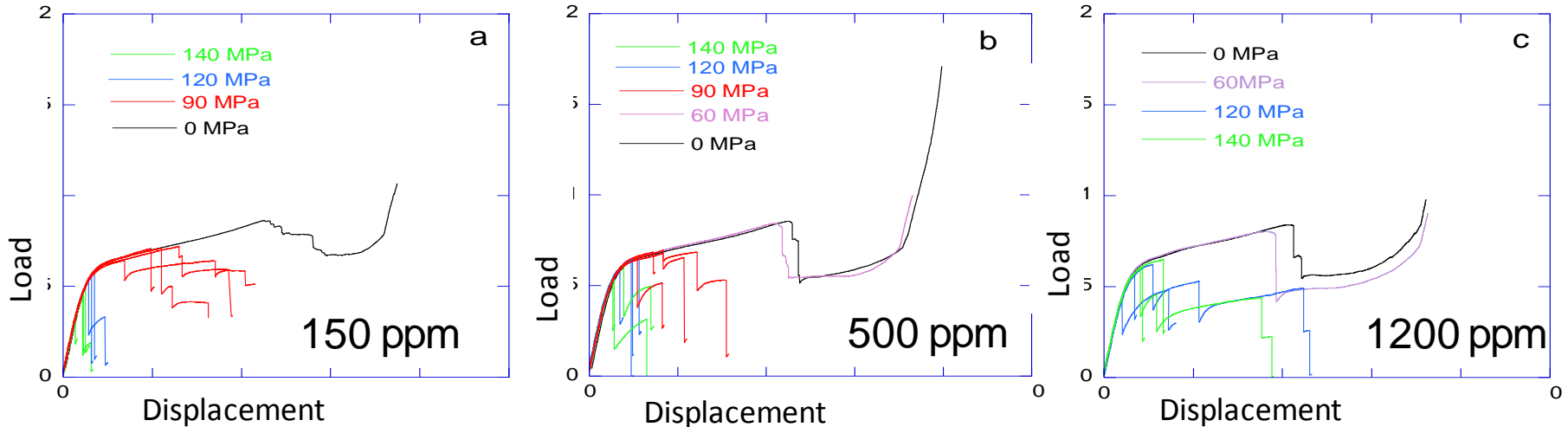
150 ppm  
Relevant effect of radial  
hydrides

Higher radial effect for lower hydrogen content  
Related with Radial-Hydride-Continuity Factor (RHCF) <sup>(2)</sup>

**DUCTILE BEHAVIOUR EXCEPT FOR 150PPM AND 140 MPA**

# RCT- Radial Hydrides

20 °C



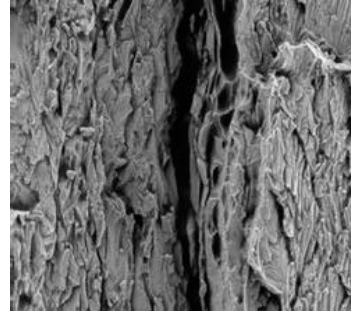
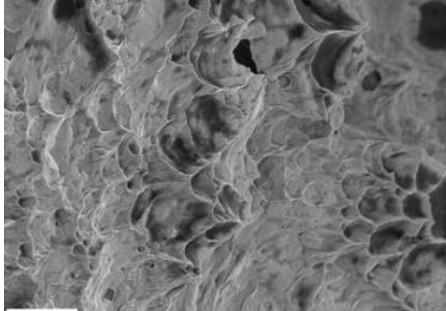
- Important effect of radial hydrides
- Relevant decrease of displacement for failure when radial hydrides increase
- Rupture in elastic zone in some cases for reorientation stresses higher 90 MPa

**DUCTILE ONLY FOR REORIENTATION HOOP STRESS  
LOWER THAN 90 MPa**

# Fractographic analysis

- Scanning Electron Microscopy analysis of fracture surface to identify fracture micromechanism has been performed

ductile



brittle

## Failure criteria

- Three different failure criteria based on strain, plastic deformation and Strain Energy Density has been considered.



# Conclusions

- CSN, ENRESA & ENUSA have performed R&D projects regarding cladding material behaviour during dry storage and transport
- Samples with embrittlement states similar to irradiated material has obtained
- RCT at temperatures representative of storage and transport have been performed
- Circumferential hydrides: the material is ductile, even for 2000 ppm hydrogen and 20°C
- For radial hydrides, hydrogen content, reoriented hydride percentage, and temperature are key parameters
- The results are coherent with other authors published data for non irradiated material

**Thank you  
for  
your attention**

[www.enusa.es](http://www.enusa.es)

