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On the impact of the fuel assembly design evolution in the spent fuel management

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INTRODUCTION: SPENT FUEL MANAGEMENT IN SPAIN

- Spanish model based on Dry Storage
- Current situation: some NPPs storing fuel assemblies in casks
- Near future: Spanish spent fuel (9 spent fuel pools) <u>transported</u> to a centralized interim storage facility (ATC)
- Regulation by Spanish National Safety Council (CSN). Based on dry storage and transportation US NRC 10 CFR parts 72 and 71
- Damage fuel definition in ISG-1 Rev.2:

Damaged fuel is any fuel rod or fuel assembly that cannot fulfill its fuel-specific or system-related functions



INTRODUCTION: ENUSA IN THE NUCLEAR FUEL CYCLE



ENUSA state owned company:

- Engineering
- Manufacturing (350 Tm, PWR and BWR)
- On-Site services
- Madrid: Engineering and
 Commercial
 - Juzbado (Salamanca): Fuel

Assembly Manufacturing and

On-Site Services



INTRODUCTION: ENUSA IN THE NUCLEAR FUEL CYCLE

- > 40 years on design, manufacturing, follow up, on-site services, etc. of PWR and BWR fuel in several European NPPs
- >10 years on spent fuel characterization, inspection, conditioning, classification and loading into dry storage casks in Spanish NPPs

ENUSA has deep **knowledge** and **experience** of the entire nuclear **fuel cycle** and possible effects of different steps of the fuel cycle in late steps







OBJECTIVE OF THE PRESENTATION

Effects of the **evolution** of fuel assembly design in the **spent fuel management.** Through three representative examples on PWR fuel:

- **1.** Fuel rod design: rod internal pressures,
- 2. Assembly materials: stress corrosion cracking,
- 3. Fuel rod materials: Zr oxide layer spalling.

For each example: spent fuel **regulation basis**, phenomena **description**, **impact** on spent fuel management and ENUSA **solutions**.



1.-FUEL ROD DESIGN: HIGH FUEL ROD INTERNAL PRESSURE

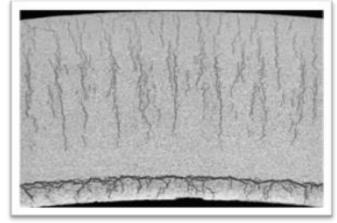
ISG 11 Rev. 3 "Cladding Considerations for the Transportation and Storage of Spent Fuel"

Low burnup fuel (*BU* < 45 *MWd/kgU*)

- Cladding T < 400°C for normal conditions and short-term loading operations</p>
- If short-term loading operations cladding T > 400 °C , $\sigma_{\theta} ≤ 90$ MPa (σ_{θ} , hoop stress, should be calculated)

Goal:

<u>Avoid hydride reorientation</u> = cladding with lower mechanical properties





1.-FUEL ROD DESIGN: HIGH FUEL ROD INTERNAL PRESSURE

First PWR fuel rods had:

- High as-built internal pressure to avoid cladding collapse
- Low plenum length to compensate irradiation growth
- Non-controlled pellet porosity
- Constant pitch plenum spring



Low volume to

accommodate

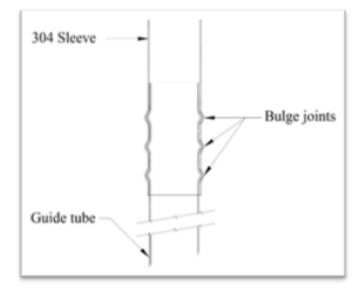
- > Impact on spent fuel management : several assemblies having first rod designs for which σ_{θ} <90 MPa should be justified
- > ENUSA has developed a hoop stress calculation methodology:
 - By thermomechanical code calculations
 - Cladding axial temperature profile inside the cask



2.- ASSEMBLY MATERIALS: STRESS CORROSION CRACKING

ISG 2 Rev. 1 "Fuel Retrievability"

- Fuel assemblies must be retrievable by normal means (grapple and hook). Those assemblies that cannot meet this criterion should be placed in a can for damaged fuel or modified, so the assembly or can may be ready retrievable from the storage canister by normal means".
- First PWR designs SCC of SS304 top nozzle sleeves
 - Material: sensitized 304 stainless steel
 - Residual **stresses** after cold bulge deformation
 - **Environment**: non controlled sulfate concentration in the SFP



2.- ASSEMBLY MATERIALS: STRESS CORROSION CRACKING

Risk of top nozzle detachment, affecting to ready retrievability requirement

Impact on spent fuel management:

- More than 18000 affected assemblies worldwide
- Sleeves visual inspections
- Handling limitations
- Handling using special tooling
- Conditioning to be handled by normal means
- > Avoided by **design evolution** to a different top nozzle joint concept
- For the old designs, ENUSA is currently performing visual inspections and handling with limitations the Spanish fuel affected by SCC



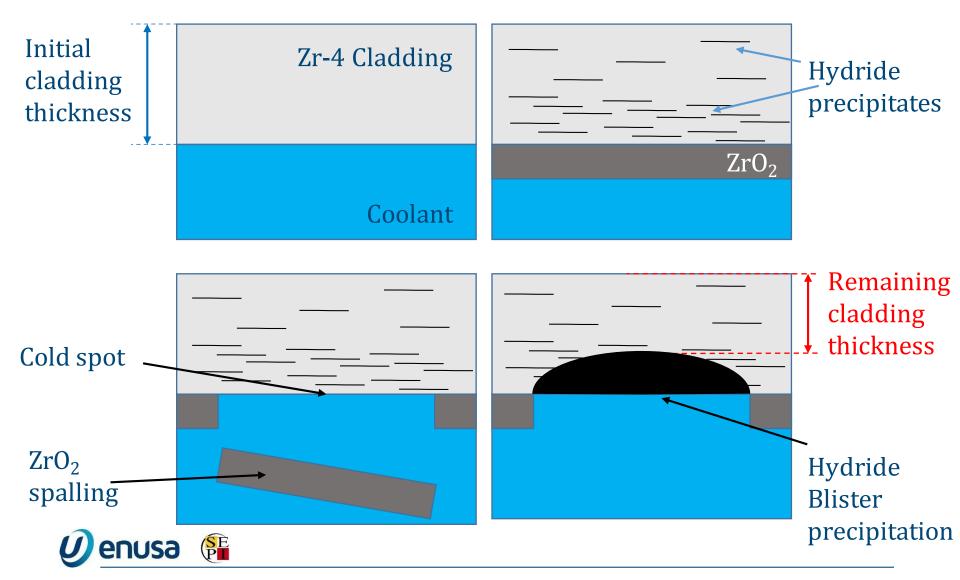
3.- IMPACT OF CLADDING MATERIALS: OXIDE SPALLING

ISG 1 Rev. 2 "Classifying the Condition of Spent Nuclear Fuel for Interim Storage and Transportation Based on Function"

- The spent fuel cladding must be protected during storage against degradation that leads to gross ruptures.
- The geometric form of the package would not be substantially altered.



3.- IMPACT OF CLADDING MATERIALS: OXIDE SPALLING



3.- IMPACT OF CLADDING MATERIALS: OXIDE SPALLING

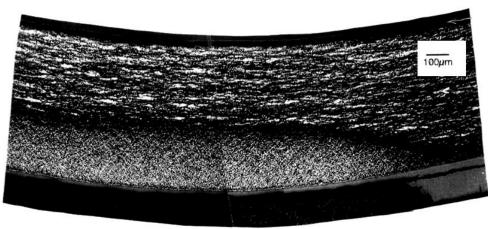
- Zircaloy-4 cladding oxide layer spalling
 - Primary coolant contacts the base metal: **cold spot**
 - Local $\Delta T \rightarrow \text{massive Zr hydride precipitation: hydride blister (brittle)}$



P. Bossis, ASTM STP 1467 (2006)

A.M. Garde, ASTM STP 1295 (1996)





IMPACT OF CLADDING MATERIALS: OXIDE SPALLING

Possible local decrease of cladding mechanical integrity for storage and transportation in the spalled areas

Impact on spent fuel management:

- Several Zircaloy-4 cladding assemblies are affected (not observed in ZIRLO cladding)
- Cladding visual inspections
- ENUSA, in collaboration with other partners in the Spanish nuclear industry, has analyzed this effect by conservative calculation
- Besides, ENUSA is involved in R&D programs focused in obtaining knowledge and data about the fracture modes during dry storage and transportation of fuel cladding affected by hydride blister precipitation.



SUMMARY

- Analysis of the evolution of three main PWR fuel assembly design fields and their **impact on spent fuel management**:
 - High rod internal pressures in transportation and storage,
 - Stress corrosion cracking in spent fuel retrievability,
 - Zr oxide layer spalling in transportation and storage.
- Knowledge of the past and current designs and the potential effects of future design changes are fundamental in order to accomplish an optimum spent fuel management.
- The design process should include an analysis of the impact of the design changes in the future spent fuel management.



THANK YOU FOR YOUR ATTENTION

QUESTIONS?

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